

LBNL update: air cooling studies, beam pipe bake-out

Nicole Apadula

EICSC Meeting

Feb 28, 2023

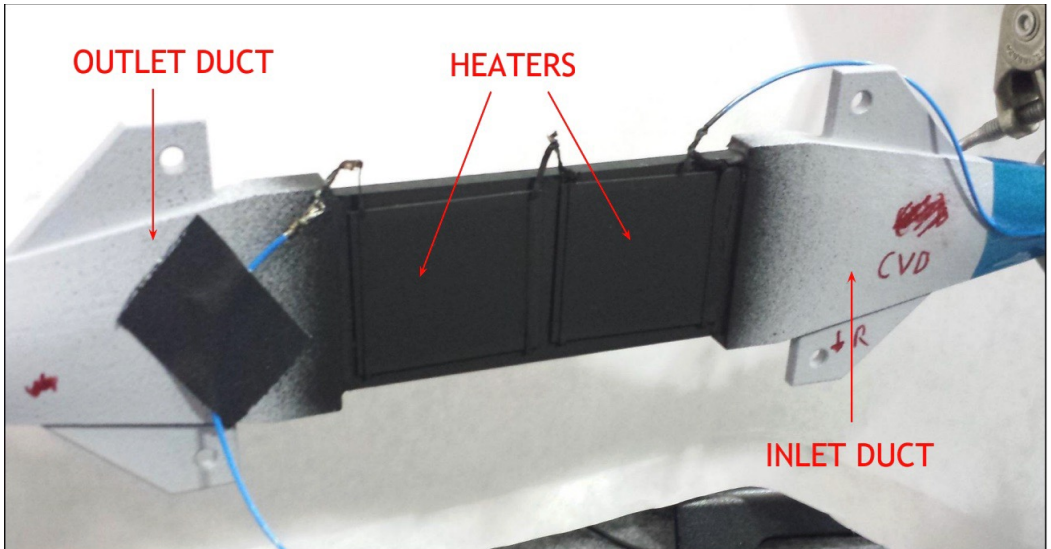
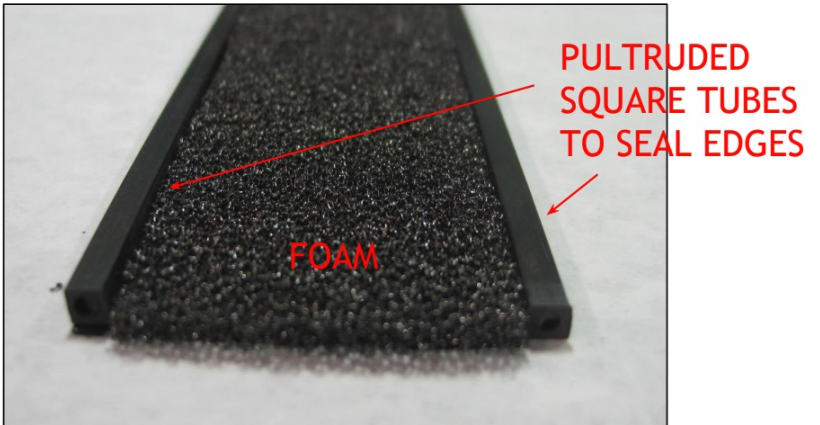
Outline

- Internal air cooling project started summer 2022
 - Previous talk: [EICSC Meeting 10/10/22](#)
- Beam pipe bake-out studies
 - Previous talk from Brian Eng: [EICSC Meeting 6/6/22](#)
 - 5 mm gap between beam pipe and 1st silicon layer

eRD111 air cooling project

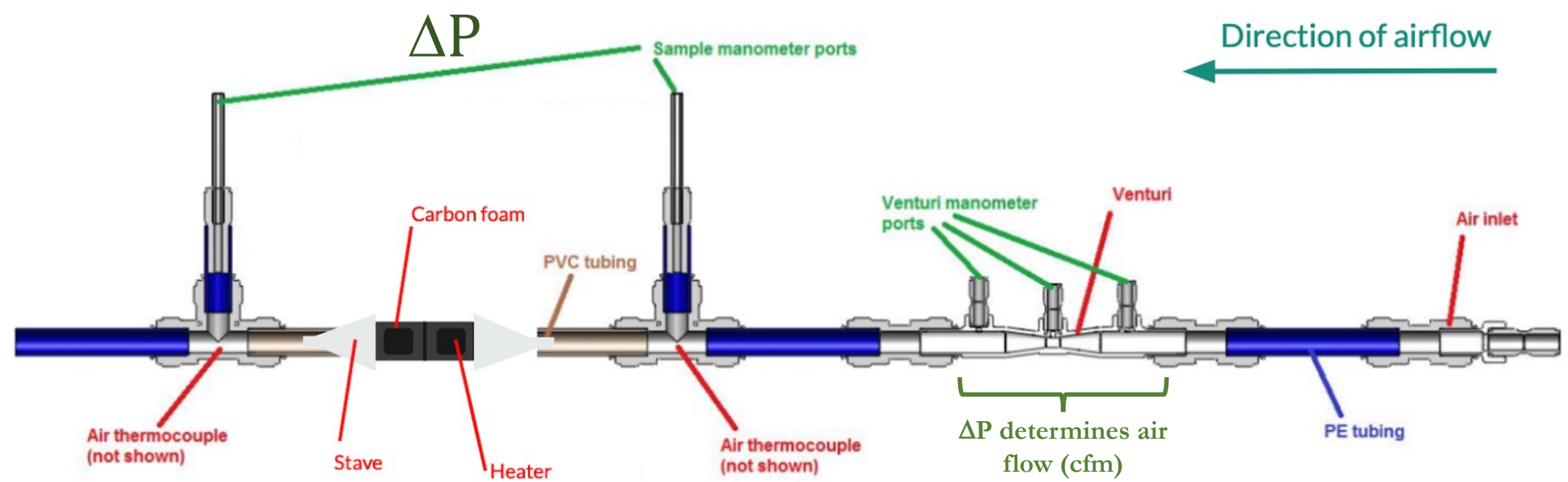
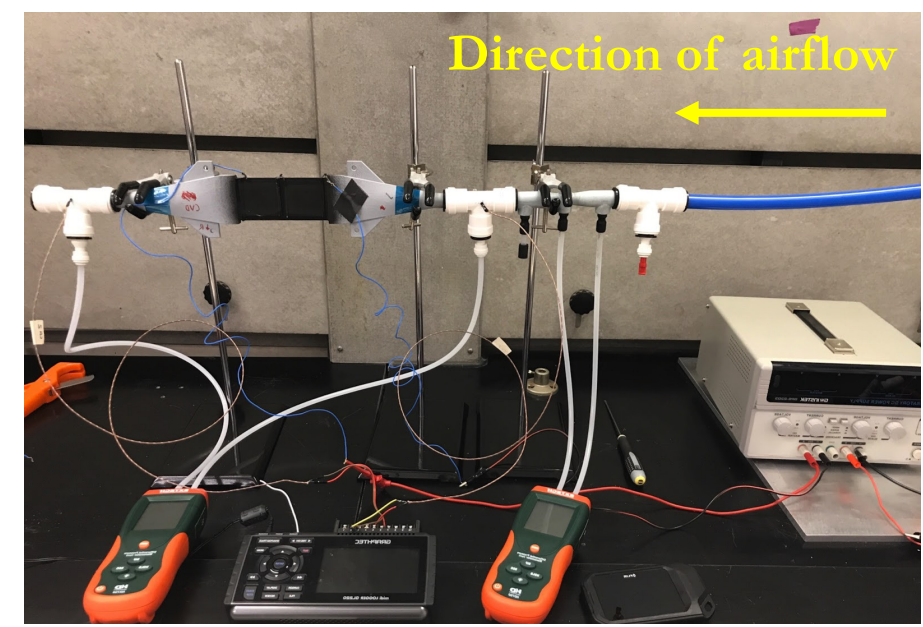
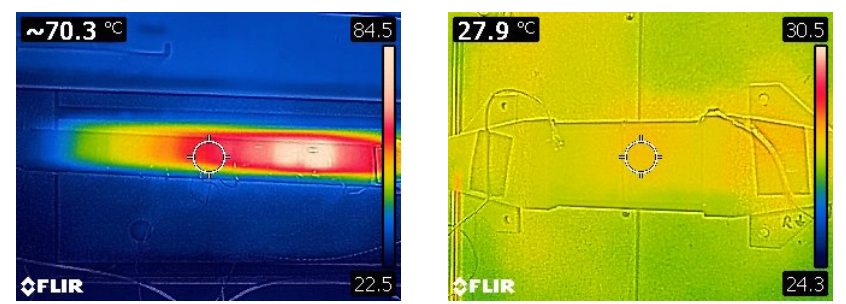
Currently led by
 Beatrice Liang-Gilman
 (blianggilman@lbl.gov)

- Is internal air cooling a viable option?
 - Periphery: 1 - 2 W/cm²
 - Matrix: ~10 mW/cm²
- Is design stable enough to withstand air?
- Goal: find option with optimized temperature & pressure differences
- Adjustable:
 - Power density
 - Foam types
 - Foam thicknesses
 - Air speed



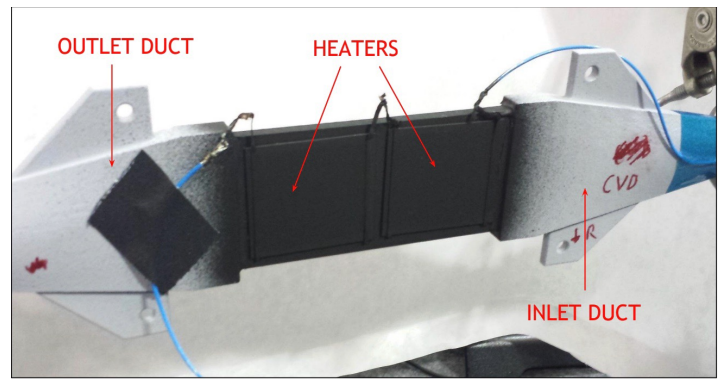
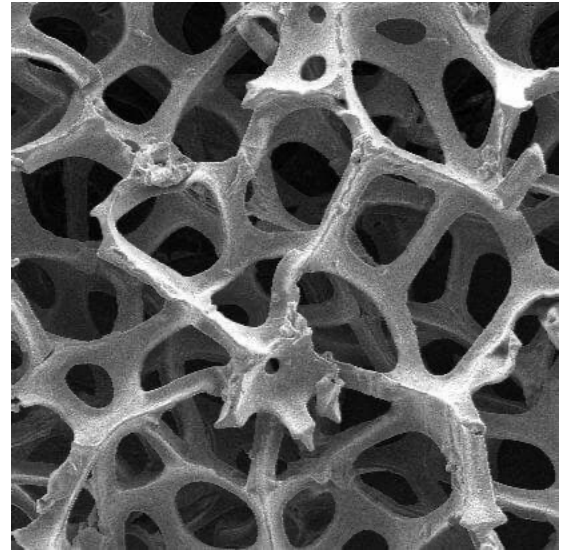
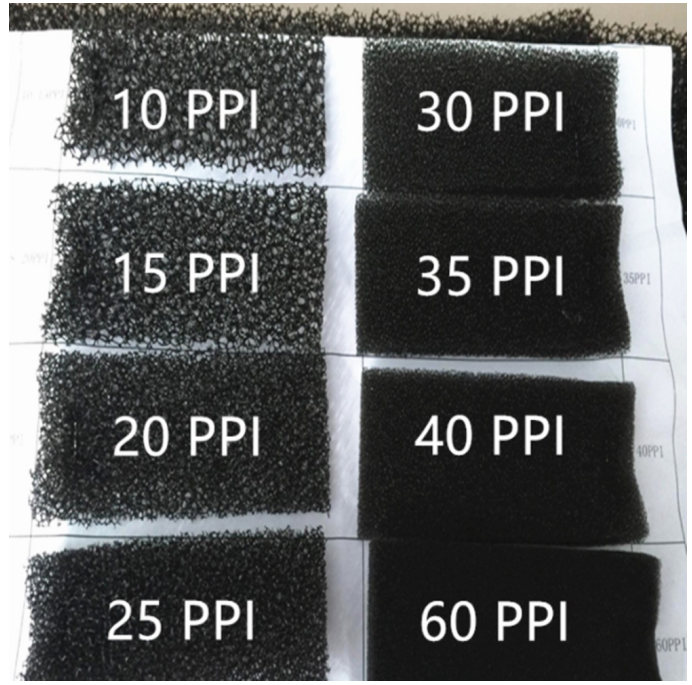
Setup

ΔT : "bright" temp – "dark" temp



Stave variations

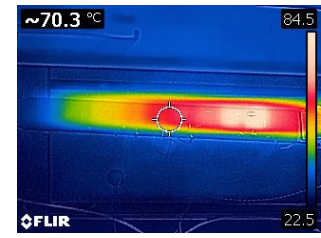
- Foam types:
 - CVD – conducting, denser than RVC
 - RVC – insulating, lower material budget
- Thicknesses: 4 & 6 mm
- PPI(pores per inch): 30 & 45
- Stave lengths: 100 & 500 mm



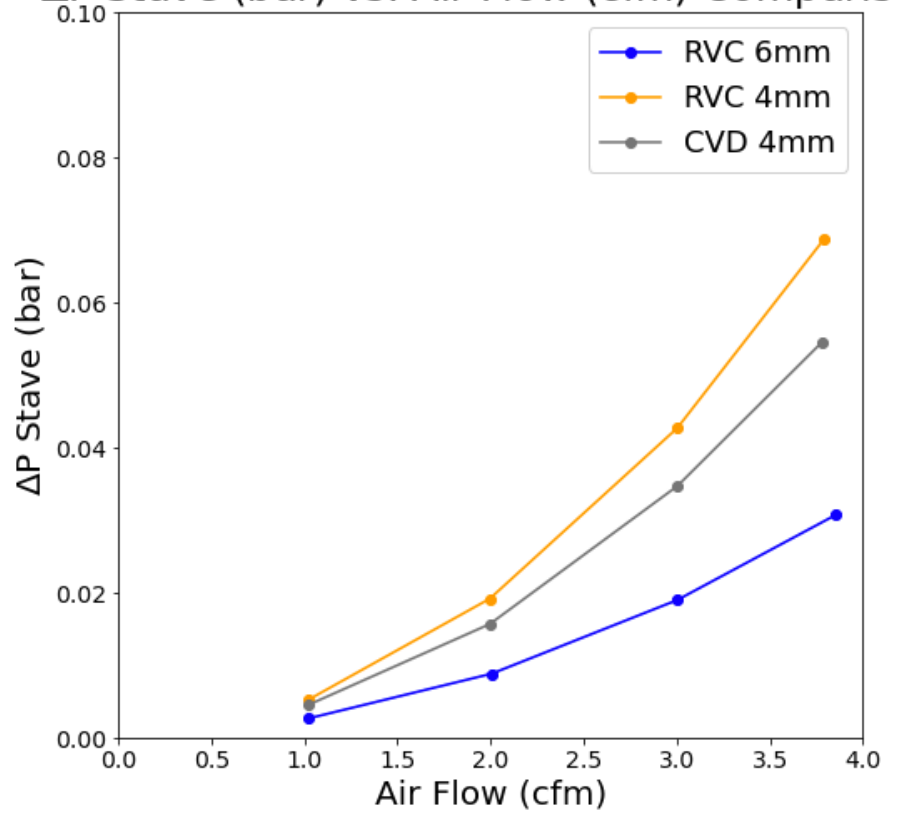
ΔT & ΔP results

ΔT : “bright” temp – “dark” temp

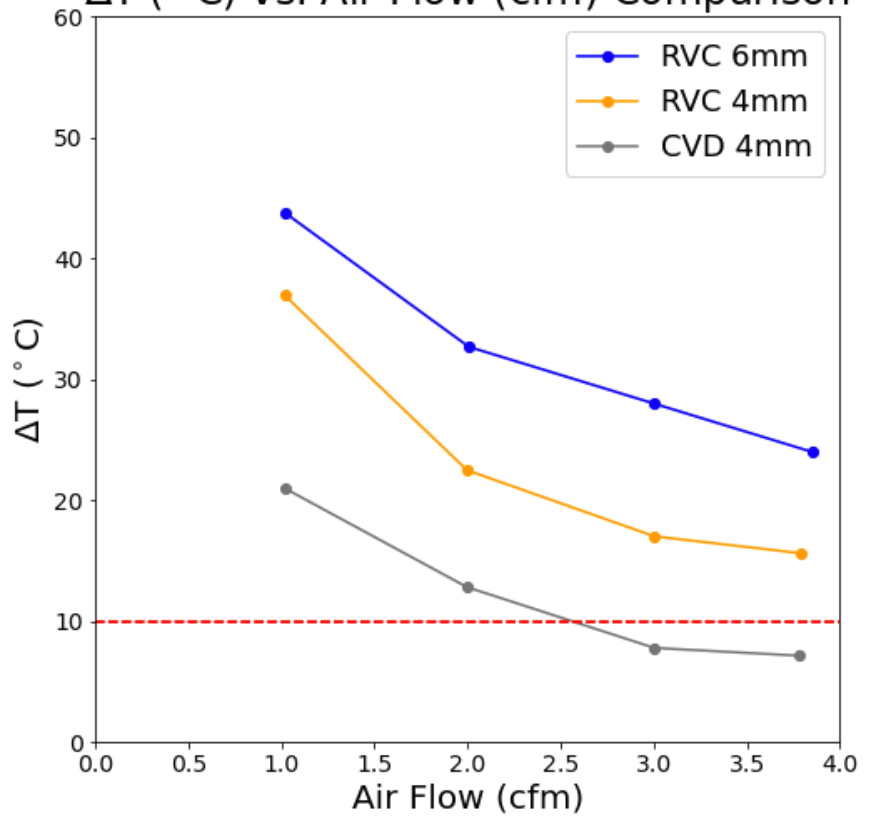
Power density = 0.5 W/cm^2



ΔP Stave (bar) vs. Air Flow (cfm) Comparison



ΔT (°C) vs. Air Flow (cfm) Comparison



Aim:

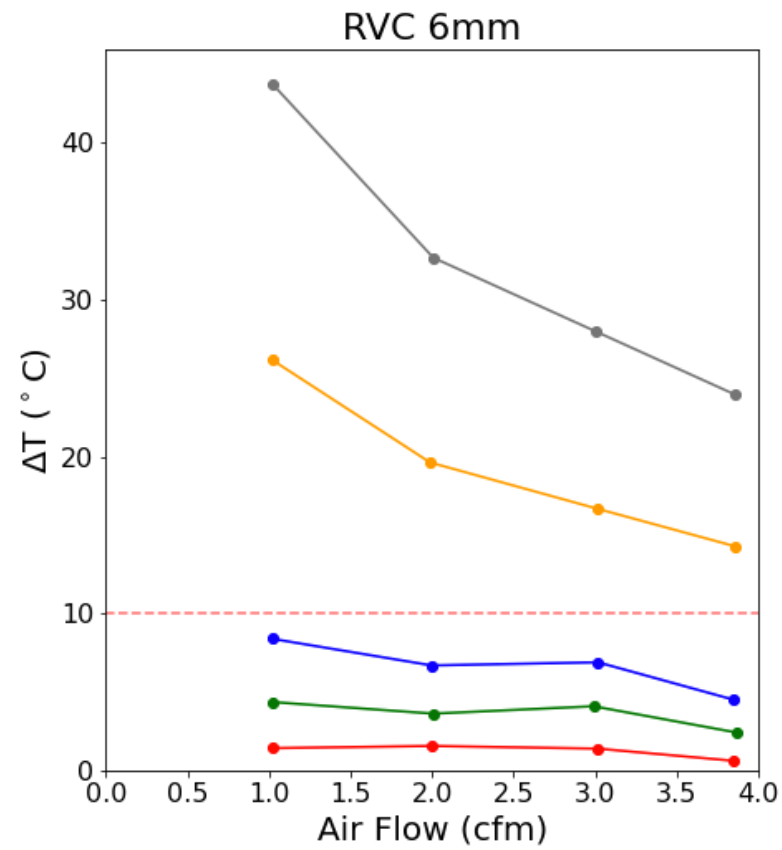
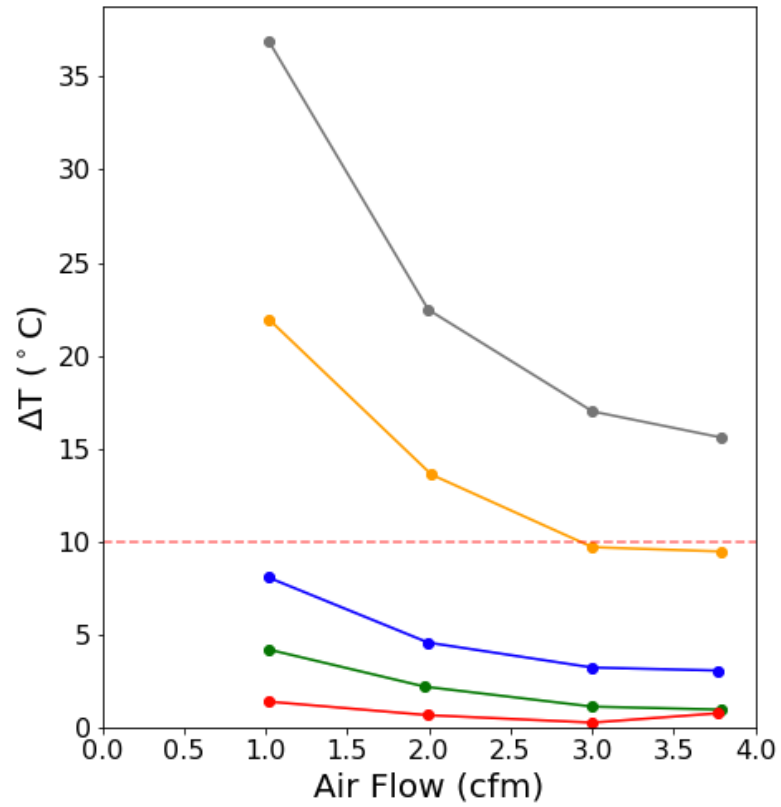
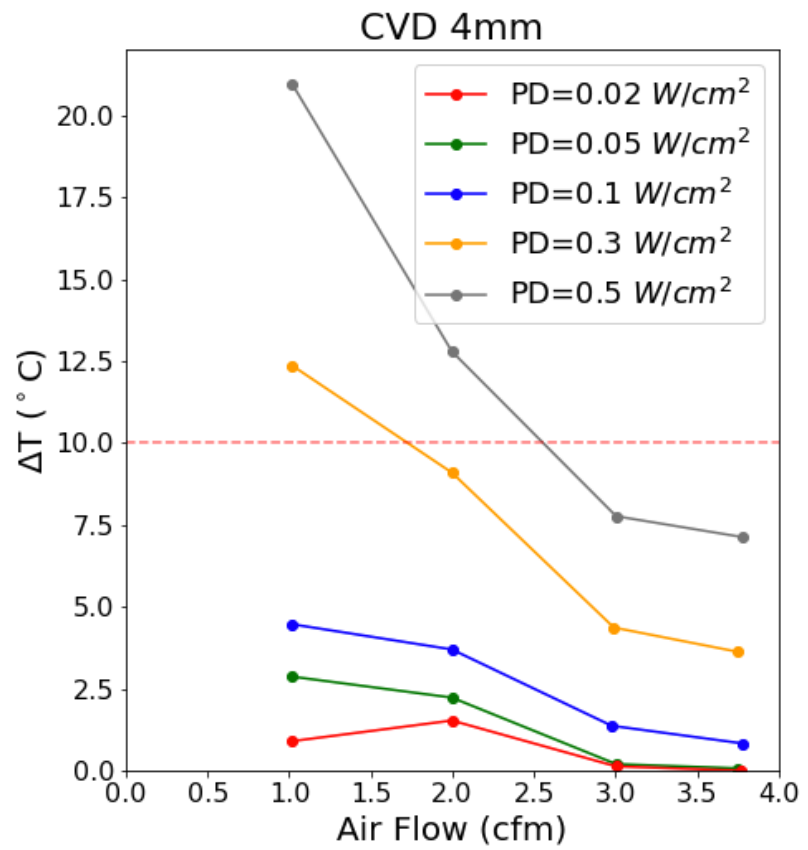
- $\Delta T < 10^\circ\text{C}$
- $\Delta P < 1 \text{ bar}$ for 1m stave

CVD meets both requirements

ΔT for different power densities

CVD achieves ΔT for all power densities

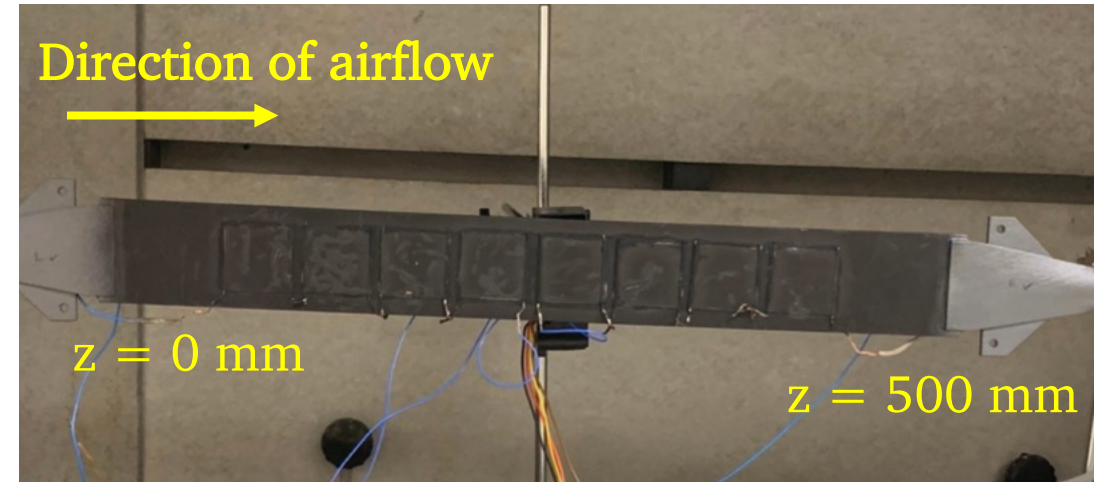
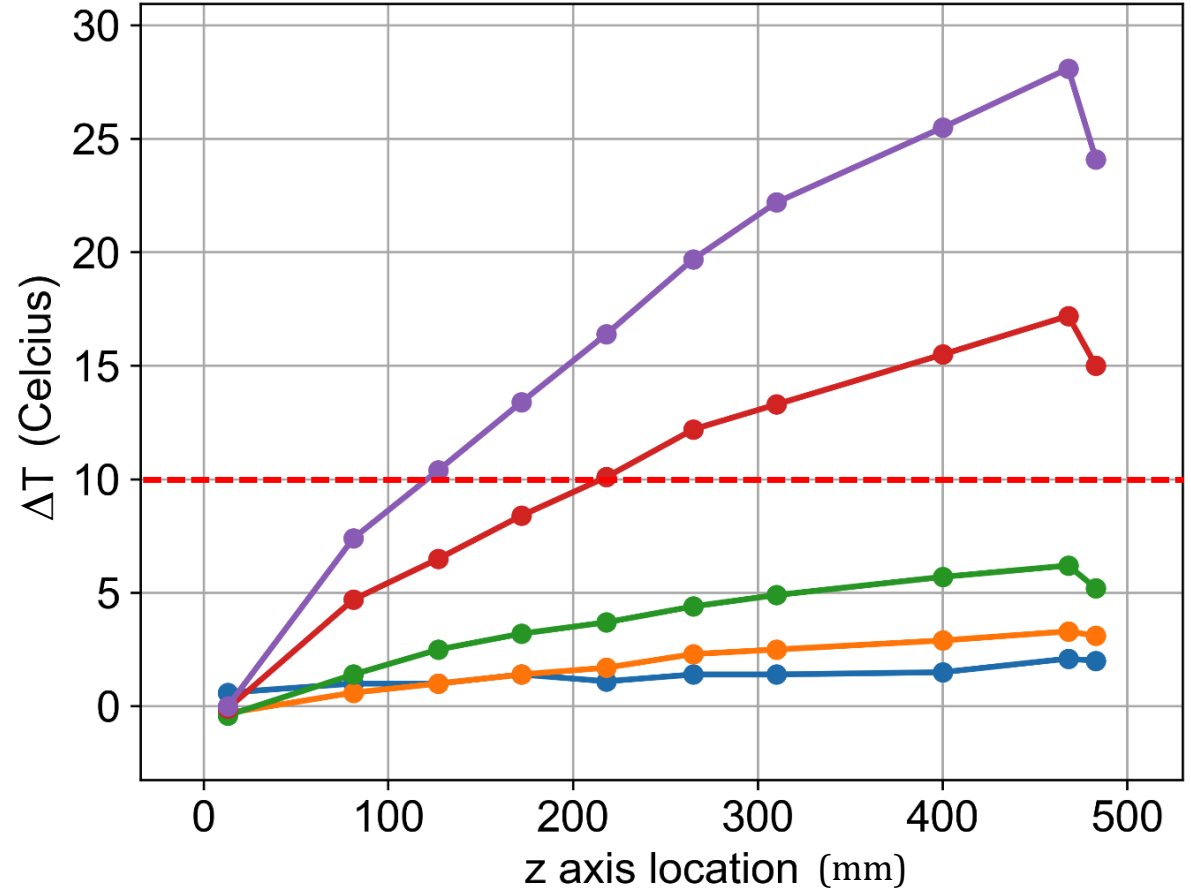
ΔT (°C) vs. Air Flow (cfm) Comparison



Pixel matrix < 0.02 W/cm², periphery > 0.5 W/cm²

Heat gradient

Heat gradient across long RVC stave
 $L = 50$ cm, air flow = 3.4 cfm

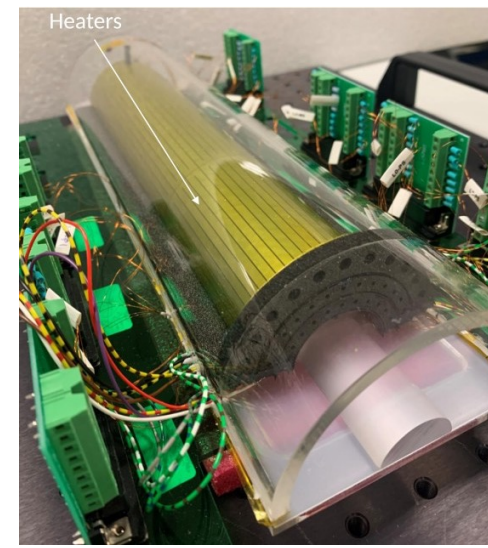
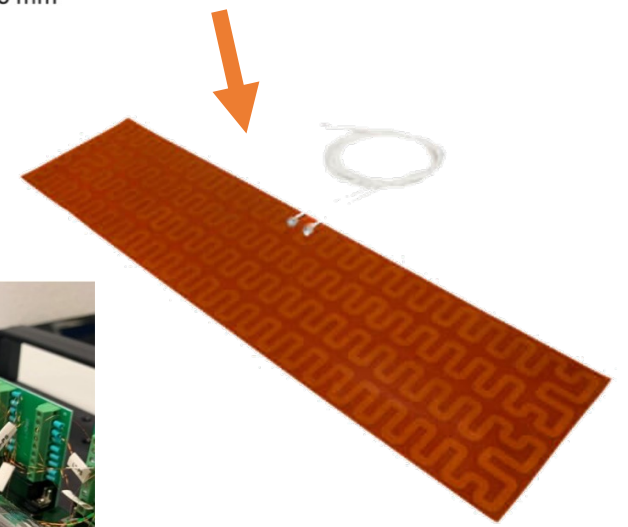
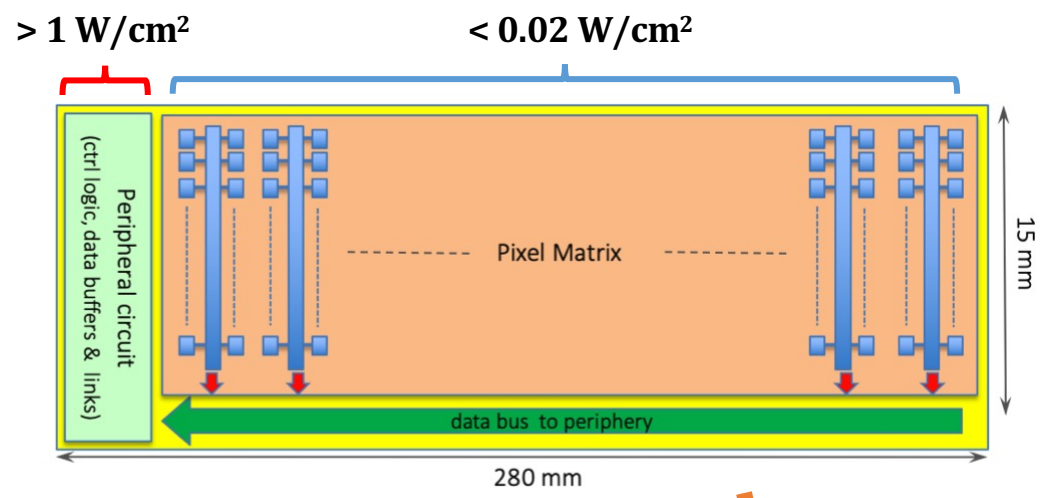


- 0.5 W/cm²
- 0.3 W/cm²
- 0.1 W/cm²
- 0.05 W/cm²
- 0.02 W/cm²

$\Delta T < 10^\circ\text{C}$ for power densities $< 0.1 \text{ W/cm}^2$

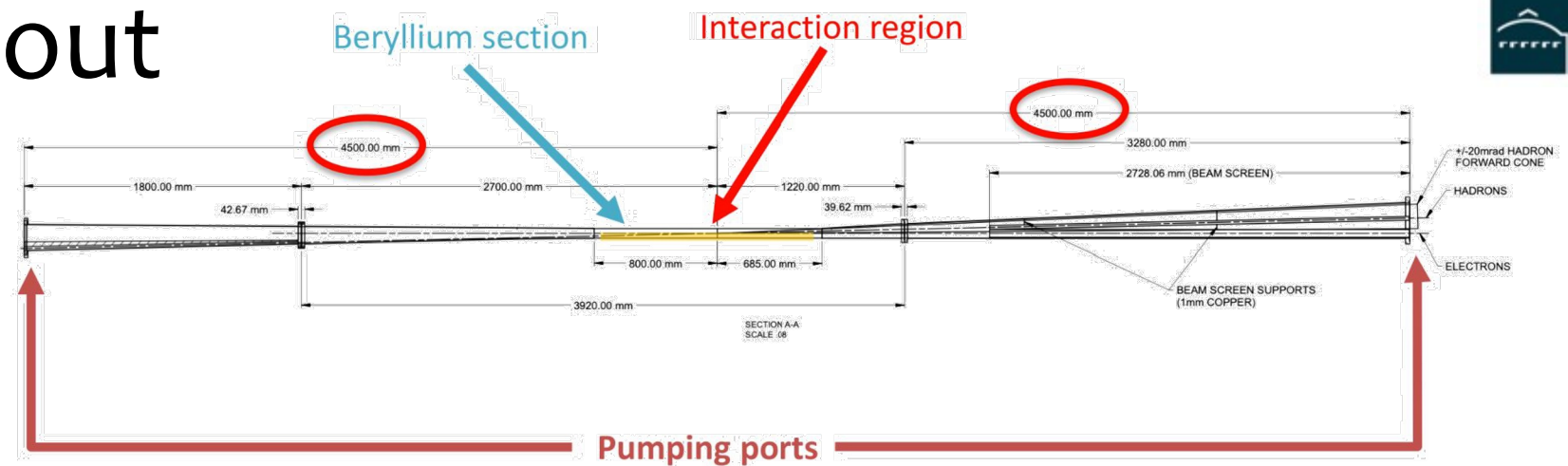
Air cooling: upcoming

- Increase air flow: new pump
- New “staves”
 - Proper heating & power densities → new heaters
 - EIC sizes
 - Careful attention to material budget
- Wind tunnel for vertex layers
- Combine air & liquid
 - Route liquid cooling near the periphery?



Beam pipe bake-out

No heater around beam pipe: keep material budget low



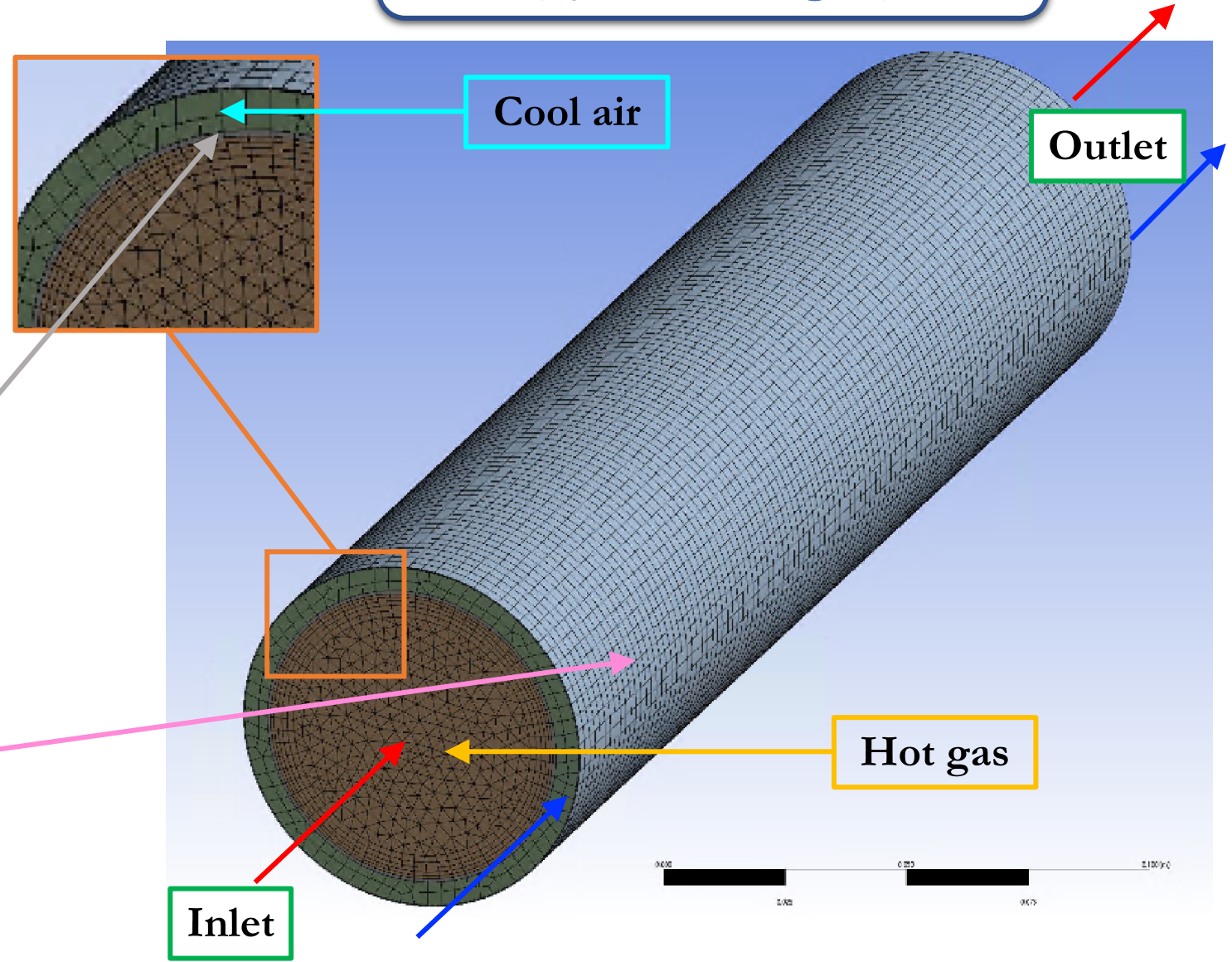
- Need to remove water molecules & other contaminants from interior of beam pipe
 - Pump hot gas in at $\geq 100^{\circ}\text{C}$ (needed to break water molecule bonds)
- Previous ANSYS study ([6/6/22](#)): increase distance between beam pipe & first layer (~ 5 mm) to keep T at silicon $\sim 30^{\circ}\text{C}$
 - **Did not include effects of air cooling on the beam pipe temperature \rightarrow recent Jlab results indicate this is a significant effect**
- Can we model this in ANSYS to see what hot gas temp is needed to maintain 100°C and keep the silicon cool enough?

Work done by Emma Yeats
(eyeats@lbl.gov)

ANSYS Setup

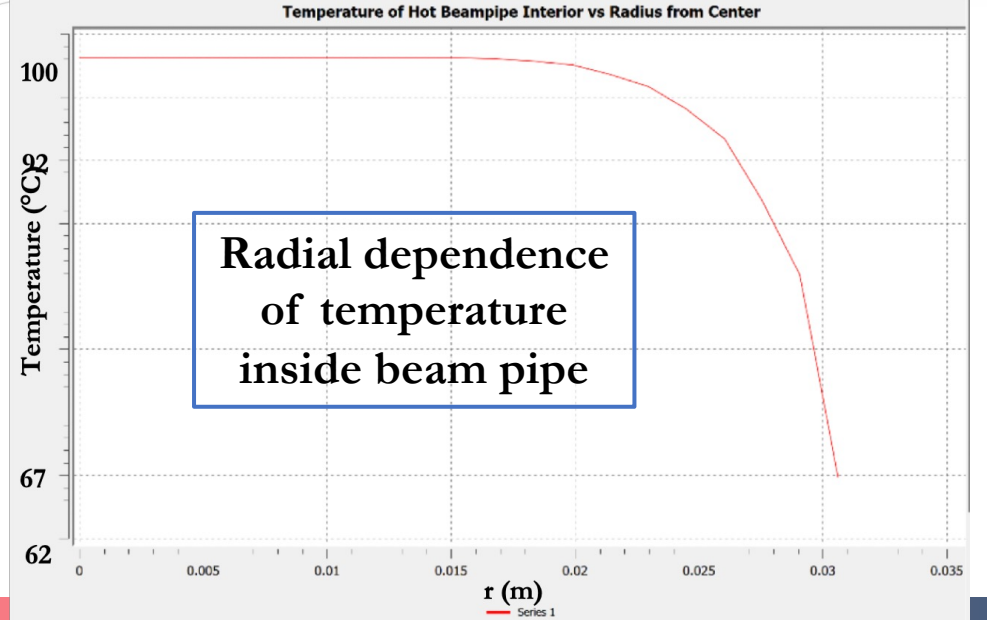
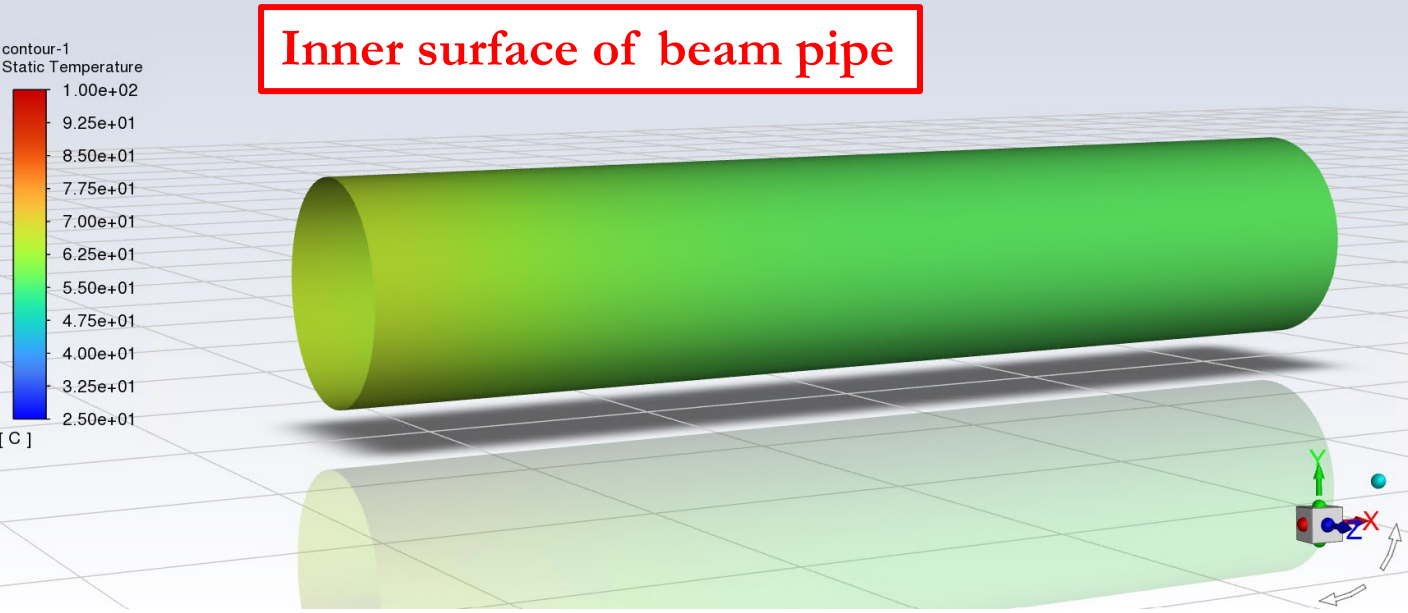
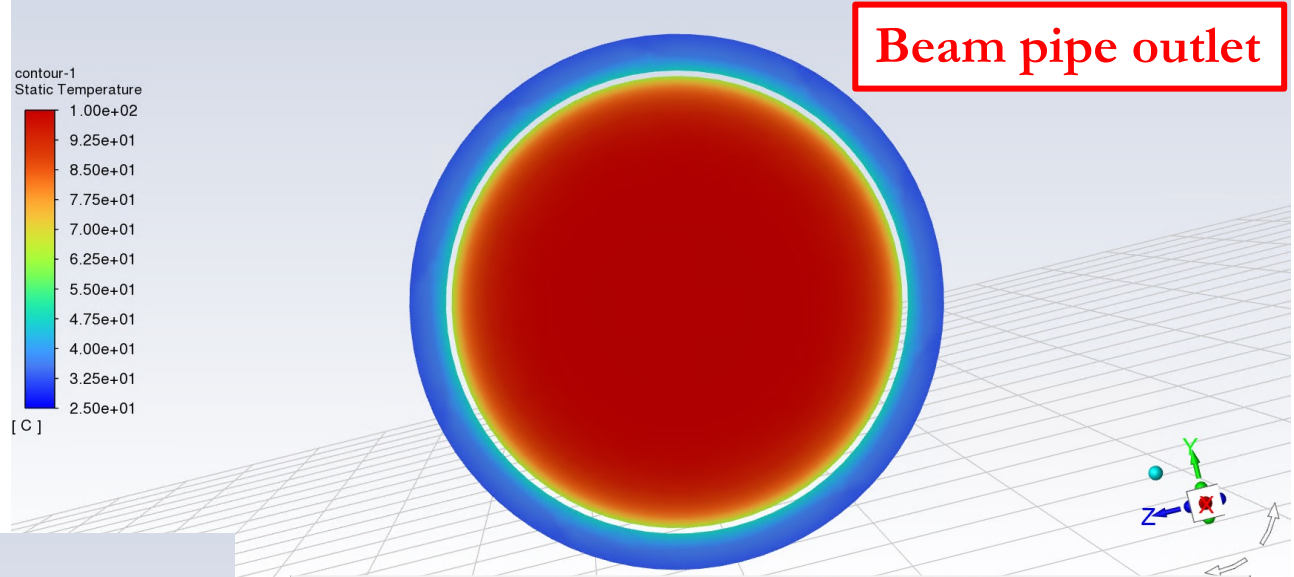
- Initial conditions at inlet
 - Cool air temp = 25°C
 - Hot gas temp = 100°C
 - Cool air velocity = 5 m/s
 - Hot gas velocity = 5 m/s

- Materials
 - Beryllium Alloy
 - Silicon

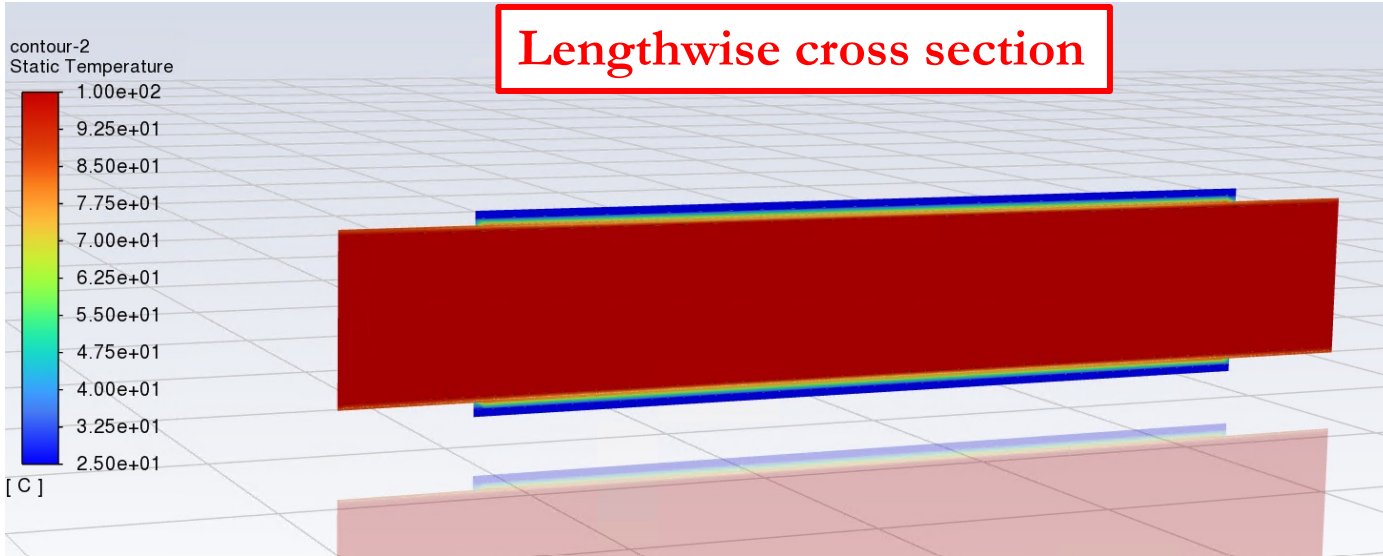


Effect of air cooling on beam pipe

Inner surface cools significantly
(60 - 70°C)



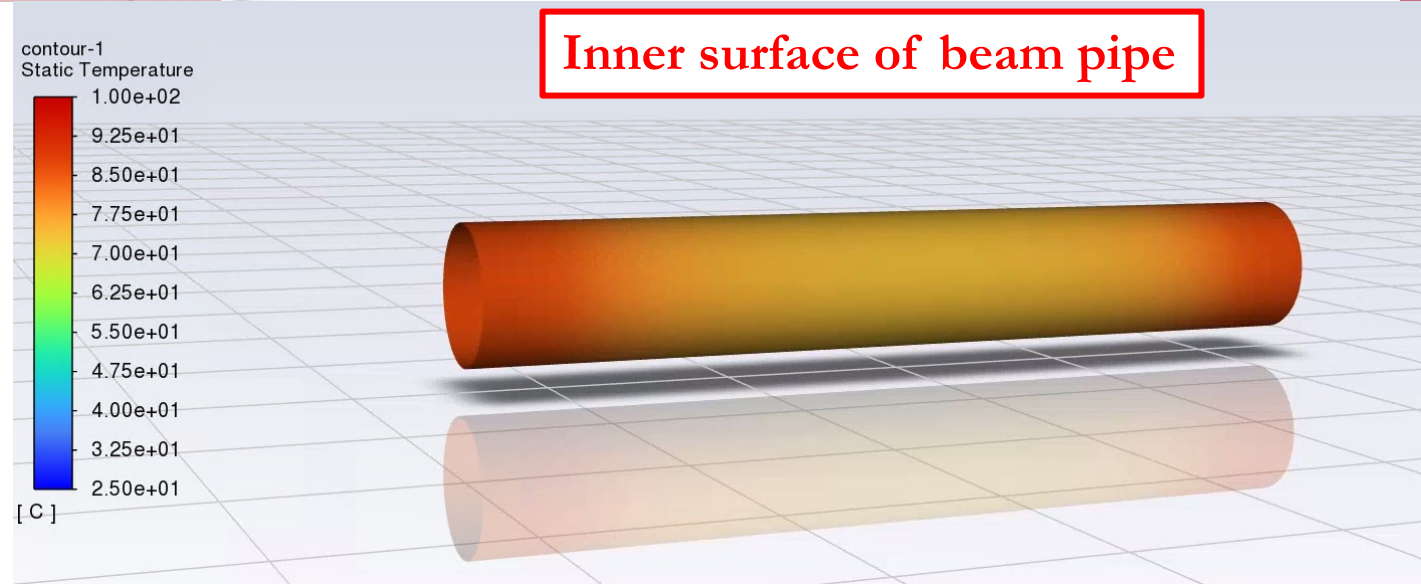
Back to basics



Sanity check:
 Hot air @ 100°C
 Ambient temp outside @ 25°C
 No air flow

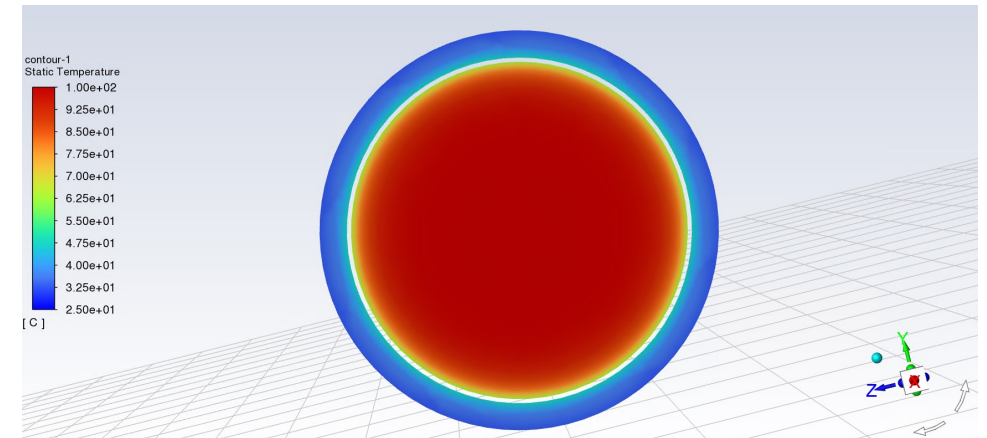
What is the minimum hot gas temperature to keep inner surface of beam pipe at 100°C?

Work in progress



Beam pipe bake-out: upcoming

- Air flow & temperature have a significant effect on inner beam pipe temperature
 - What temperature is needed to keep inner surface of beam pipe @ 100°C ?
 - What does that do to the temperature of the silicon?
- Vary air flow & temperatures
 - Want to keep silicon $< 30^{\circ}\text{C}$



Backups

Part Name	Part Color	ID [mm]	OD [mm]	Thickness [mm]	Length [mm]
Beryllium pipe	Yellow	62.00	63.52	0.76	1470.00
PEEK Support	Red	64.00	66.00	1.00	10.00
Silicon sensor L1	Green	66.00	66.08	0.04	320.50

Table 1. Dimensions from imported STEP file

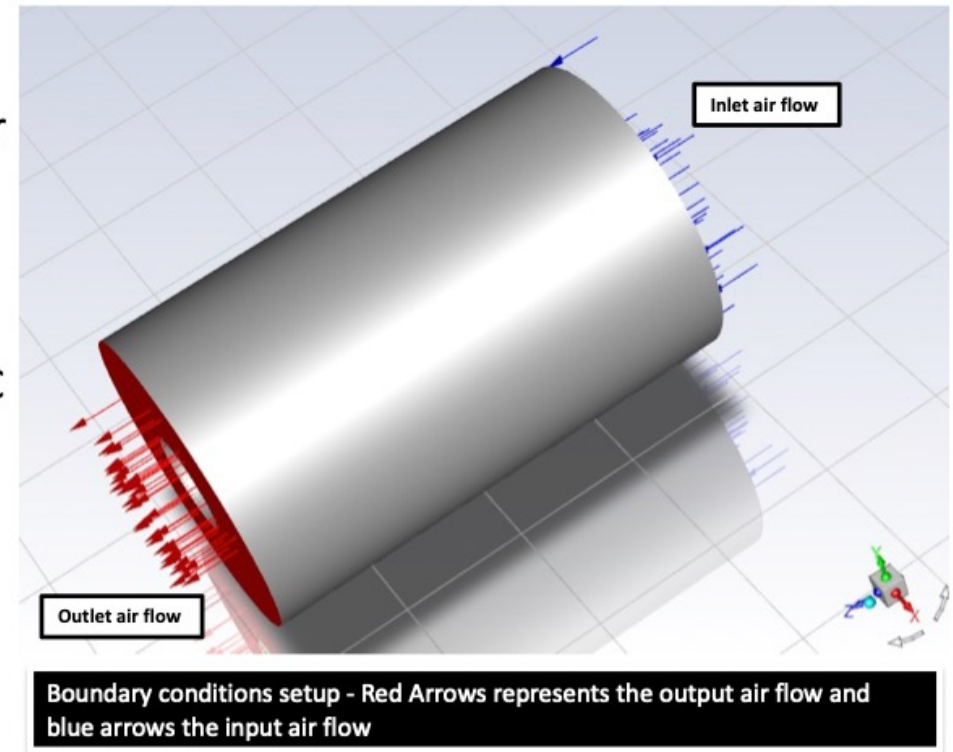
- **Materials**
 - **Air**
 - Density: 1.225 Kg/m³
 - Specific heat: 1006.43 J/Kg*K
 - Thermal conductivity: 0.0242 W/m*K
 - **Beryllium**
 - Density: 1850 Kg/m³
 - Specific heat: 1825 J/Kg*K
 - Thermal conductivity: 190 W/m*K
 - **Silicon**
 - Density: 2330 Kg/m³
 - Specific heat: 700 J/Kg*K
 - Thermal conductivity: 148 W/m*K

Ansys Fluid Flow Fluent Analysis – Conditions

LBNL

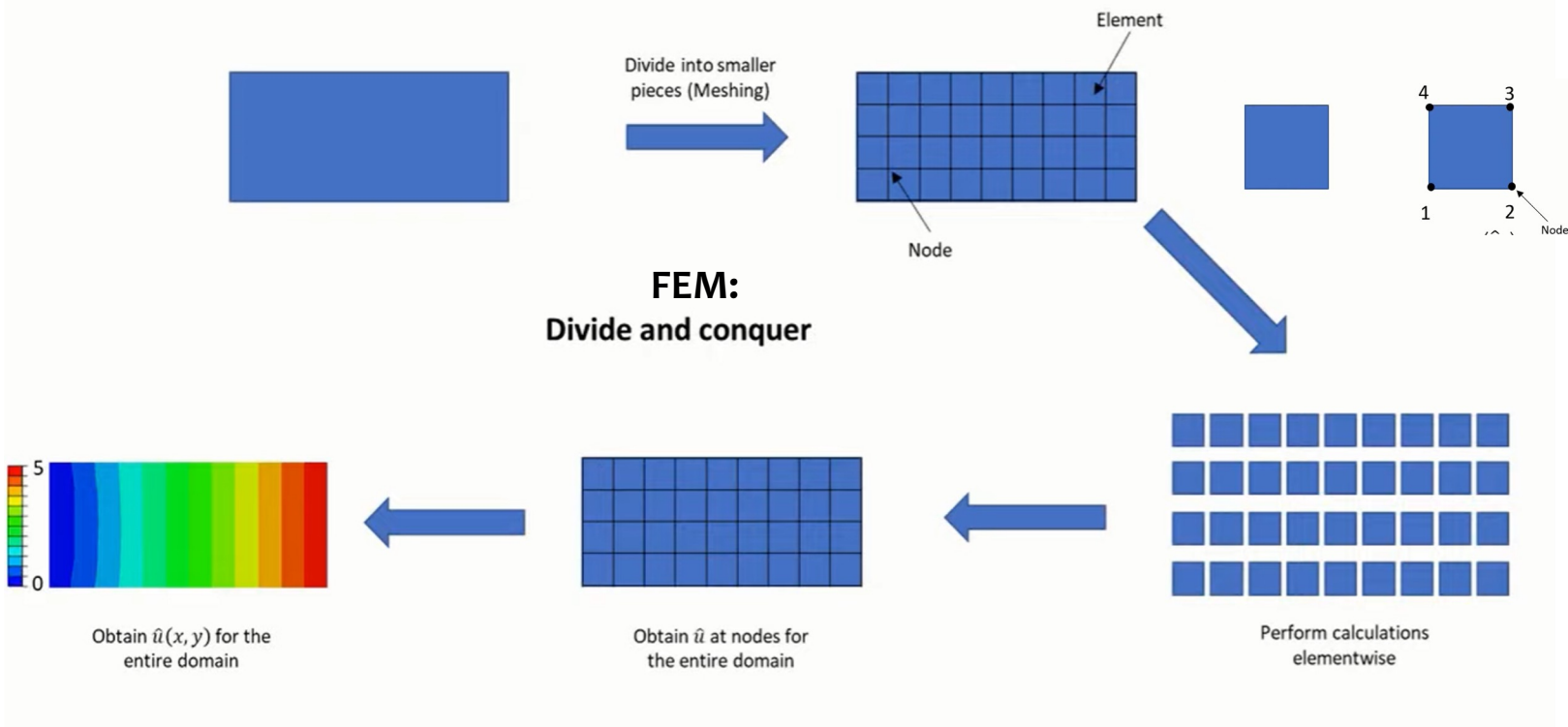
- Solver: CFD Fluid Flow Fluent
- Viscous Model: k-omega, Shear Stress Transport (SST)
- Simulation Iterations: 75
- Precision Option: Single Precision (32 bits)
- Be pipe inner face temp: not held fixed
- Inner hot gas temp: 100 – 200 C
- Air temperature: 26.85C
- Air velocity: 5 m/s
- Thermal heat transfer: forced convection

- Solver: CFD Fluid Flow Fluent
- Viscous model: k-omega, Shear Stress Transport (SST)
- Simulation Iterations: 50
- Precision option: Double
- Be pipe inner face temp: 100°C
- Air temperature: 20 to 14°C
- Air flow velocity: 0 to 20 m/s
- Thermal heat transfer: forced convection



Quick Intro to Finite Element Analysis (FEA)

FEA: Utilizes the general Finite Element Method (FEM) to analyze and calculate the solution to boundary value problems on complex 3D geometries.



FEM: obtains an approximate solution to a set of differential equations, boundary conditions by converting the boundary value problem to a system of linear equations.

General steps:

- ❖ Create your complex geometry in ANSYS's CAD software, SpaceClaim
- ❖ Create a mesh

smaller mesh size ↔ more accurate solution ↔ longer computation

- ❖ State initial conditions, materials and domains
- ❖ Initialize and calculate. Then check out your results!

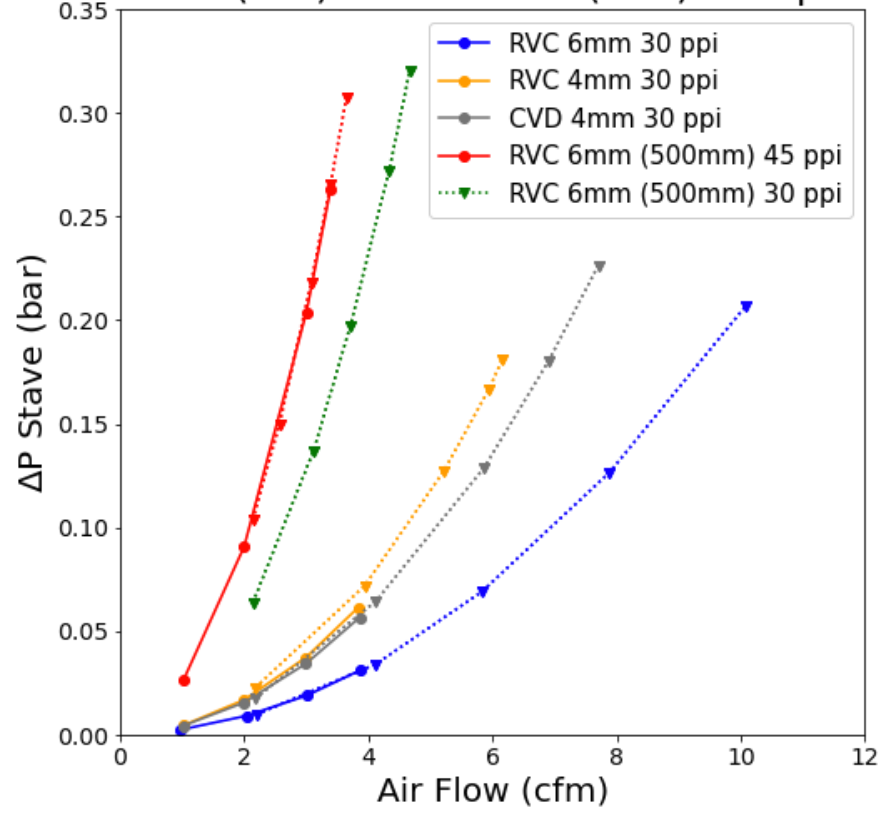
All simulations were solved using ANSYS Fluent software.

- ❖ Typically used for fluid flow simulations, but we calculated temperature distributions to study the effects of air cooling.

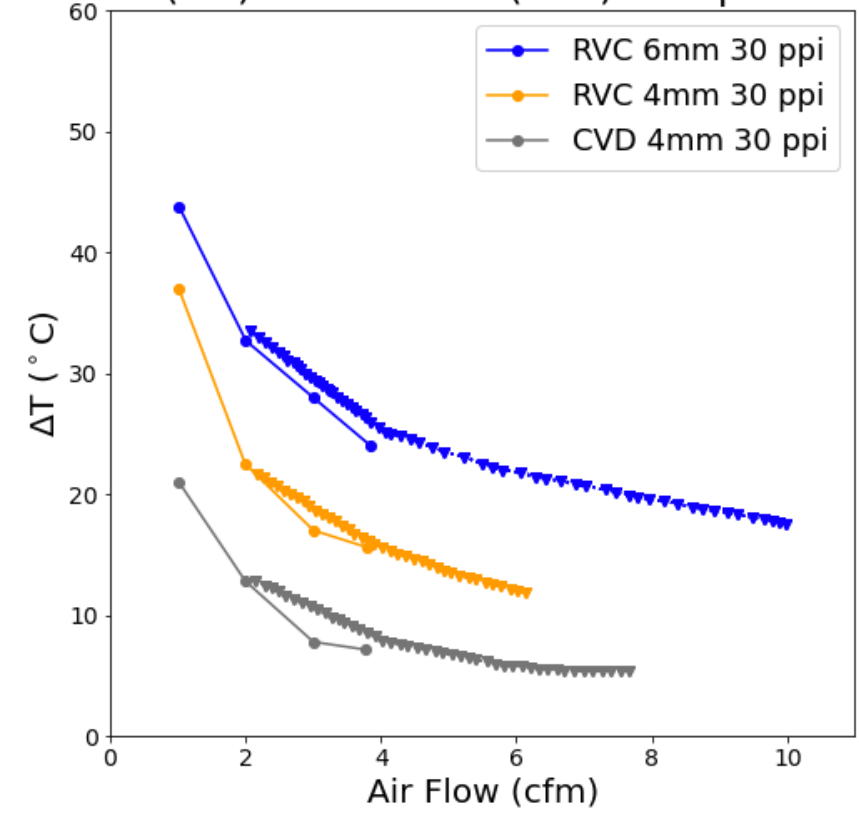
ΔT & ΔP results

Power density = 0.5 W/cm^2

ΔP Stave (bar) vs. Air Flow (cfm) Comparison



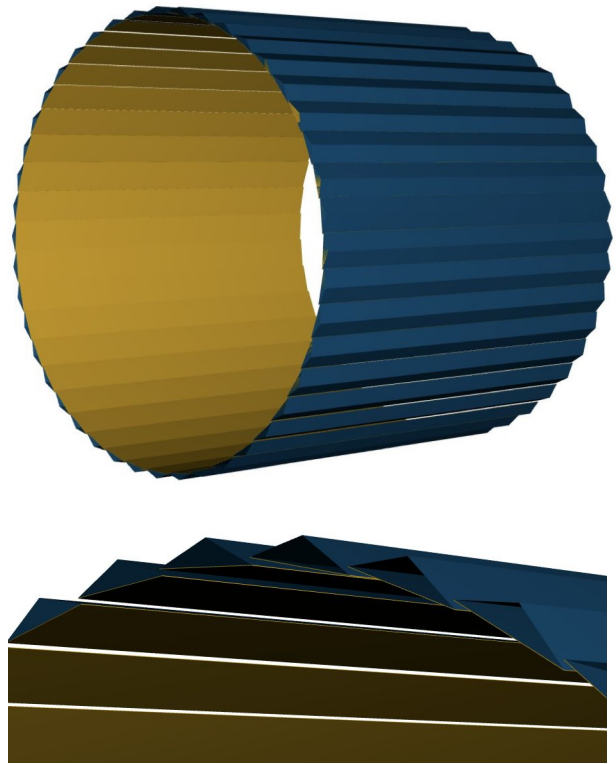
ΔT ($^{\circ}\text{C}$) vs. Air Flow (cfm) Comparison



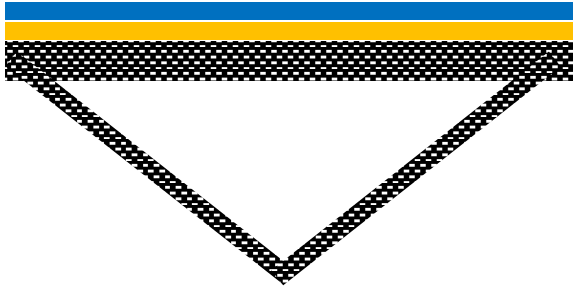
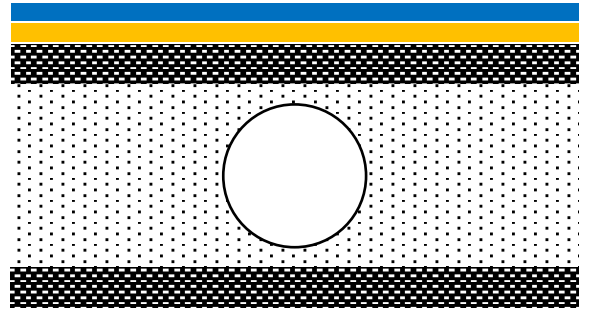
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 - - - Eng LDRD

Staves & discs

- Material budget an issue for tracking
 - Longer lengths mean more material (power, support)



Potential stave & disc cross sections



Not to scale

- FPC/power (aluminum)
- Silicon
- Carbon fiber
- Carbon foam

