

# Characterization of the TES sensors for the Ricochet experiment

Ran Chen  
for the Ricochet Collaboration

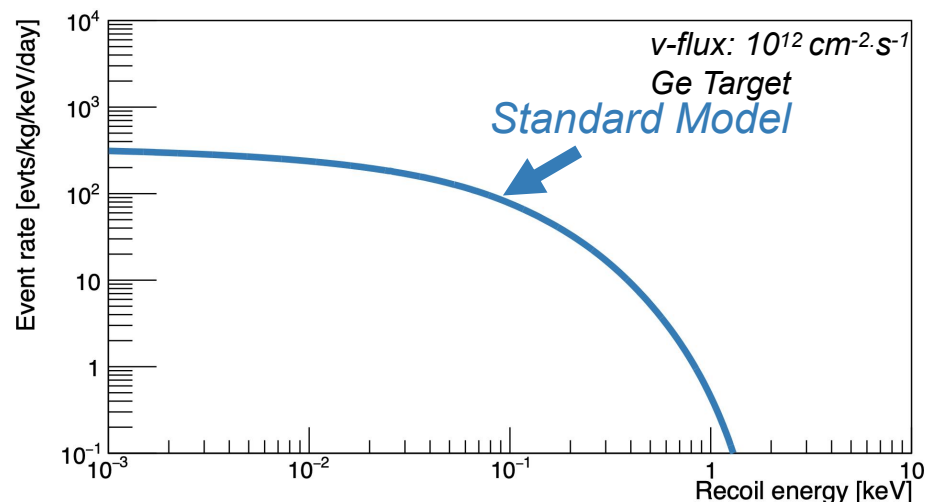
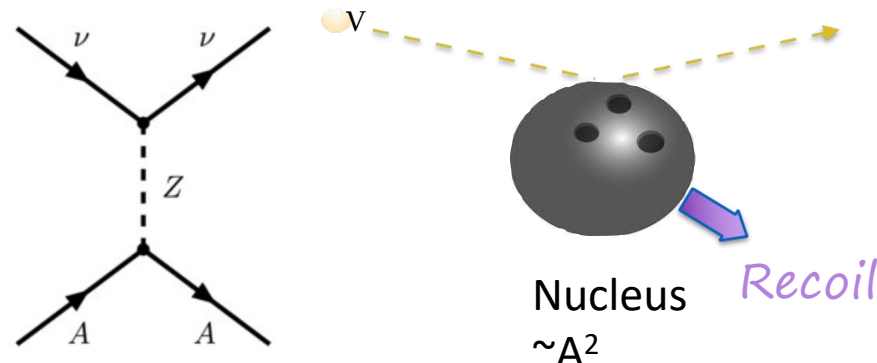
## CEvNS: Coherent Elastic Neutrino-Nucleus Scattering

CEvNS:

- Coherent Elastic Neutrino-Nucleus Scattering
- 2017: Observed via neutrinos of tens of MeV at SNS.
- 2022: Observed at reactors.

Ricochet goals:

- First,  $5\sigma$  observation of low-energy CEvNS
- Then, precision measurement of spectrum



## CEvNS: Coherent Elastic Neutrino-Nucleus Scattering

CEvNS:

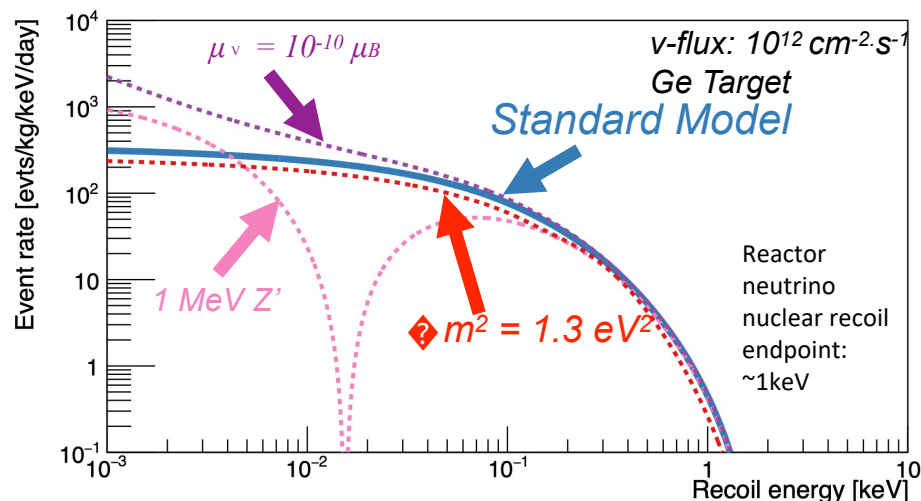
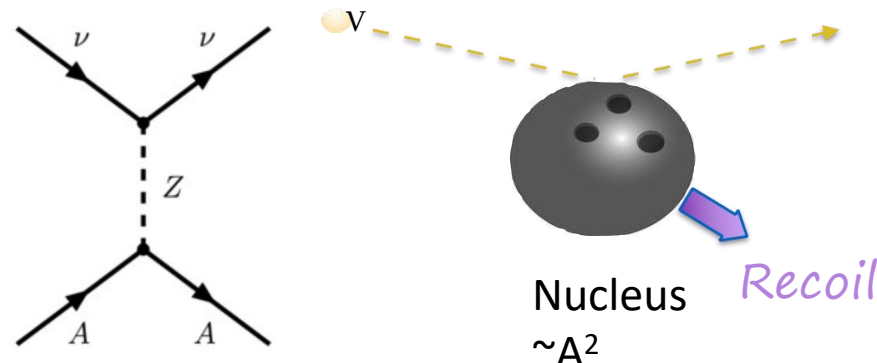
- Coherent Elastic Neutrino-Nucleus Scattering
- 2017: Observed via neutrinos of tens of MeV at SNS.
- 2022: Observed at reactors.

Ricochet goals:

- First,  $5\sigma$  observation of low-energy CEvNS
- Then, precision measurement of spectrum

Sensitive to new physics, including

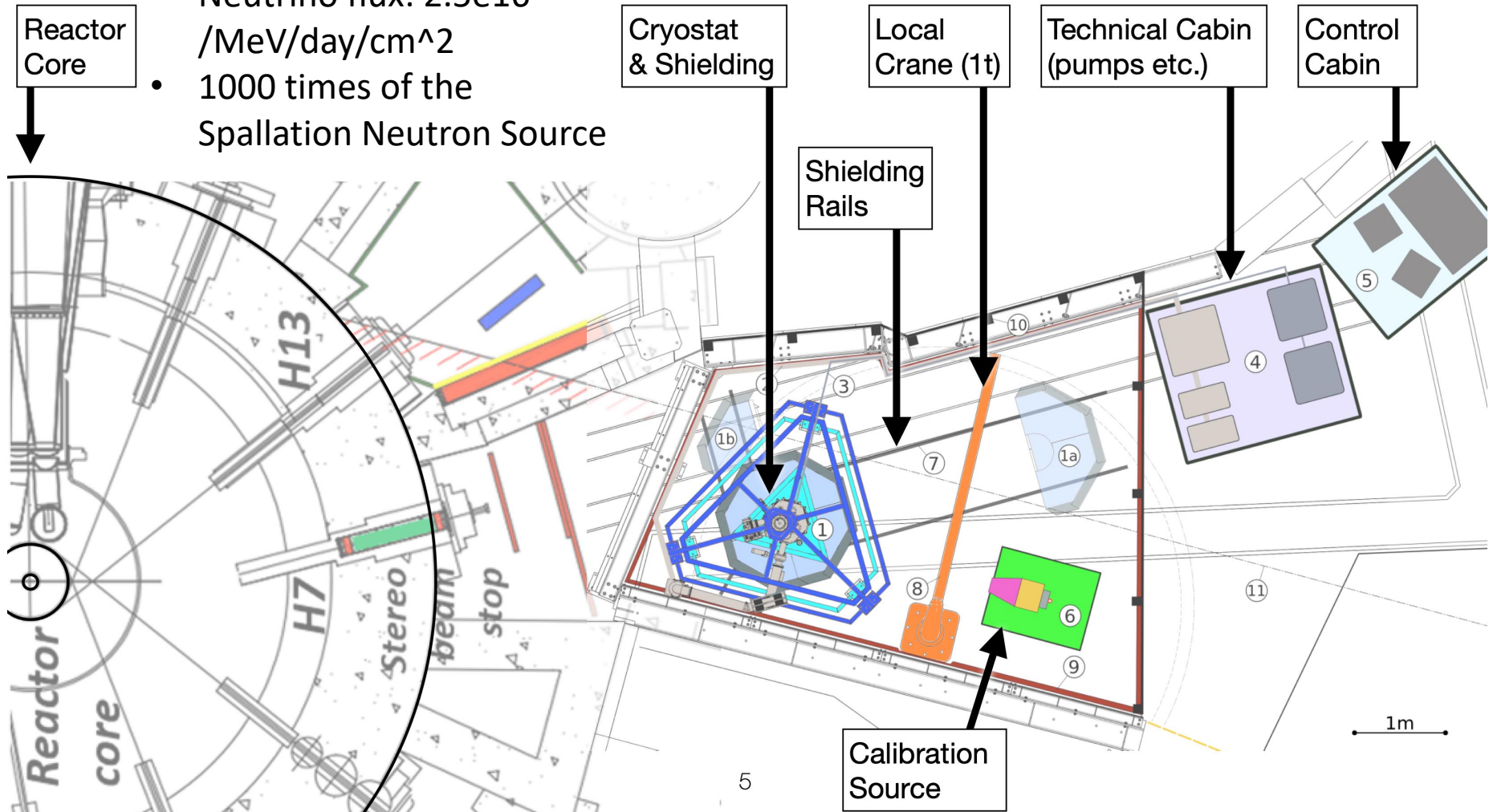
- neutrino mag. moment
- sterile neutrinos
- new force mediators



# The ILL Reactor in Grenoble, France

RICOCHET

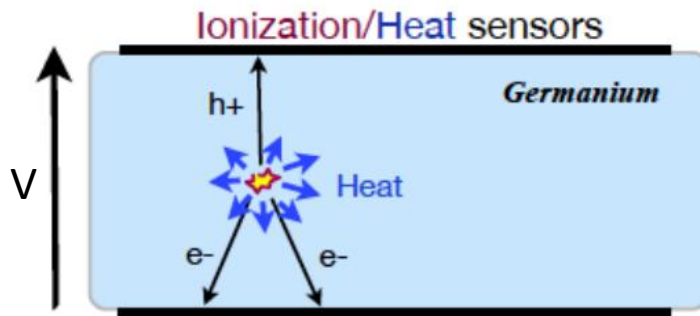
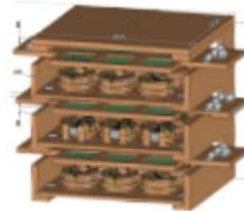
- Reactor Power: 58 MW
- Neutrino flux:  $2.5 \times 10^{16}$  /MeV/day/cm<sup>2</sup>
- 1000 times of the Spallation Neutron Source



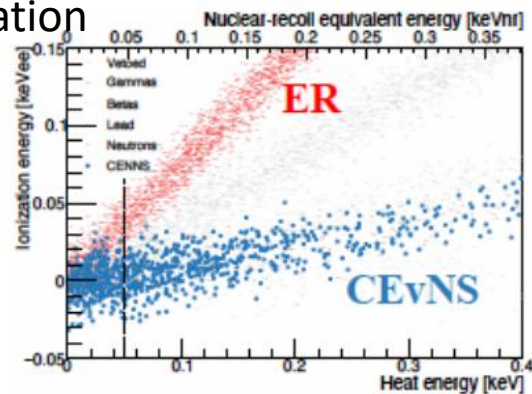
## “CryoCube”

Ionization+Heat in Ge

Sensors: NTDs and HEMTs



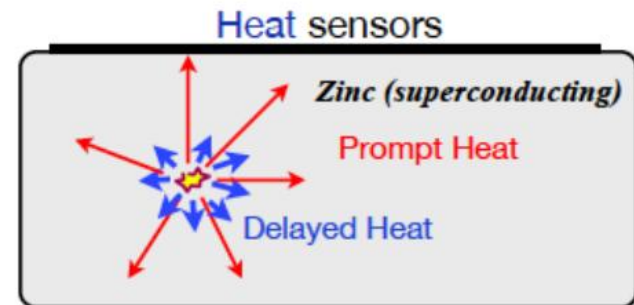
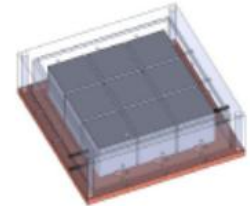
Simulation



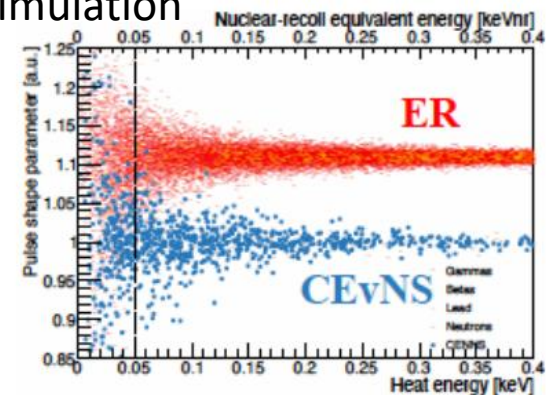
## “Q-Array”

Heat Pulse Timing in Zn

Sensors: TESs



Simulation

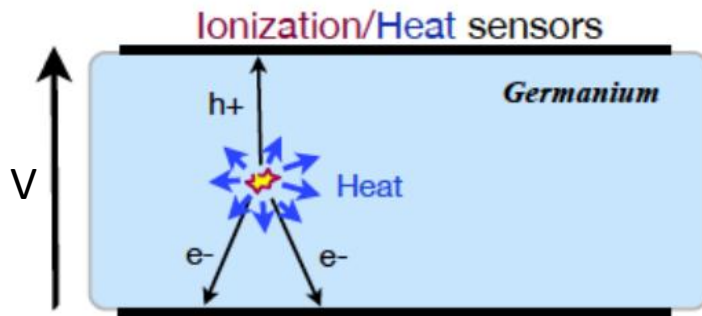
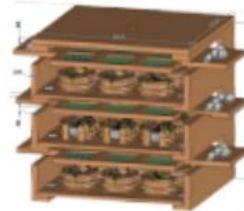




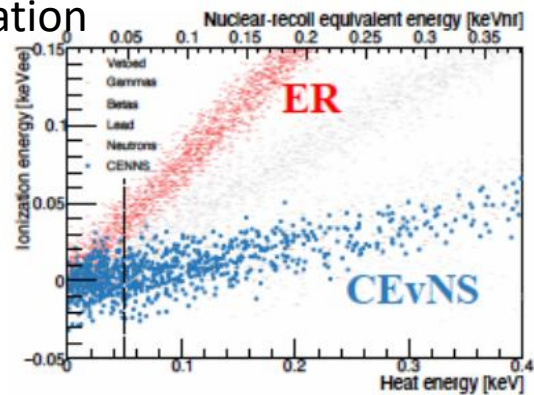
## “CryoCube”

Ionization+Heat in Ge

Sensors: NTDs and HEMTs



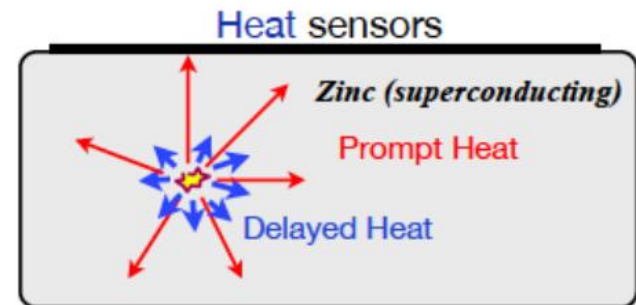
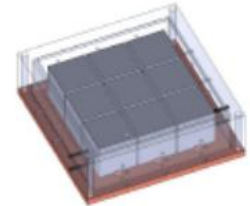
Simulation



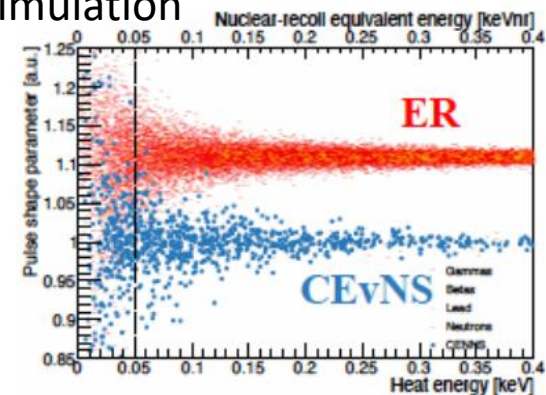
## “Q-Array”

Heat Pulse Timing in Zn

Sensors: TESs

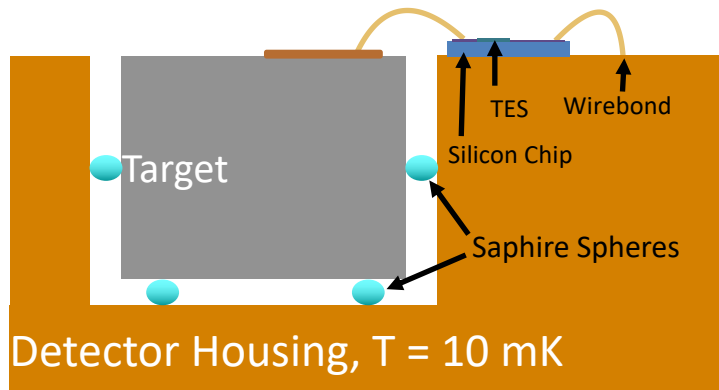


Simulation

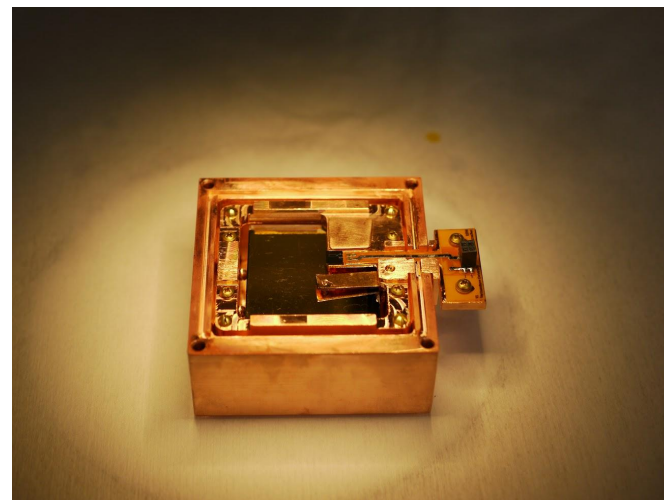


# A New Architecture for Modular Cryogenic Detectors

- New modular sensor design using Al/ Mn Transition Edge Sensors (TES)
- Scalable architecture decoupling target from thermometer
- Designs for both Ricochet (reactor coherent neutrino scattering) and CUPID (neutrinoless double beta decay) experiments underway

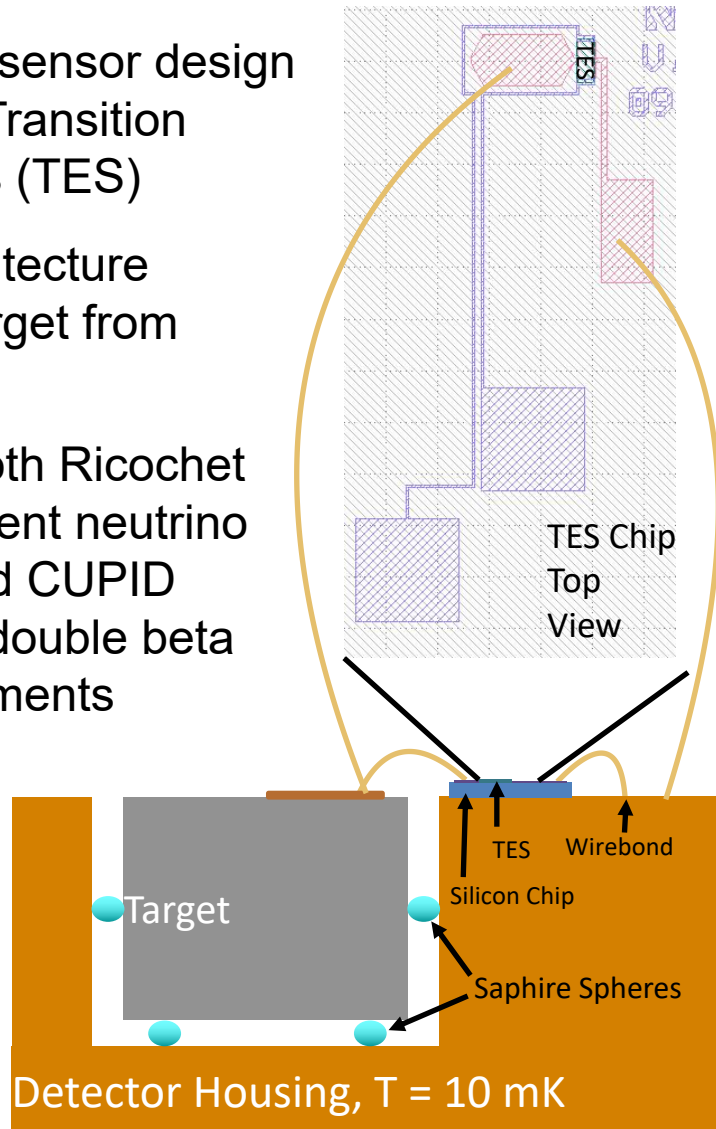


Detector Housing

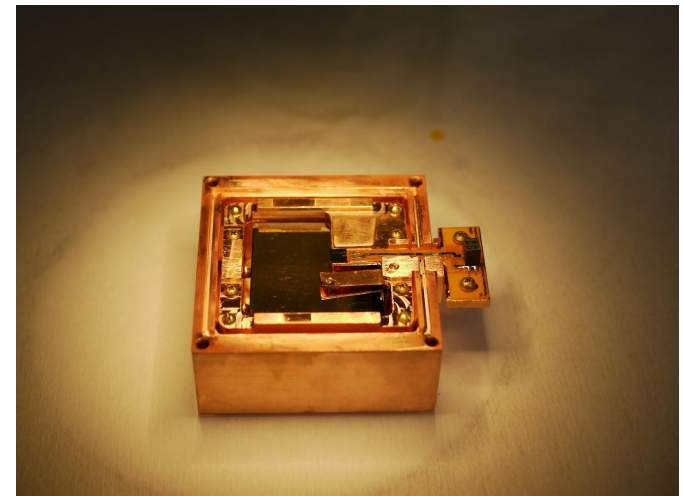


# A New Architecture for Modular Cryogenic Detectors

- New modular sensor design using Al/ Mn Transition Edge Sensors (TES)
- Scalable architecture decoupling target from thermometer
- Designs for both Ricochet (reactor coherent neutrino scattering) and CUPID (neutrinoless double beta decay) experiments underway



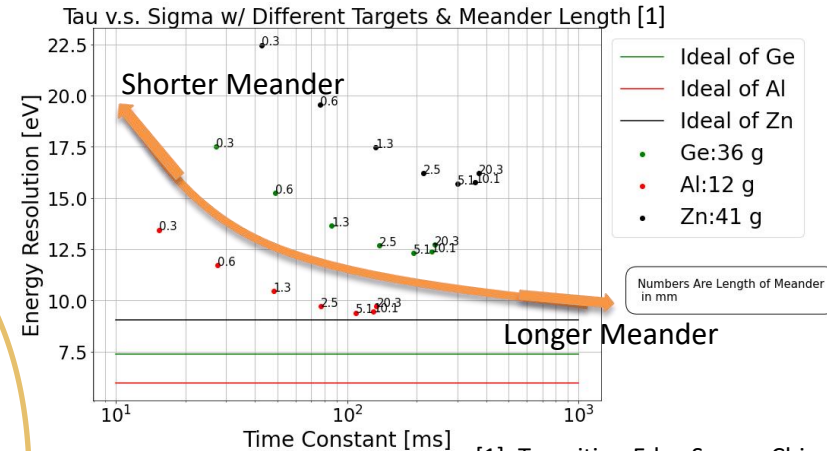
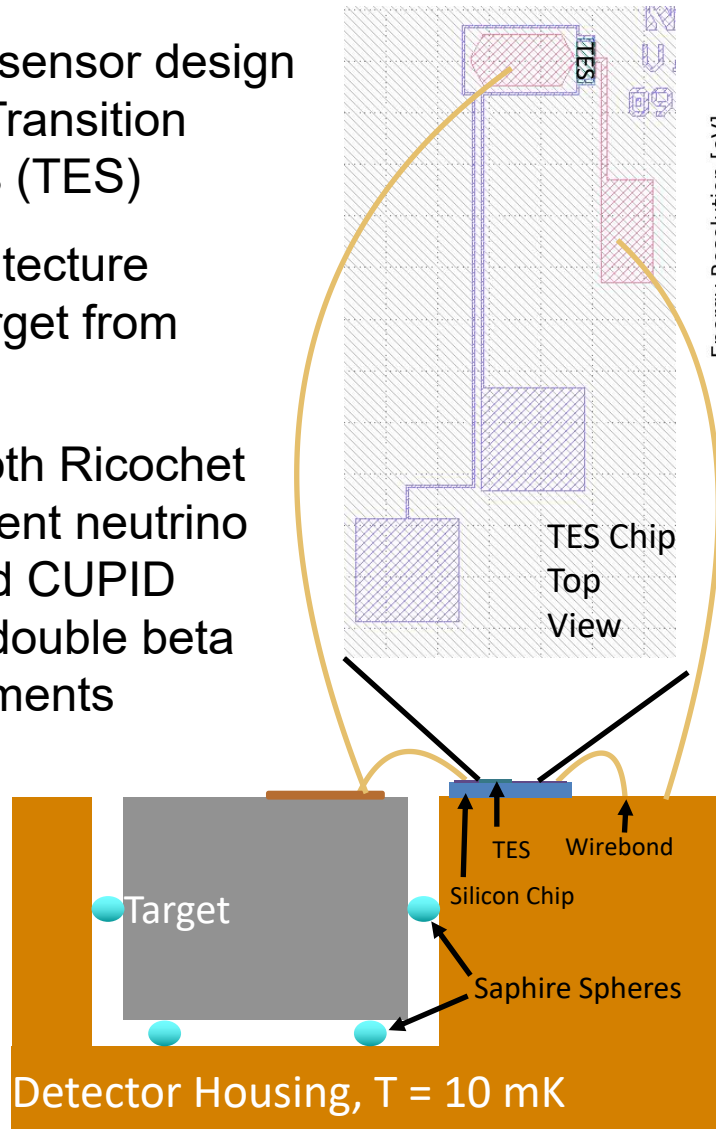
Detector Housing





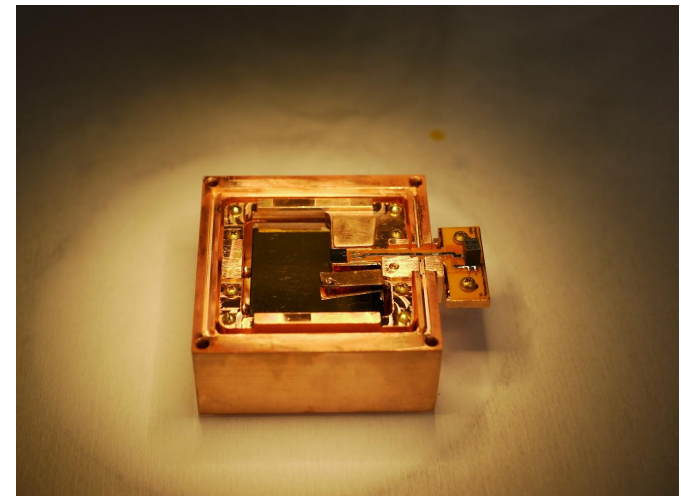
# A New Architecture for Modular Cryogenic Detectors

- New modular sensor design using Al/ Mn Transition Edge Sensors (TES)
- Scalable architecture decoupling target from thermometer
- Designs for both Ricochet (reactor coherent neutrino scattering) and CUPID (neutrinoless double beta decay) experiments underway

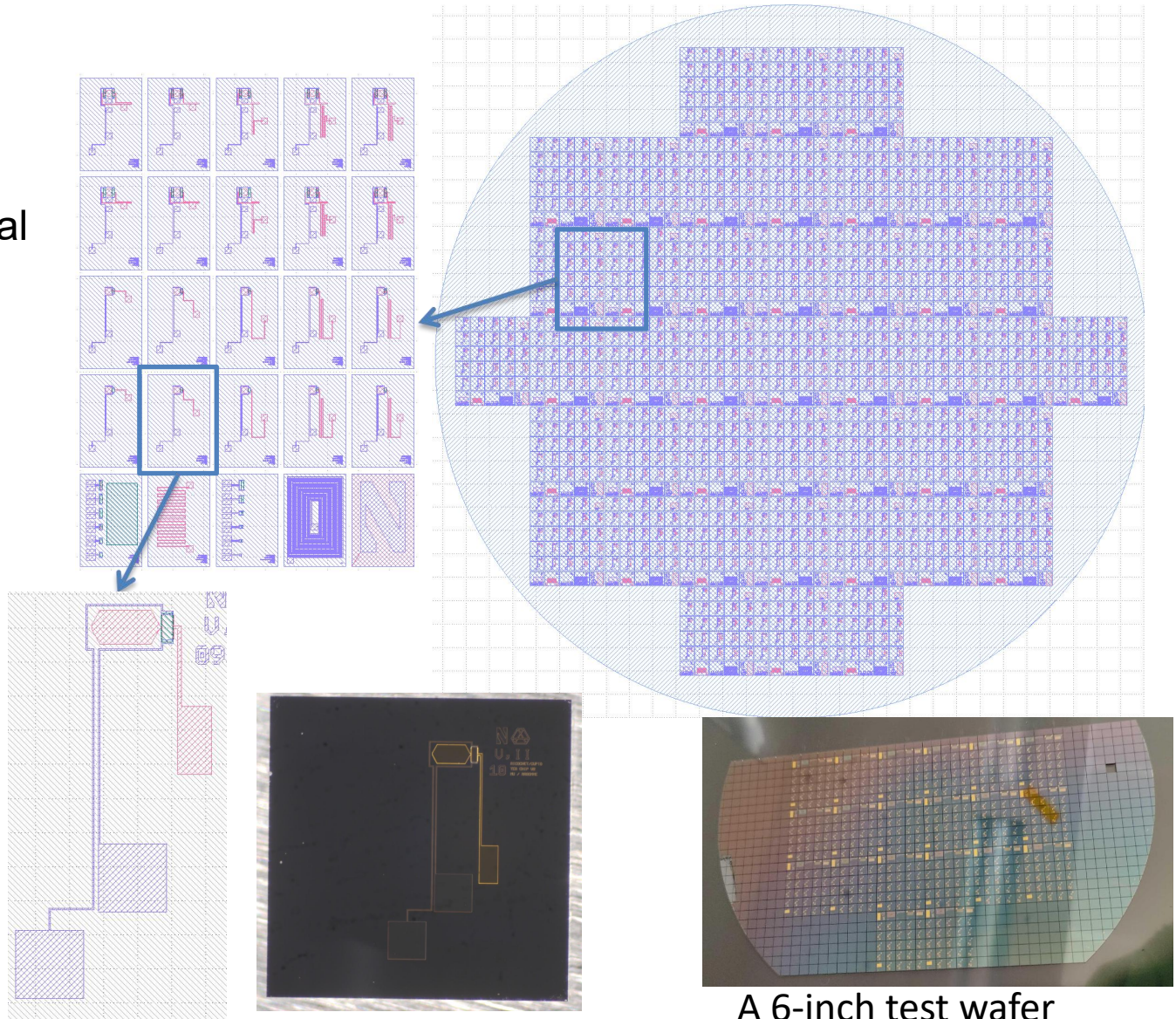


[1]: Transition Edge Sensor Chip Design of Modular CEvNS Detector for the Ricochet Experiment. R. Chen, et al. <https://arxiv.org/abs/2111.05757>

**Detector Housing**

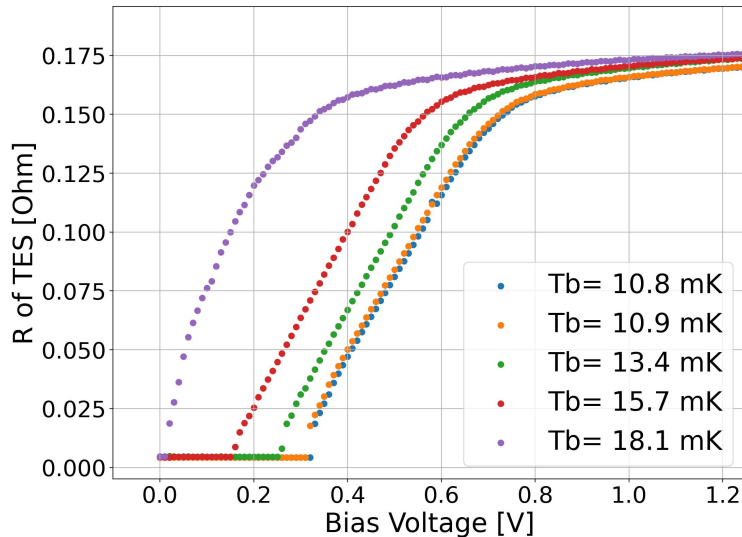
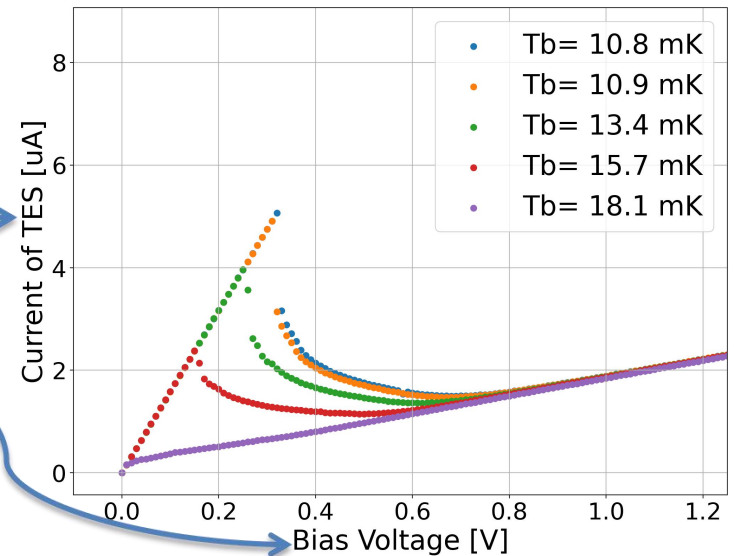
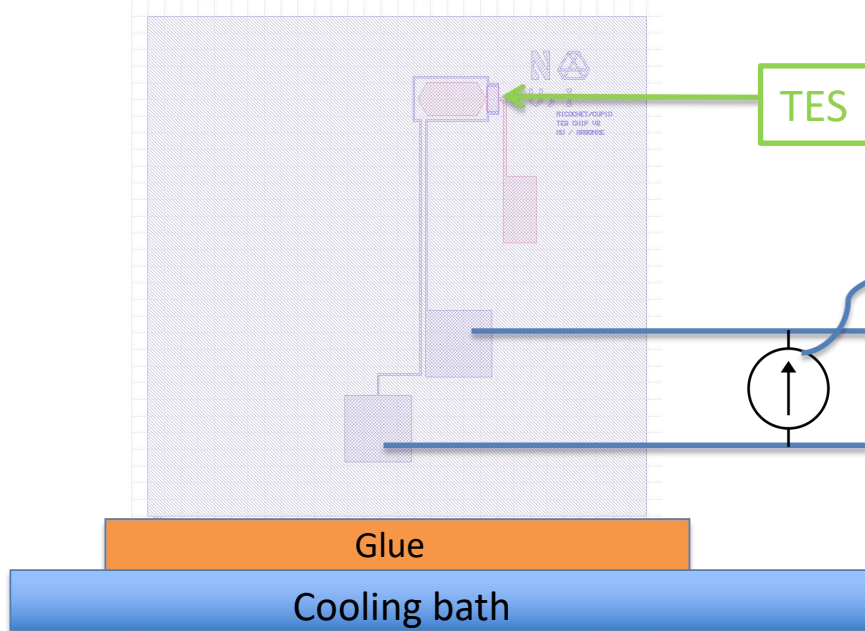


- Al/Mn TES with tunable  $T_c$  fabricated at Argonne National Laboratory
- More than 1000 chips from a single wafer
- Easy to change design and re-fabrication
- Already got a whole wafer.

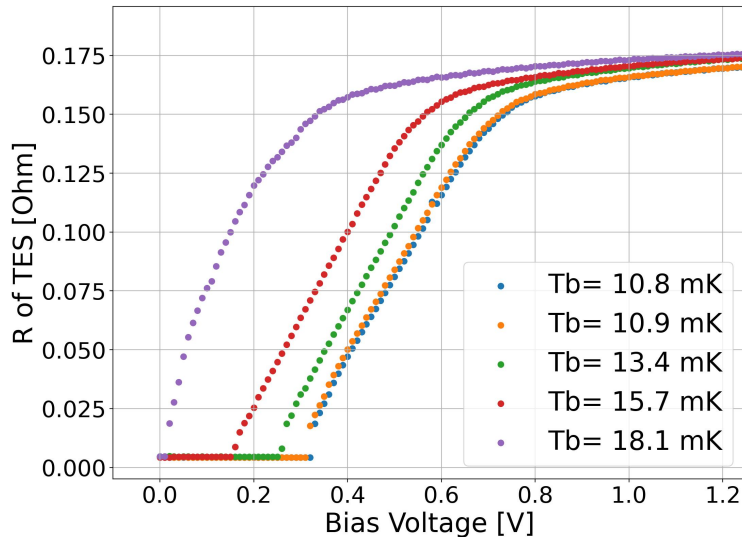
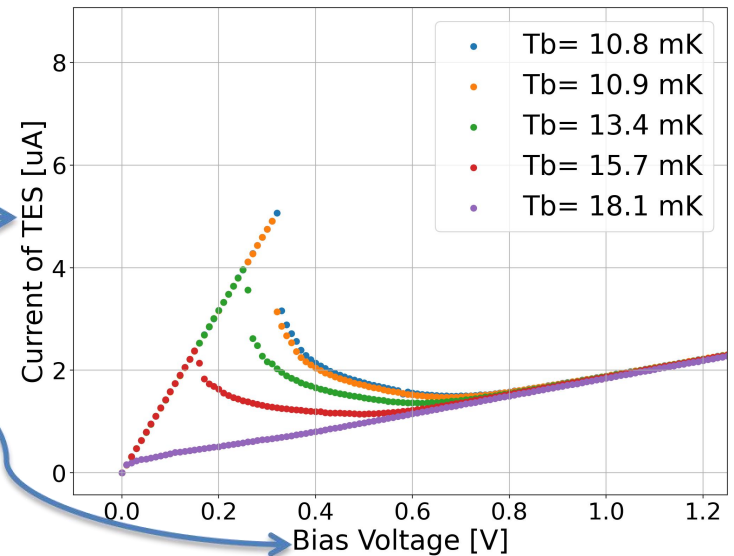
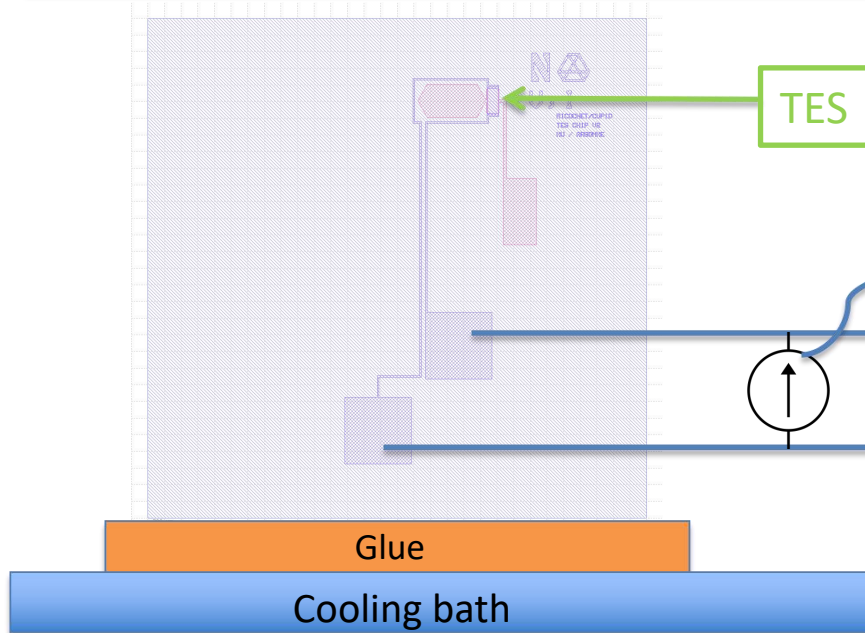


A 6-inch test wafer





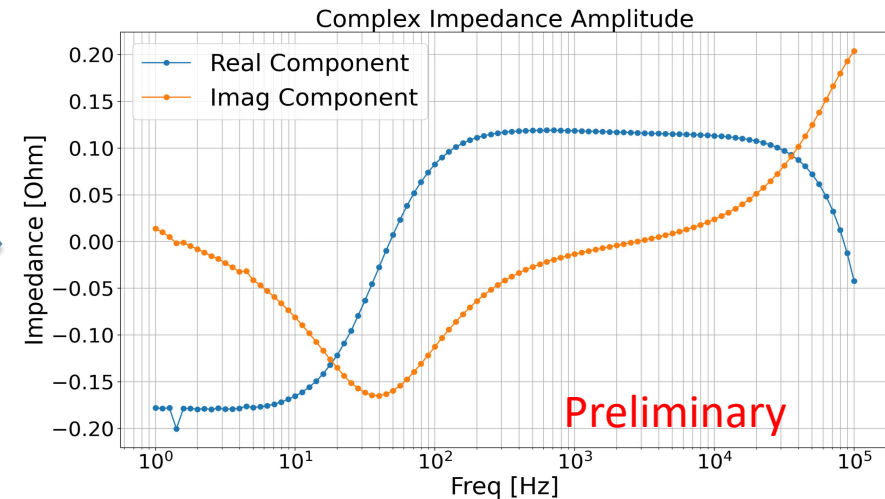
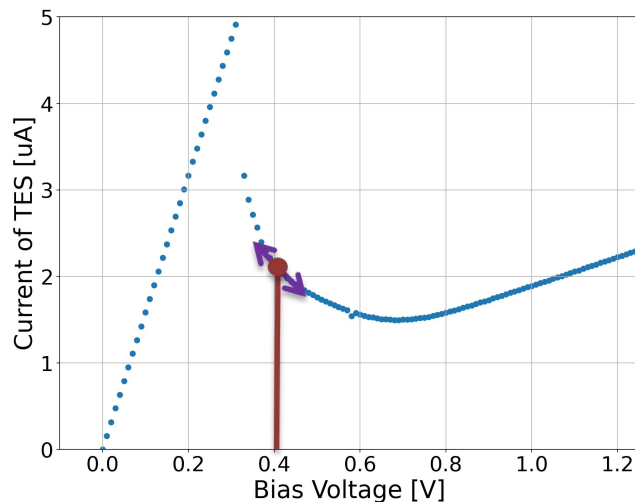
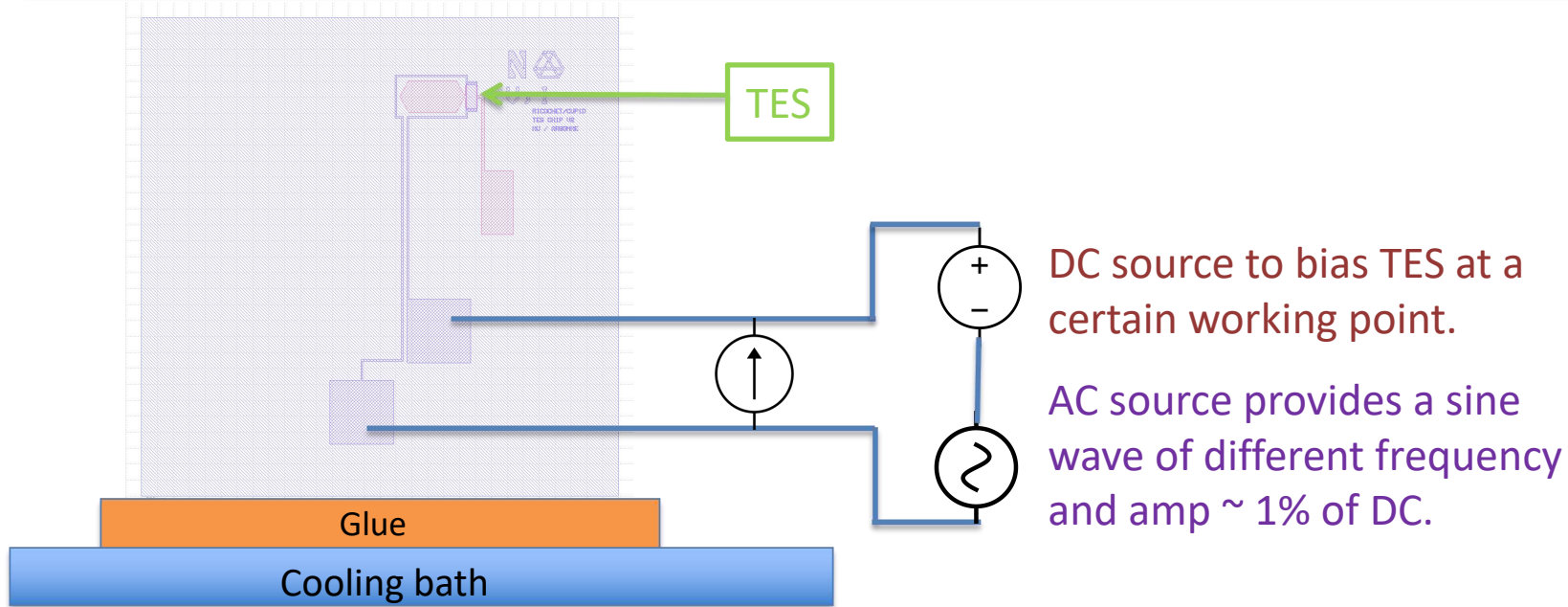
- Understanding the TES parameters is one of the first steps in understanding the full detector performance.
- To measure TES parameters, we attached a TES chip to the cooling bath without any target.
- IV curves are usually the first measurement made in characterizing a TES.
- Measured  $T_c$  is  $\sim 20$  mK for this wafer.



- Understanding the TES parameters is one of the first steps in understanding the full detector performance.
- To measure TES parameters, we attached a TES chip to the cooling bath without any target.
- IV curves are usually the first measurement made in characterizing a TES.
- IV curve tells us the static response.

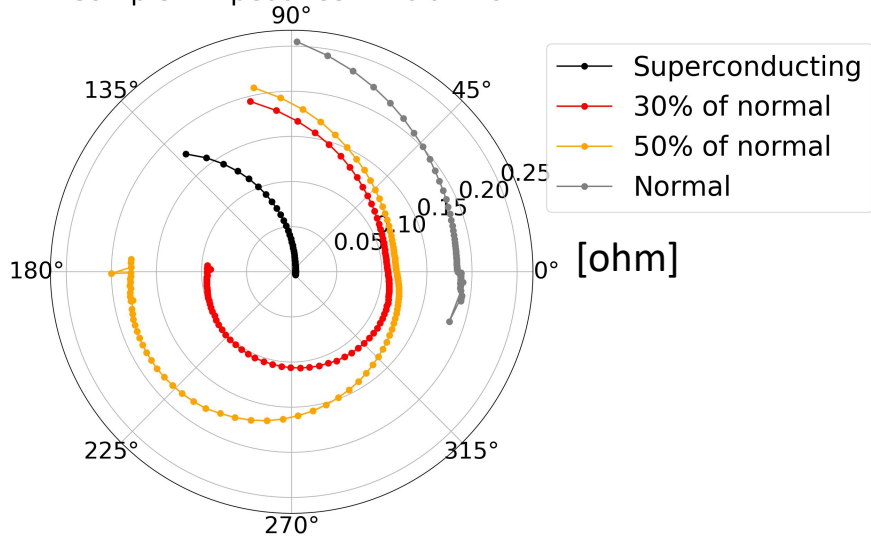
Furthermore, we want the dynamic response!

# Complex Impedance of TES chip

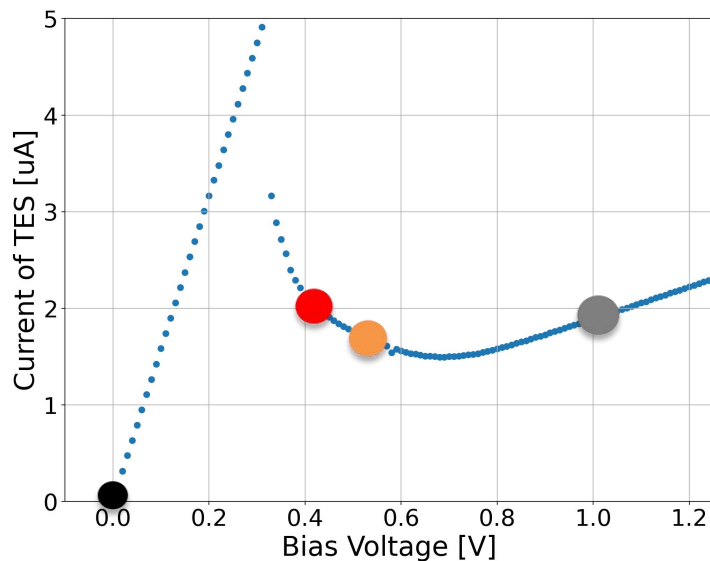




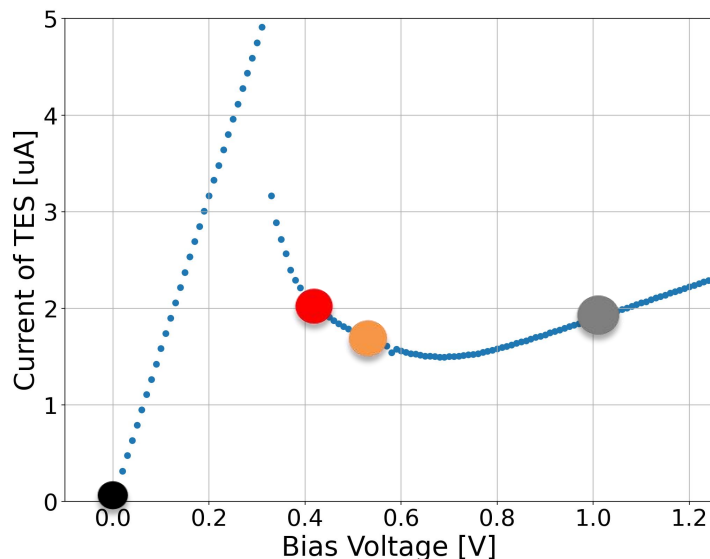
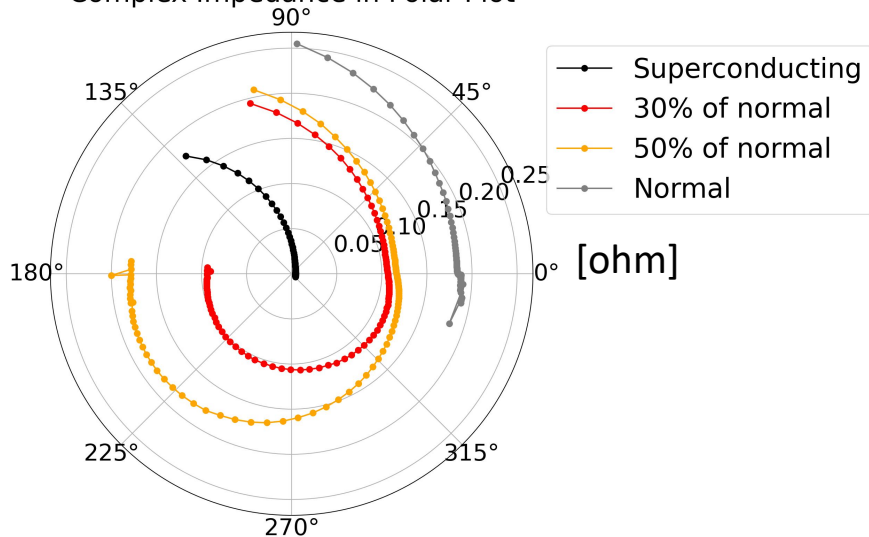
Complex Impedance in Polar Plot



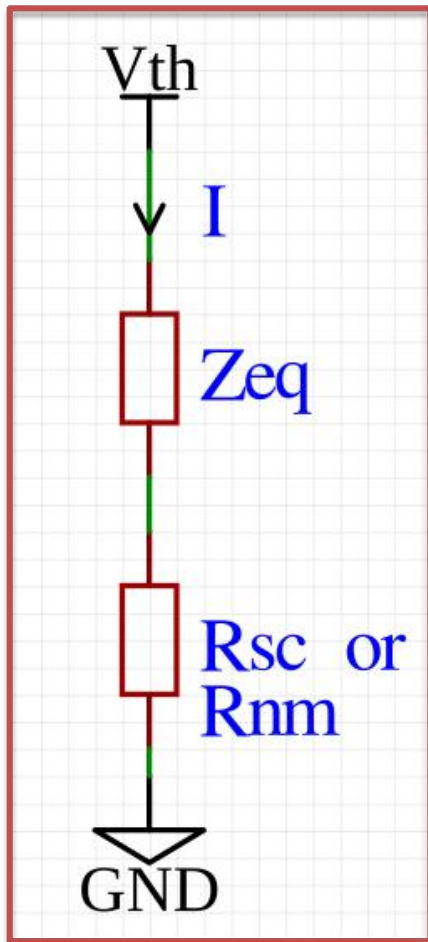
- Repeat the same measurement at different bias point:
  - 30%: Resistance of TES is  $\sim 30\%$  of normal resistance
  - 50%: Resistance of TES is  $\sim 50\%$  of normal resistance



Complex Impedance in Polar Plot



- Repeat the same measurement at different bias point:
  - 30%: Resistance of TES is  $\sim$  30% of normal resistance
  - 50%: Resistance of TES is  $\sim$  50% of normal resistance
- This still contains the impedance of the bias circuit!
- Superconducting and normal results are used to characterize the bias circuit.
  - Superconducting: No bias voltage
  - Normal: Apply large bias so that TES is totally normal.
  - When superconducting or normal, the TES is just a resistor and we know the resistance.

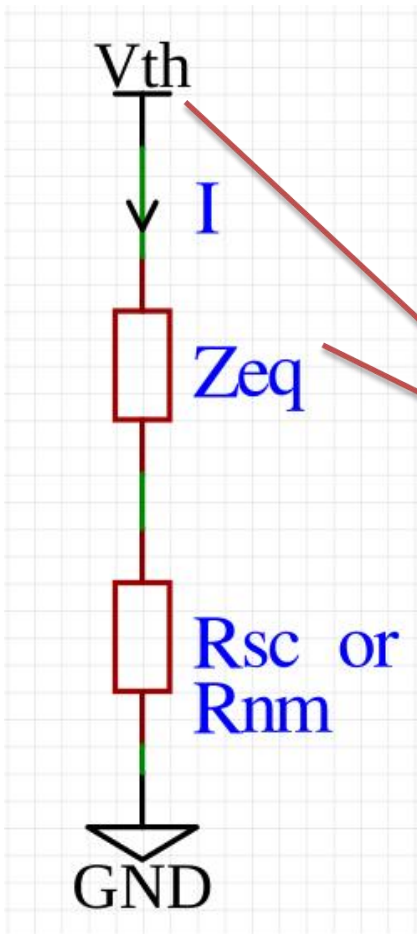


- Assume the bias circuit does not change with bias current:
- Thevenin equivalent of the bias circuit.
- $V_{th}$  and  $Z_{eq}$  represent the voltage and impedance of the bias circuit.

[1]: Impedance measurements and modeling of a transition-edge-sensor calorimeter.

M. A. Lindeman, et al.

<https://doi.org/10.1063/1.1711144>



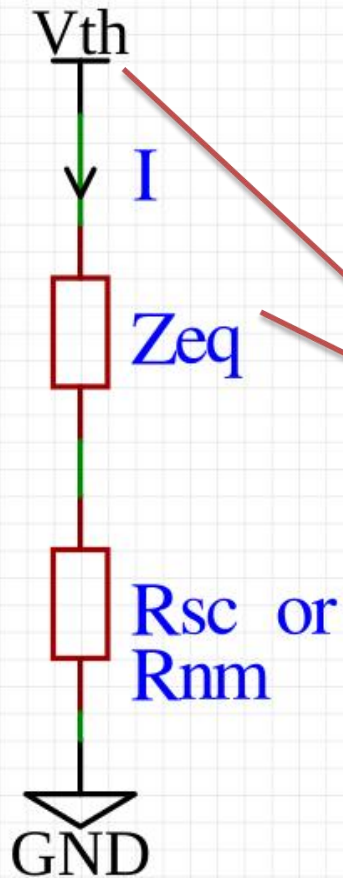
- Assume the bias circuit doesn't change with bias current:
  - Thevenin equivalent of the bias circuit.
  - $V_{th}$  and  $Z_{eq}$  represent the voltage and impedance of the bias circuit.
- Superconduction (SC) and normal (NM) response -->  $V_{th}(f)$  and  $Z_{eq}(f)$

$$I_{sc/nm}^{-1}(f) = \frac{R_{sc/nm}(f) + Z_{eq}(f)}{V_{th}(f)}$$

[1]: Impedance measurements and modeling of a transition-edge-sensor calorimeter.

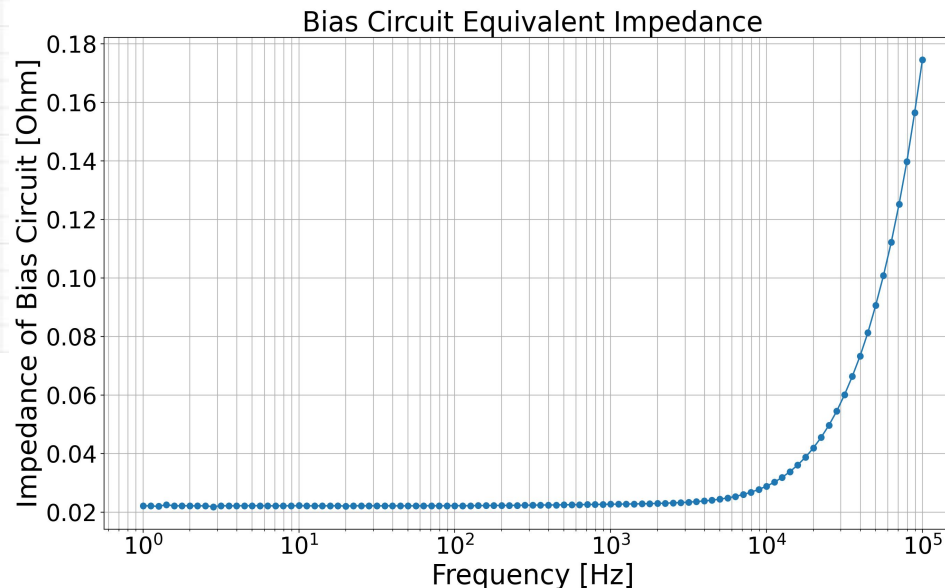
M. A. Lindeman, et al.

<https://doi.org/10.1063/1.1711144>



- Assume the bias circuit doesn't change with bias current:
  - Thevenin equivalent of the bias circuit.
  - $V_{th}$  and  $Z_{eq}$  represent the voltage and impedance of the bias circuit.
- SC and NM response  $\rightarrow V_{th}(f)$  and  $Z_{eq}(f)$

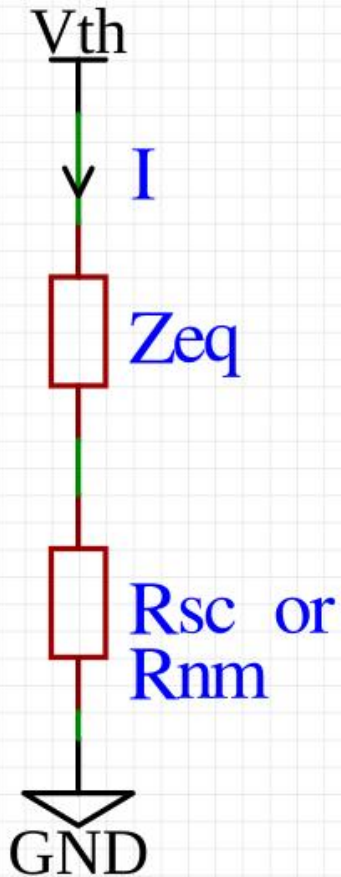
$$I_{sc/nm}^{-1}(f) = \frac{R_{sc/nm}(f) + Z_{eq}(f)}{V_{th}(f)}$$



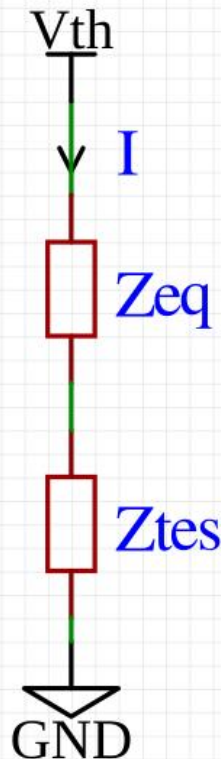
- The impedance of bias circuit is similar to a resistor + inductor.
- Match our expectation!

[1]: Impedance measurements and modeling of a transition-edge-sensor calorimeter.  
 M. A. Lindeman, et al.  
<https://doi.org/10.1063/1.1711144>





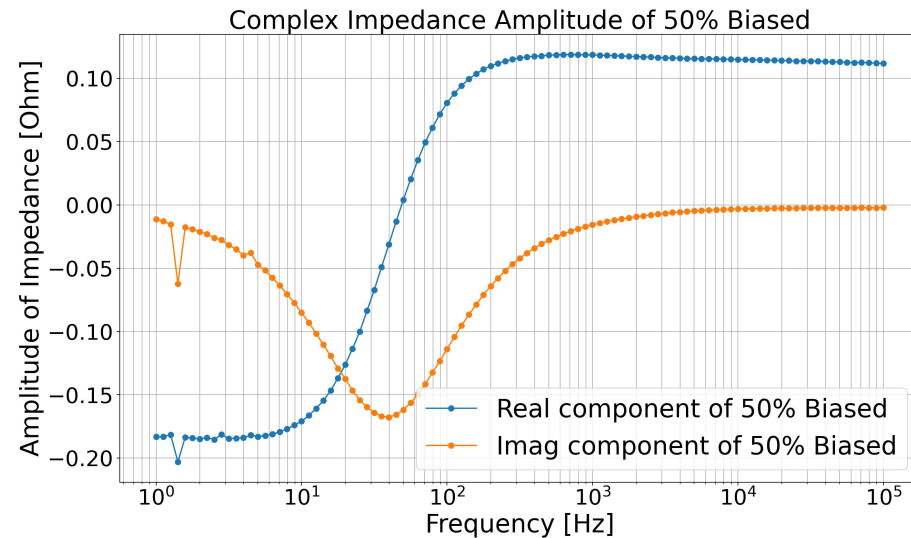
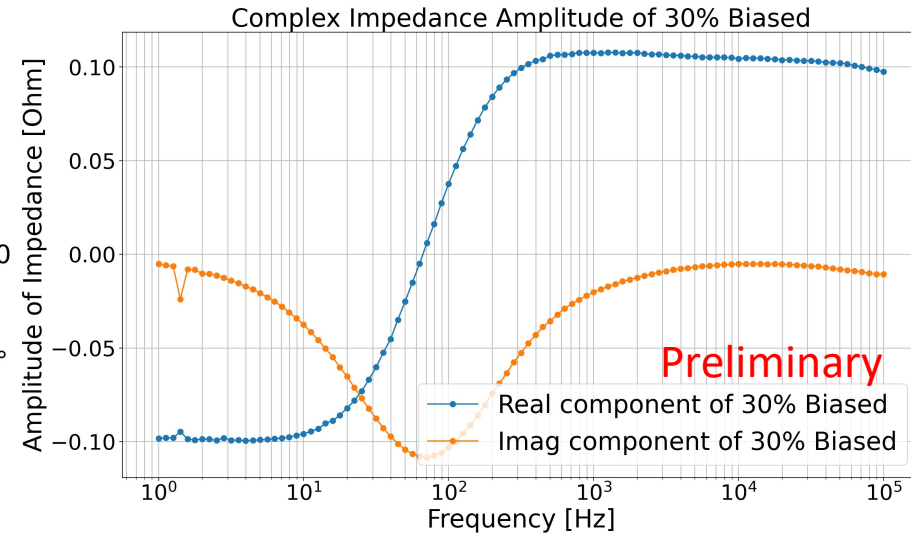
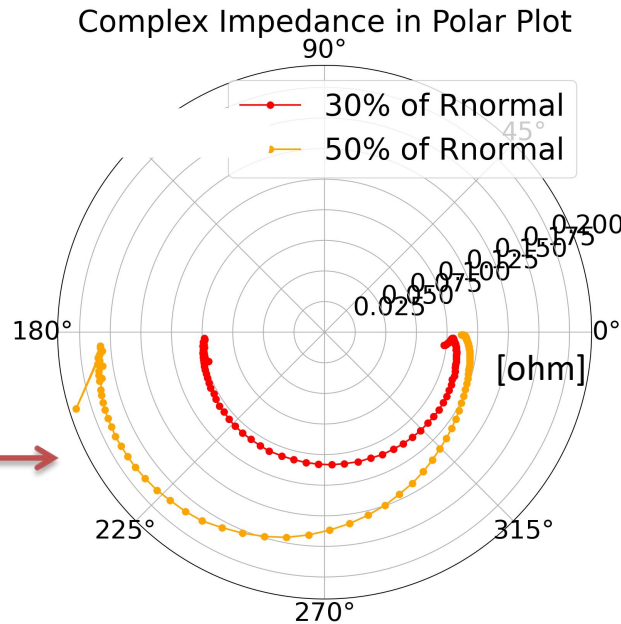
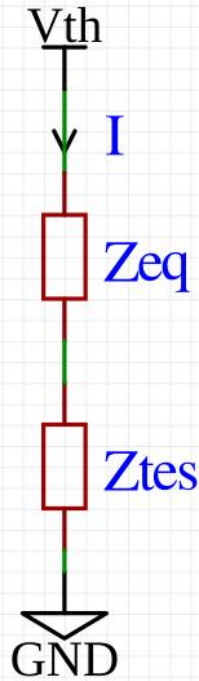
- Assume the bias circuit doesn't change with bias current:
  - Thevenin equivalent of the bias circuit.
  - $V_{th}$  and  $Z_{eq}$  represent the voltage and impedance of the bias circuit.
  - SC and NM response  $\rightarrow V_{th}(f)$  and  $Z_{eq}(f)$



- $$Z_{tes}(f, I_{bias}) = \frac{V_{th}(f)}{I(f, I_{bias})} - Z_{eq}(f)$$
- 30% and 50% response,  $V_{th}(f)$  and  $Z_{eq}(f)$   $\rightarrow Z_{tes}$

[1]: Impedance measurements and modeling of a transition-edge-sensor calorimeter.  
 M. A. Lindeman, et al.  
<https://doi.org/10.1063/1.1711144>

# Complex Impedance of TES chip



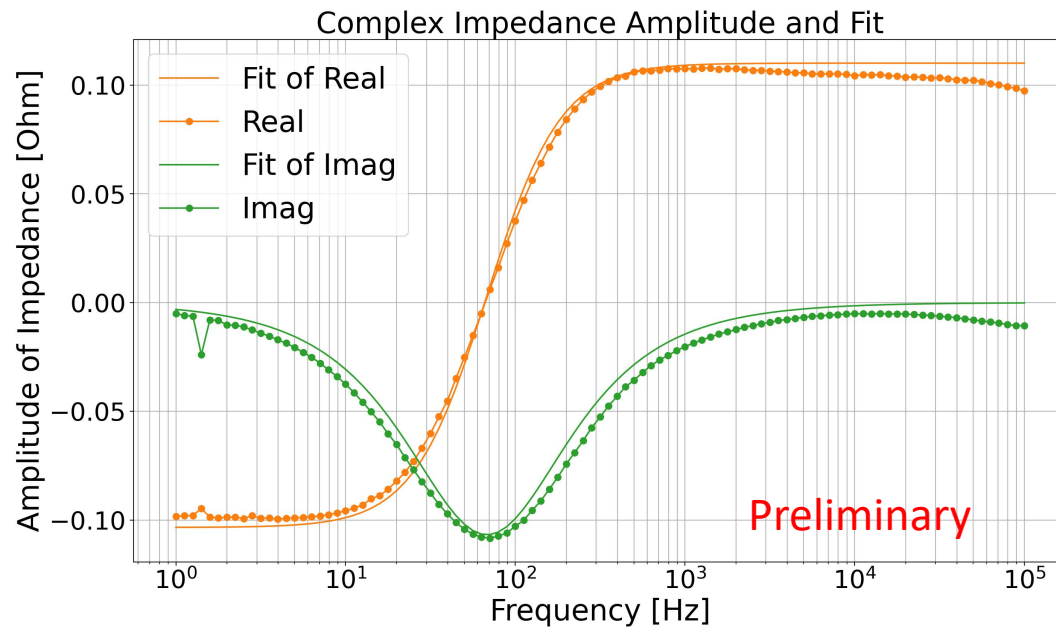
# Model for Complex Impedance of TES

- Model:  $Z_{\text{tes}}(f) = R_0 \frac{(1+\beta)(1+i2\pi f\tau)+\mathcal{L}}{1-\mathcal{L}+2i\pi f\tau}$  [1]
- $R_0$  is the resistance of TES at biased point. Depends on how TES biased.
- $\beta = \frac{I_0}{R_0} \left. \frac{\partial R}{\partial I} \right|_{T_0}$  is the current sensitivity of the TES.
- $\mathcal{L} = \frac{\alpha}{n} (1 - (\frac{T_b}{T_c})^n)$  Loop Gain.  $n=5$  determined by the coupling type.
  - $\alpha = \frac{T_0}{R_0} \left. \frac{\partial R}{\partial T} \right|_{T_0}$  is the temperature sensitivity of the TES.
- $\tau = \frac{C_{\text{TES+Au}}}{G_{\text{TES+Au}}}$  time constant of the TES.

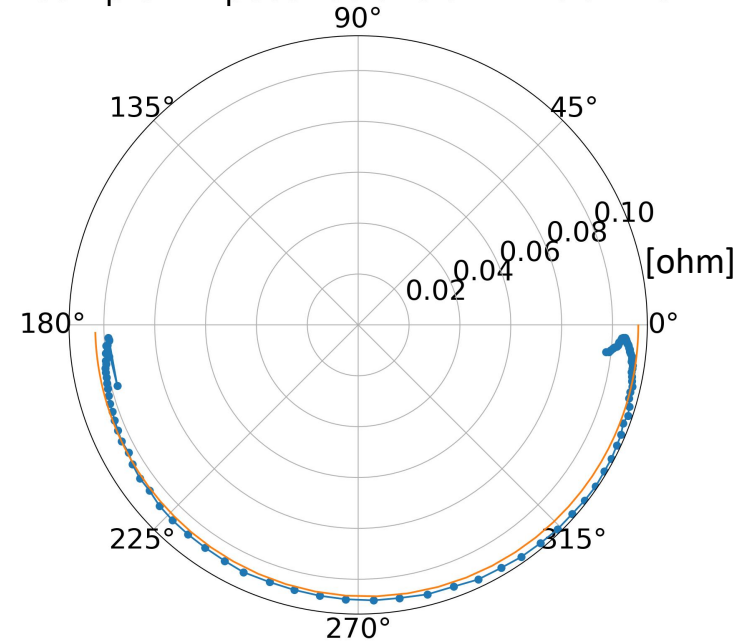
**What  
used to  
fit**

[1]: Complex impedance of a transition-edge sensor with sub- $\mu\text{s}$  time constant  
<https://doi.org/10.1063/1.5127100>

# Fit Results for 30% Bias TES



Complex Impedance and Fit in Polar Plot



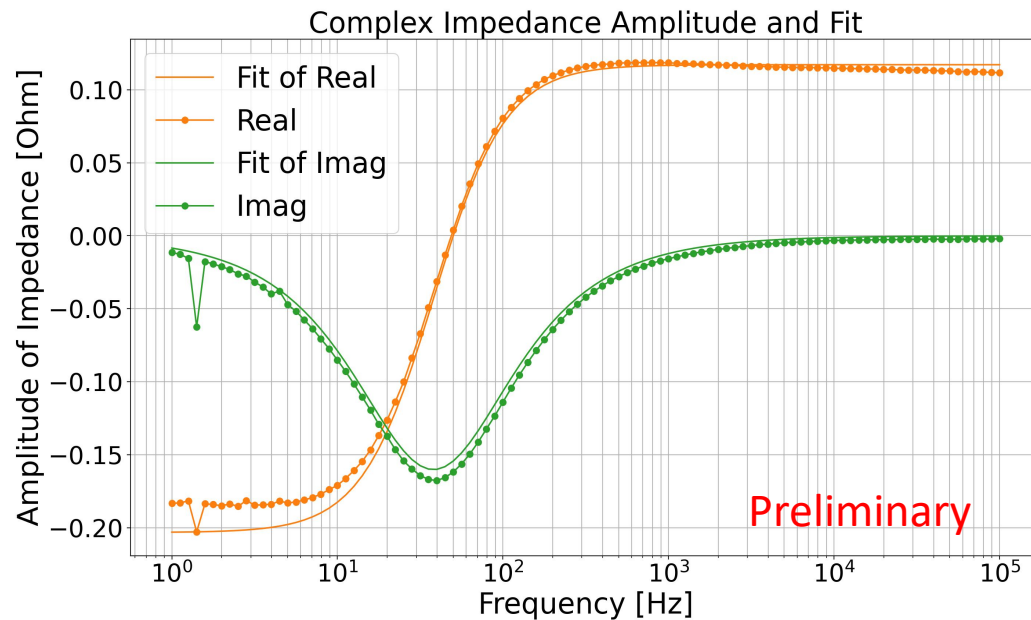
$$\mathcal{L} = 4.4 \pm 0.3$$

$$\beta = 0.92 \pm 0.03$$

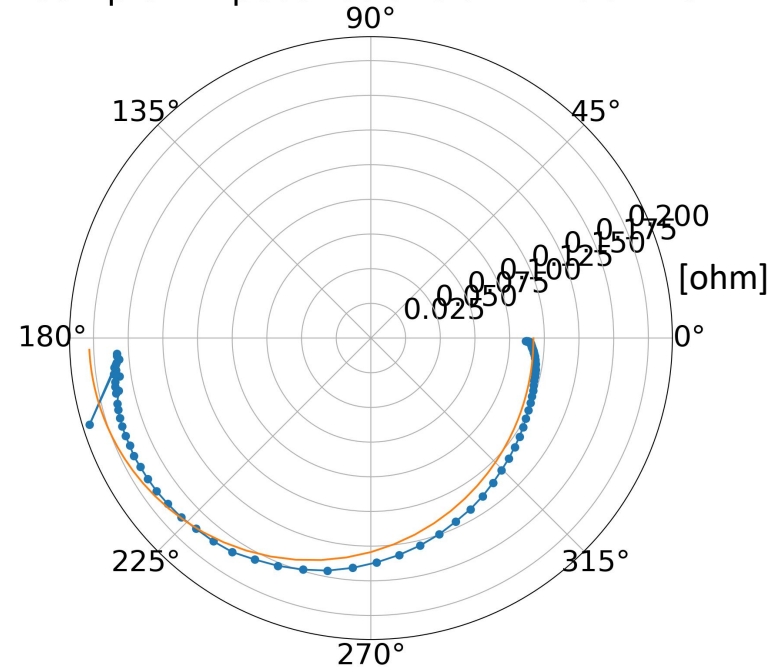
$$\tau = 8.0 \pm 0.6 \text{ ms}$$

- $R_n = 185 \text{ mOhm}$
- TES bias @ 30 % of  $R_n$
- $\alpha$  estimated by  $\mathcal{L}$  : 24

# Fit Results for 50% Bias TES



Complex Impedance and Fit in Polar Plot



$$\mathcal{L} = 2.17 \pm 0.03$$

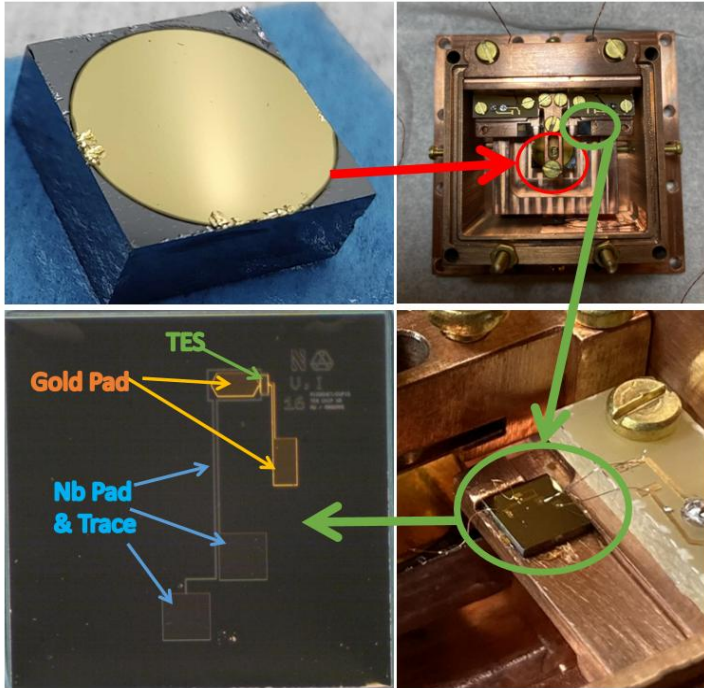
$$\beta = 1.10 \pm 0.01$$

$$\tau = 4.9 \pm 0.1 \text{ ms}$$

- $R_n = 185 \text{ mOhm}$
- TES bias @ 50 % of  $R_n$
- $\alpha$  estimated by  $\mathcal{L}$  : 12

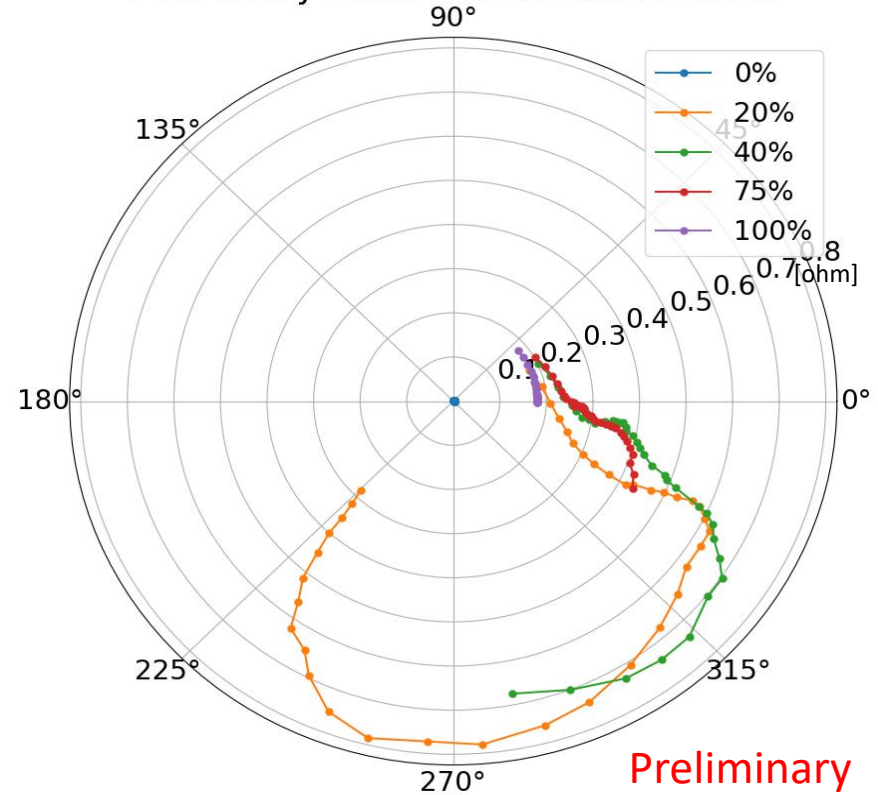


# Next Steps

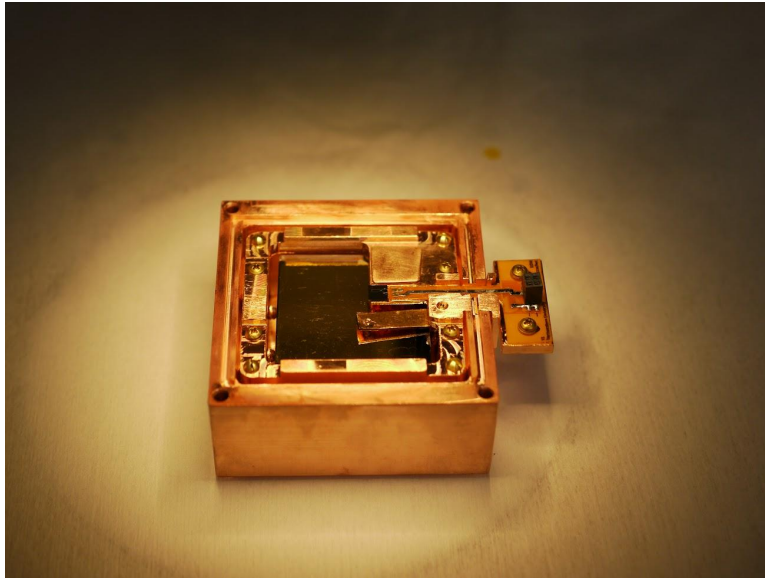


- A detector with 1 gram Silicon target has been built up at UMass Amherst
- The complex impedance measurement is ongoing!

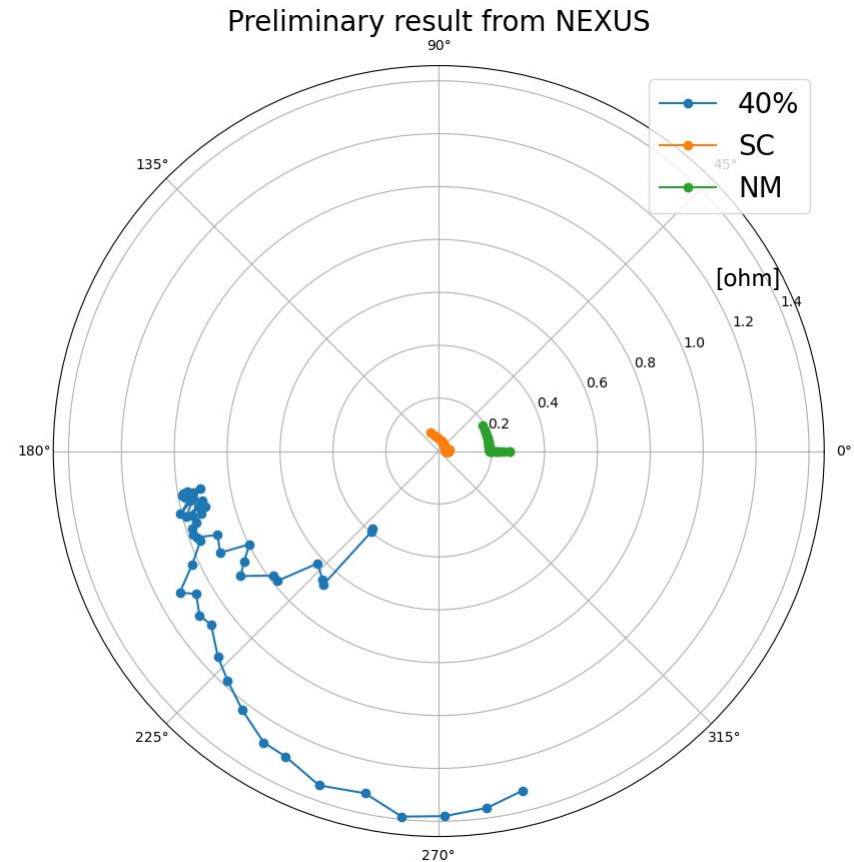
Preliminary result from UMass Amherst

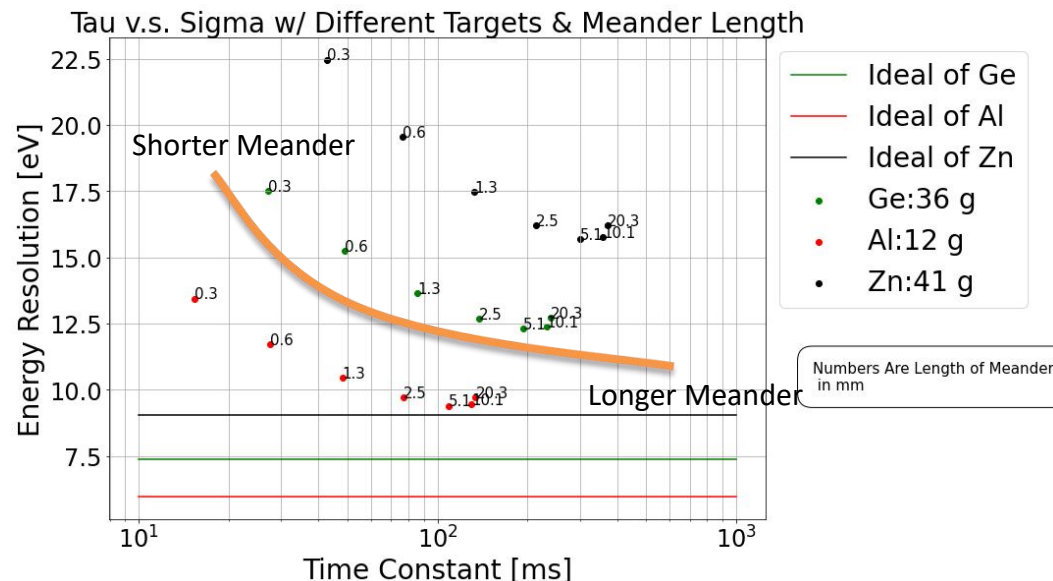
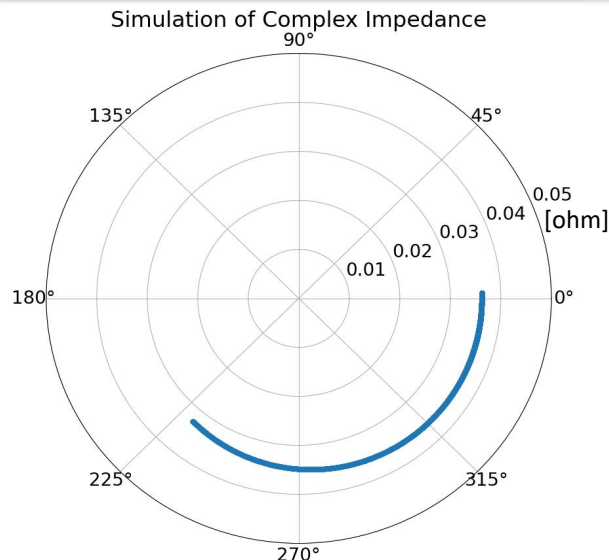


- More info will be presented on Dec 1, 2022, 11:15 AM ET by Luke Chaplinsky



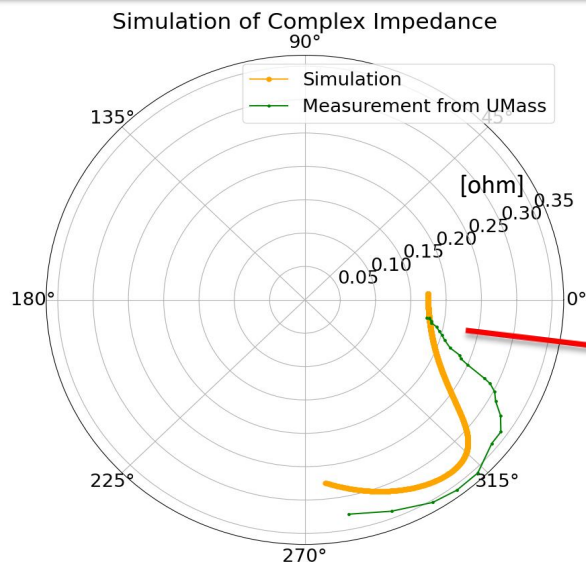
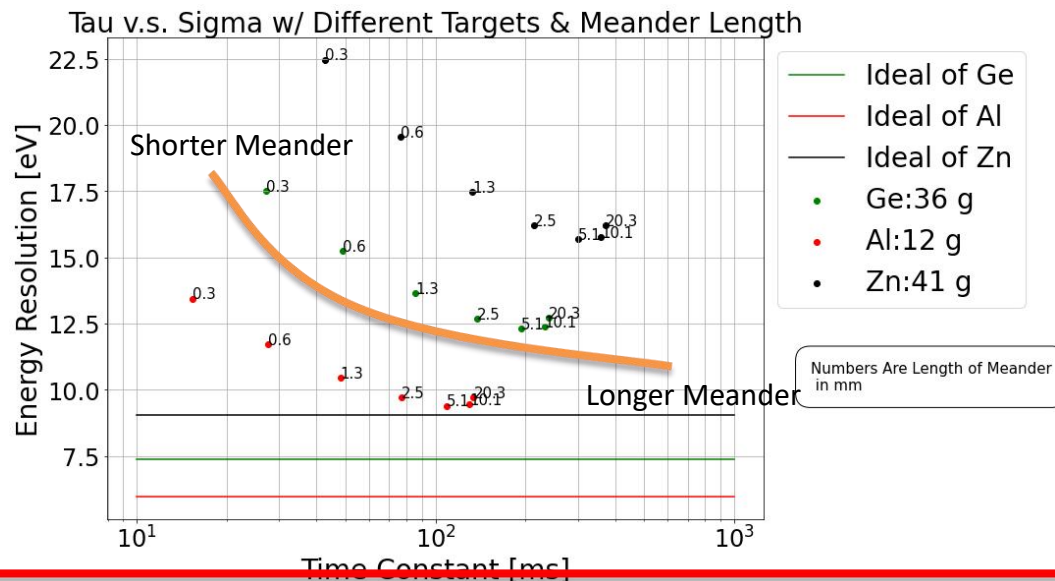
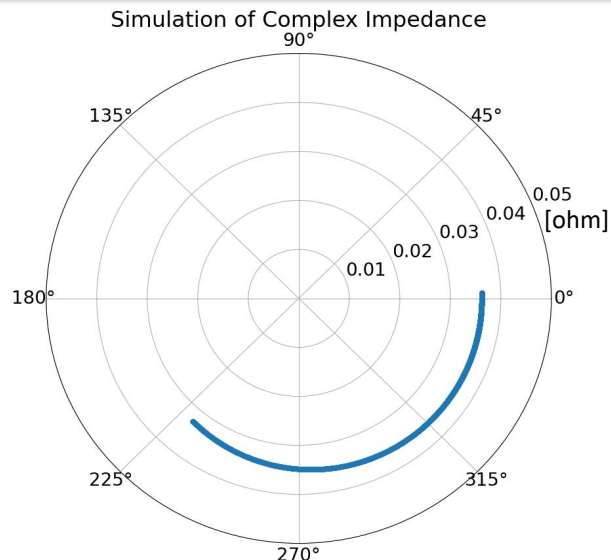
- A detector with 36 gram Germanium target is installed at NEXUS (Northwestern EXperimental Underground Site) of Fermi National Laboratory.
- The complex impedance measurement is also on going!





- In our previous simulation [1], some parameters were assumed from other kinds of TES detectors:
  - $\alpha = 100$ ,  $\beta = 1$
- Using these parameters, the simulation behaves as a semi-circle on the complex plane which does not match our measurement at UMass.

[1]: Transition Edge Sensor Chip Design of Modular CEvNS Detector for the Ricochet Experiment  
 R. Chen, et al.  
<https://arxiv.org/abs/2111.05757>



- Improving the simulation by adding parameters measured from the Al/Mn TES chip.
- Our model can now produce similar complex impedance curves!
- Fitting UMass measurements using new TES parameters underway.
- A better model of Ricochet detectors will come out!

Q&A