

Evaluation of the Pool Critical Assembly (PCA) Benchmark with ENDF/B-VIII.1beta1 using MCNP6

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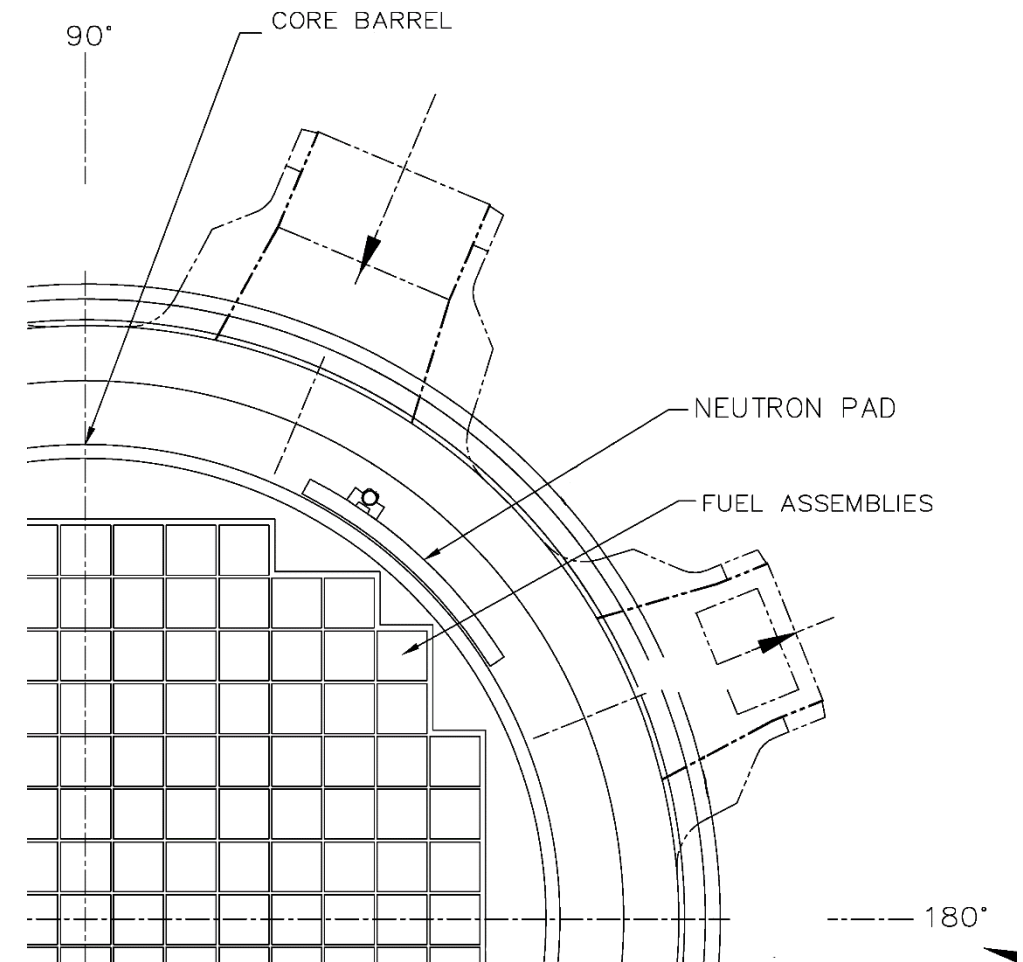
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Overview

- Background on RPV fluence calculations for LWRs
- ENDF/B-VIII.1b1 Benchmarking
 - 1D PWR Comparison
 - Pool Critical Assembly

Background on Fluence Calculations

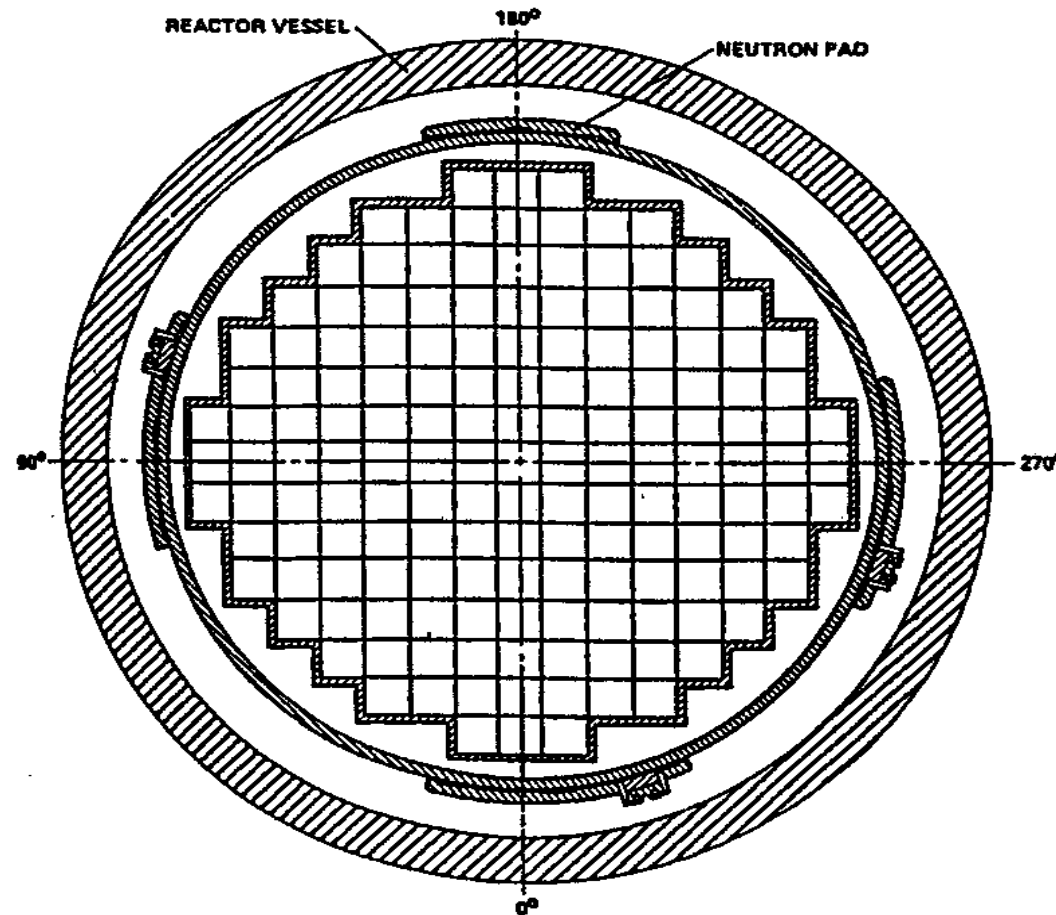
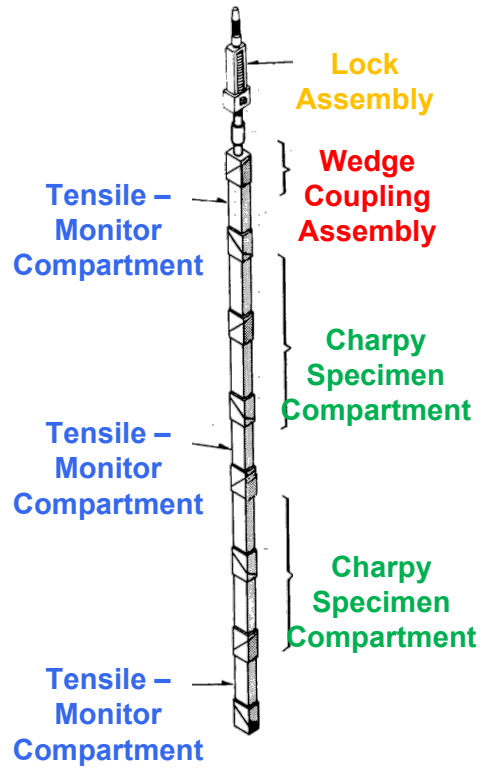
- Most fission neutrons remain inside the core, supporting the self-sustaining chain reaction
- We're interested in the relatively few neutrons that leak outside of the core and impinge upon the reactor vessel



Background on Fluence Calculations

- The reactor pressure vessel and internals components are susceptible to irradiation-induced degradation of material properties
- These changes are manifested as:
 - Reduction in the toughness during ductile fracture
 - Tendency for brittle fracture to onset at increasing temperatures
- All reactors are required to have a materials surveillance program to monitor changes in reactor vessel materials properties

Background on Fluence Calculations

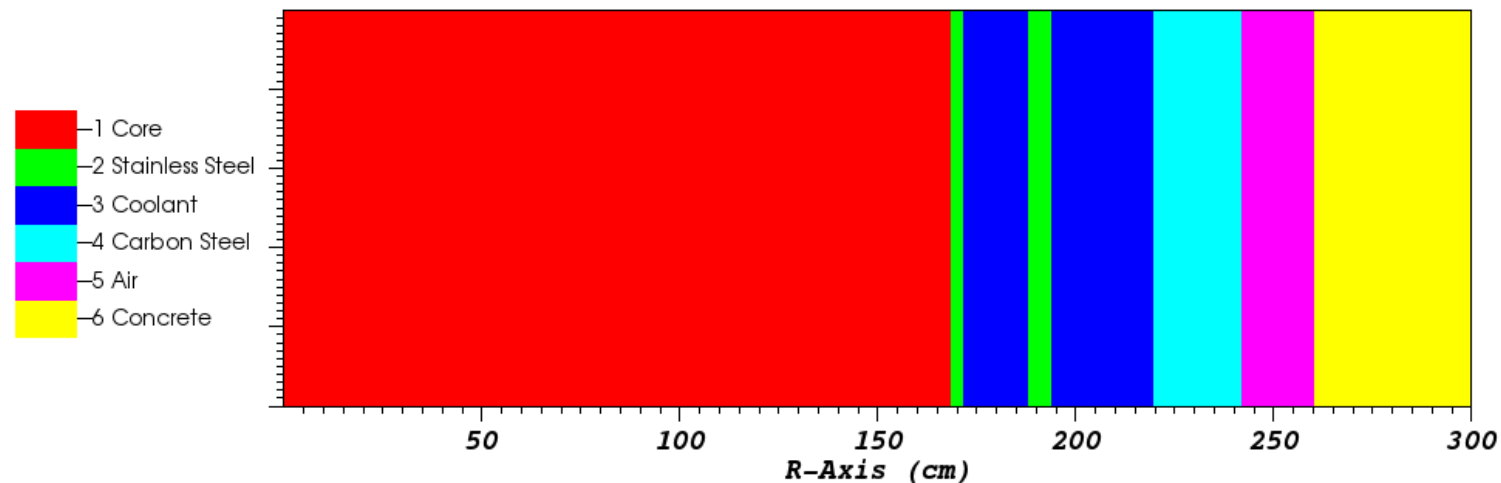


Background on Fluence Calculations

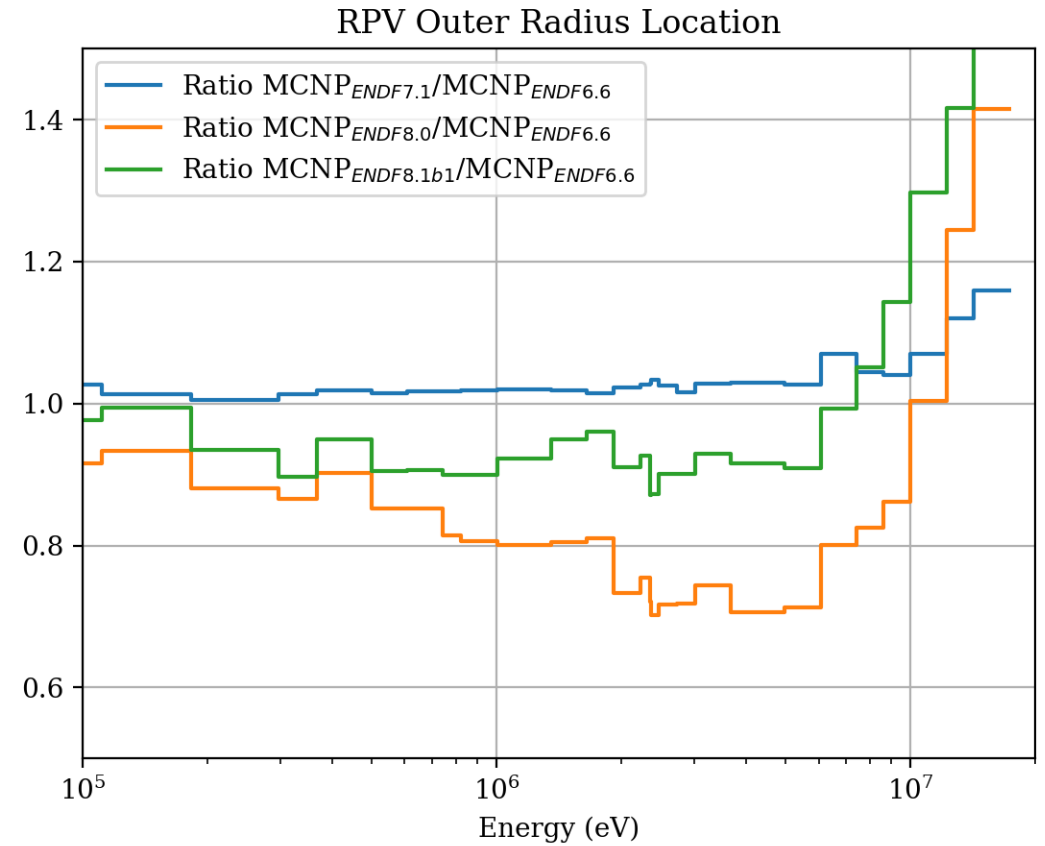
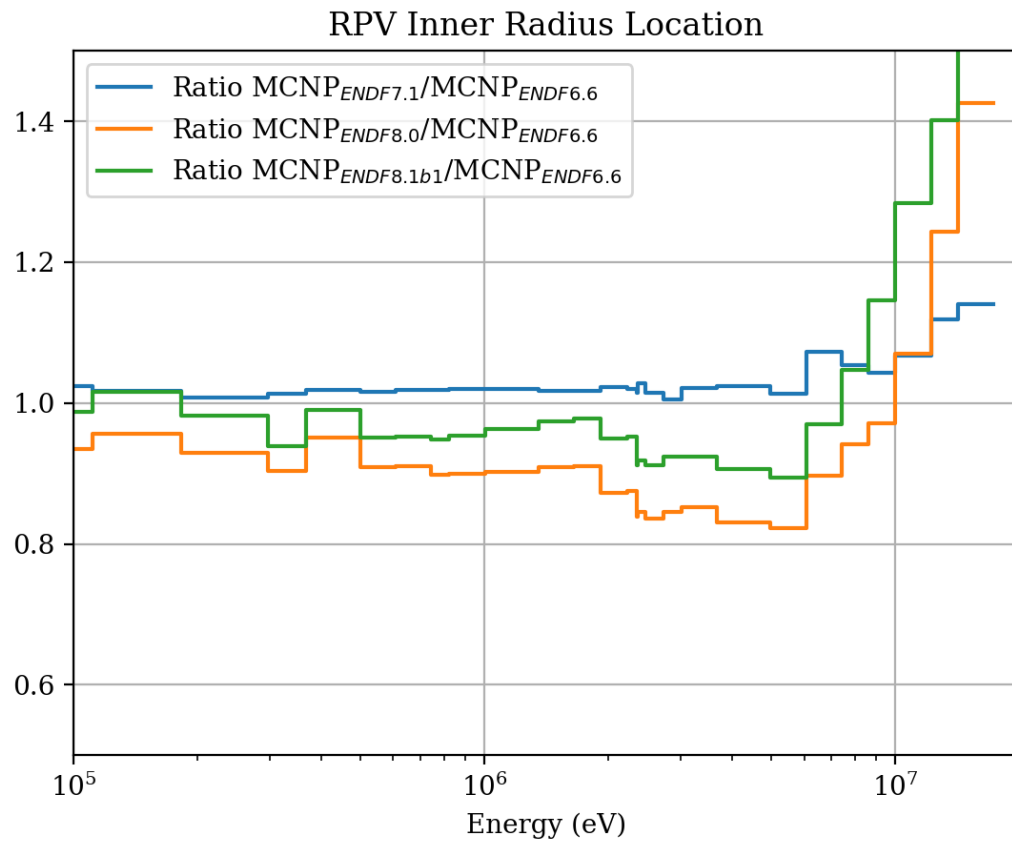
- Beginning in the 1980s, the NRC began to be concerned about the possibility of pressurized thermal shock (PTS) events
 - Postulated accident causes safety injection of cold coolant, placing severe thermal stresses on the (hot) reactor vessel
 - Event is followed by re-pressurization of the reactor vessel
 - This sequence of events could challenge the structural integrity of the reactor vessel
- Reactor vessel neutron exposure (especially for P's) is carefully tracked and monitored

1D PWR Benchmarking

- A 1-D Monte Carlo model of a PWR was constructed to benchmark the cross sections:
 - Similar to the model used to generate the “fine group” weighting spectra for the BUGLE-96 library
 - Tallies were recorded at the inside surface and outside surface of the reactor pressure vessel



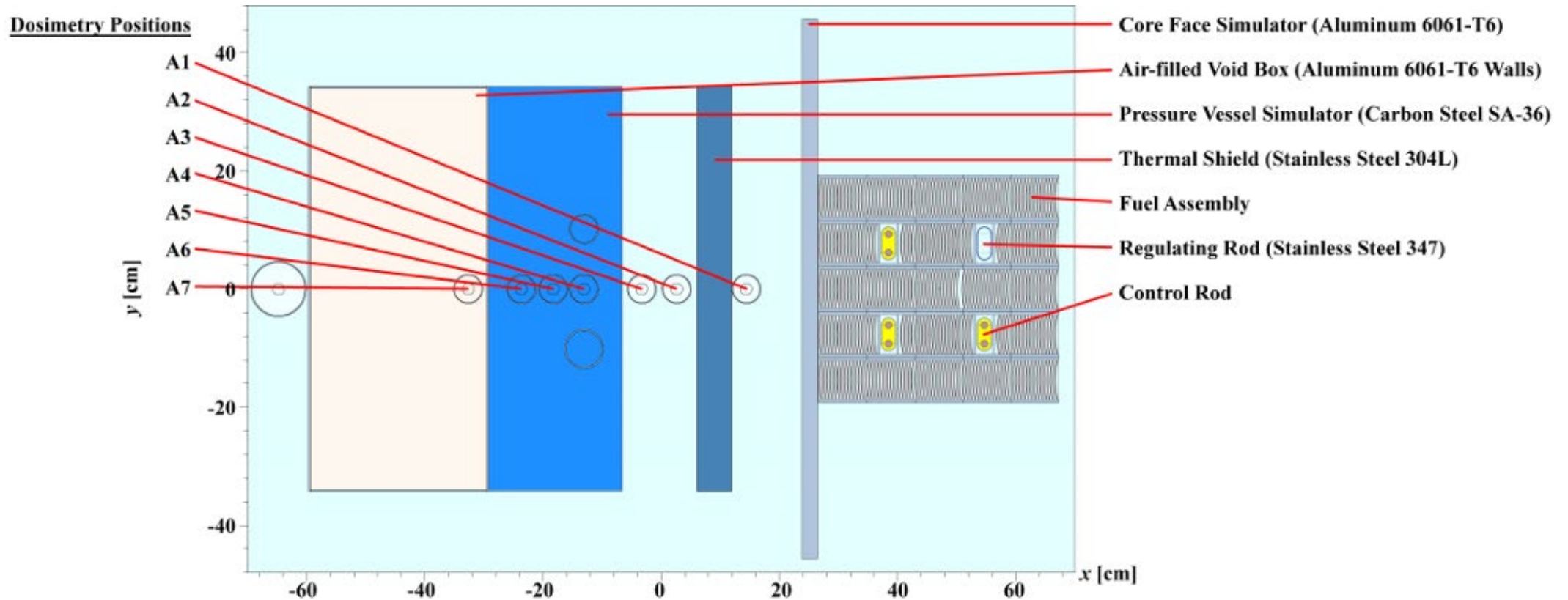
1D PWR Benchmarking



Pool Critical Assembly Benchmarking

- The Pool Critical Assembly (PCA) Pressure Vessel Simulator experiment was performed in the early 1980s as part of the NRC's LWR Pressure Vessel Surveillance Dosimetry Improvement Program (LWR-PV-SDIP)
 - Core region consists of high-enriched U-235 plates in a water pool with simulated reactor internals structural materials
 - Measurements: Al-27, Ni-58, Rh-103, In-115, U-238, and Np-237 sensor materials
 - Still widely-used as a methodology benchmark today
- Benchmark was recently re-analyzed with exact geometry by Dr. Kulesza (LANL/X-5), and MCNP inputs were published and available for use:
 - NUCLEAR TECHNOLOGY · VOLUME 197 · 284–295 · MARCH 2017
 - Paper: <https://doi.org/10.1080/00295450.2016.1273711>
 - MCNP Inputs: <https://doi.org/10.2172/1601379>

Pool Critical Assembly Benchmarking



Ref: Kulesza, Martz

Pool Critical Assembly Benchmarking

- MCNP workflow:
 - Step 1: KCODE calculation
 - Step 2: SSW (volumetric) – record fission source
 - Step 3: SSR - neutron transport to sensor locations
- Other notes:
 - Dosimetry cross sections used IRDFF-II data: <https://www-nds.iaea.org/IRDFF/>
 - Weight windows generated with ADVANTG
 - High-energy weight windows for Al-27 (tricky)
 - Lower-energy weight windows for the other sensors

Pool Critical Assembly Benchmarking

- Measurements:

	Reaction Rate (rps per source neutron) ($\pm 1\sigma$ Uncertainty)					
Location	$^{27}\text{Al}(n, \alpha)$		$^{58}\text{Ni}(n, p)$		$^{103}\text{Rh}(n, n')$	
A1	5.55E-33	(1.0%)	6.35E-31	(1.4%)	4.06E-30	(1.0%)
A2	7.19E-34	(2.0%)	6.74E-32	(2.0%)	—	—
A3	3.16E-34	(1.0%)	2.52E-32	(1.4%)	—	—
A4	7.19E-35	(2.0%)	5.78E-33	(1.0%)	5.67E-32	(1.5%)
A5	2.89E-35	(2.2%)	2.28E-33	(1.8%)	3.19E-32	(5.0%)
A6	1.09E-35	(2.2%)	8.10E-34	(2.2%)	1.61E-32	(5.0%)
A7	—	—	—	—	—	—
Location	$^{115}\text{In}(n, n')$		$^{238}\text{U}(n, f)$		$^{237}\text{Np}(n, f)$	
A1	1.06E-30	(1.0%)	—	—	8.71E-30	(6.2%)
A2	1.15E-31	(2.0%)	—	—	—	—
A3	3.76E-32	(1.0%)	—	—	2.98E-31	(6.3%)
A4	1.11E-32	(0.7%)	1.86E-32	(6.9%)	1.22E-31	(5.5%)
A5	5.22E-33	(1.5%)	8.36E-33	(6.8%)	6.80E-32	(5.7%)
A6	2.21E-33	(3.0%)	3.42E-33	(7.1%)	3.54E-32	(5.8%)
A7	—	—	—	—	9.51E-33	(9.2%)

Pool Critical Assembly Benchmarking

- C/E Results (ENDF/B-VII.1):
 - MC uncertainty \approx 1%

	al27a	ni48p	rh103n	in115n	u238f	np237f	avg	std dev
	0.99	1.00	1.07	1.03			1.02	3.7%
	1.00	1.05	1.14	1.06			1.06	5.3%
	1.01	1.06	1.12	1.11			1.08	4.6%
	0.98	1.01	1.06	1.07	1.04	1.08	1.04	3.7%
	0.98	1.03	1.00	1.07	1.04	1.10	1.04	4.4%
	0.99	1.09	0.98	1.09	1.04	1.08	1.04	5.0%
			1.02	1.05	1.05	1.20	1.08	7.6%
avg	0.99	1.04	1.05	1.07	1.04	1.11	1.05	
std dev	1.4%	3.3%	6.1%	2.4%	0.2%	1.1%		4.8%

Pool Critical Assembly Benchmarking

- C/E Results (ENDF/B-VIII.0):
 - MC uncertainty \sim 1%

	al27a	ni48p	rh103n	in115n	u238f	np237f	avg	std dev
	0.96	0.96	1.04	1.00			0.99	3.9%
	0.95	0.93	1.05	0.97			0.97	5.4%
	0.98	0.95	1.03	1.01			0.99	3.3%
	0.94	0.86	0.94	0.92	0.90	0.97	0.92	4.3%
	0.89	0.83	0.87	0.90	0.87	0.97	0.89	5.3%
	0.88	0.85	0.85	0.90	0.84	0.95	0.88	4.7%
			0.88	0.86	0.84	1.05	0.91	10.5%
avg	0.93	0.90	0.95	0.94	0.86	0.98	0.93	
std dev	4.1%	6.3%	9.3%	5.2%	3.1%	1.3%		6.9%

Pool Critical Assembly Benchmarking

- C/E Results (ENDF/B-VIII.1b1):
 - MC uncertainty \sim 1%

	al27a	ni48p	rh103n	in115n	u238f	np237f	avg	std dev
	0.97	0.96	1.04	1.00			0.99	3.9%
	1.02	0.98	1.08	1.01			1.02	4.3%
	1.05	1.01	1.07	1.06			1.05	2.5%
	1.03	0.96	1.00	1.01	0.98	1.03	1.00	2.7%
	1.03	0.96	0.95	1.00	0.98	1.05	0.99	4.0%
	1.04	1.02	0.93	1.03	0.98	1.03	1.00	4.1%
			0.96	0.99	0.99	1.13	1.02	7.6%
avg	1.02	0.98	1.01	1.01	0.98	1.06	1.01	
std dev	2.8%	2.9%	6.4%	2.1%	0.1%	1.0%		4.2%

Conclusions

- ENDF/B-VIII.1b1 reduces the magnitude of the differences observed with ENDF/B-VIII.0 as compared to current cross section data.
- PCA comparisons with ENDF/B-VIII.1b1 seem to show better agreement with the measured data than ENDF/B-VII.1 or ENDF/B-VIII.0.