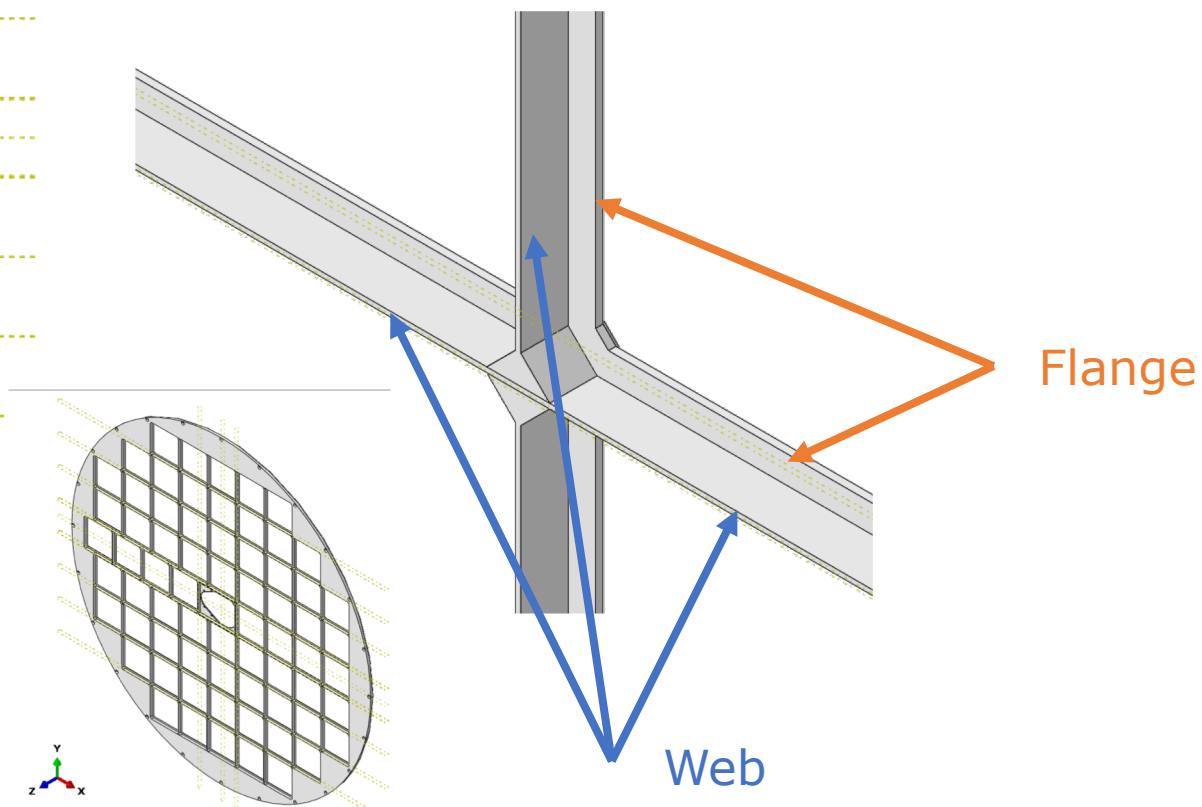
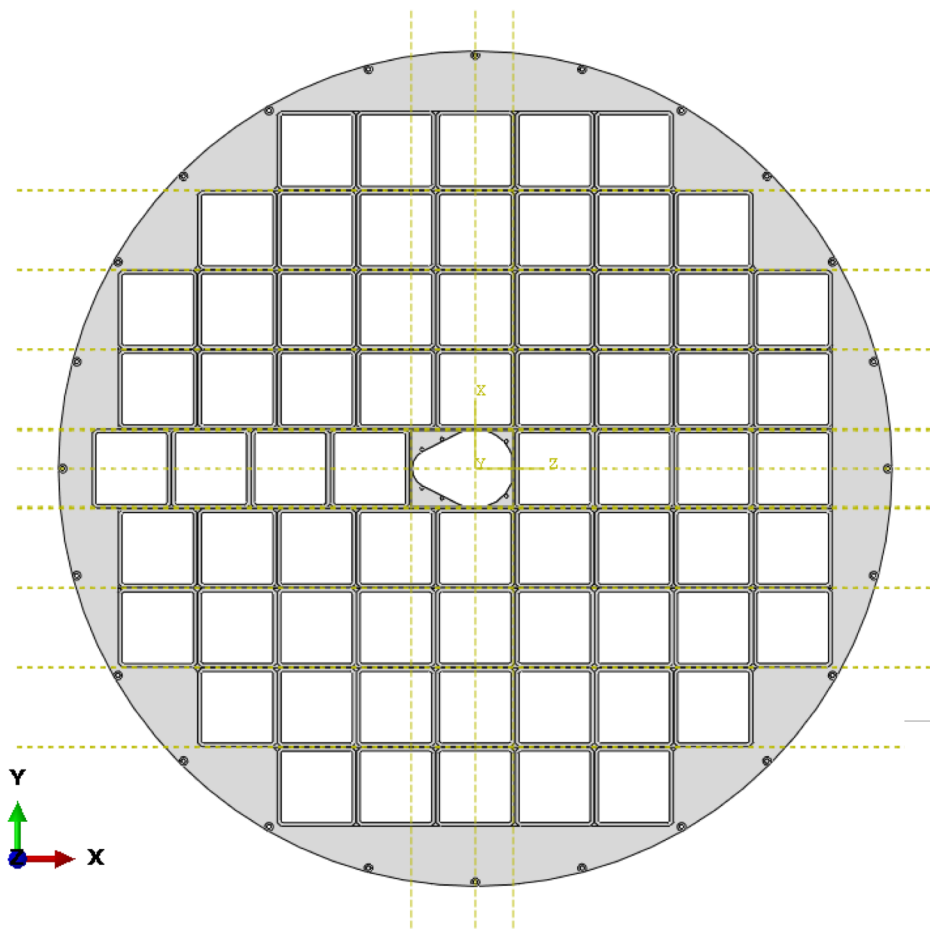


pfRICH top sensor plate structural simulation results – 22 Oct 2023

Sushrut Karmarkar, Andy Jung

- As given in the CAD the web is 1 mm and the flange is 1.5 mm thick.
- Entire structure is envisioned to be made from CFRP laminates



⬡ Layup used in $[0/+45/-45/90/0]_s$ which approximates the material properties

⬡ Two iterations are tried out

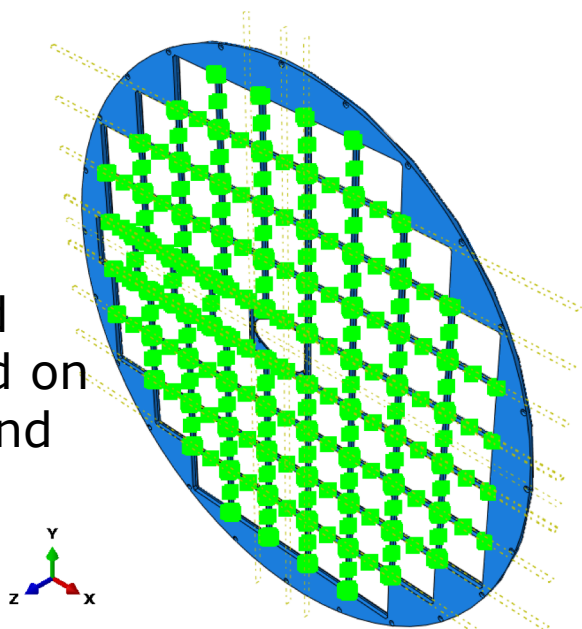
1. Standard modulus carbon fiber properties (AS4 / 8552 40 % RC)
2. High modulus carbon fiber properties (M55j / Patz F6 39% RC)

⬡ Nonstructural load of 97 kg is used for the 68 sensors, equally distributed on the web and flange for each condition

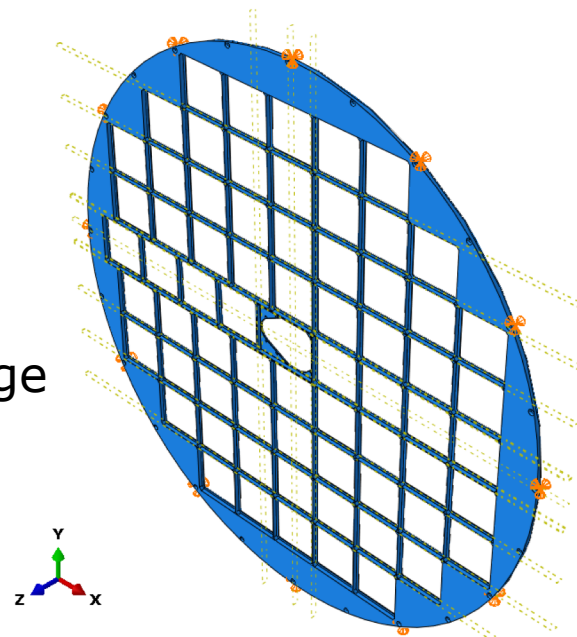
⬡ BC – edge held with $u_1=u_2=u_3=0$

⬡ Simulation results are presented for both when pfRICH is held vertical (as installed) as well as horizontal (during assembly stage)

97 kg load distributed on the web and flange

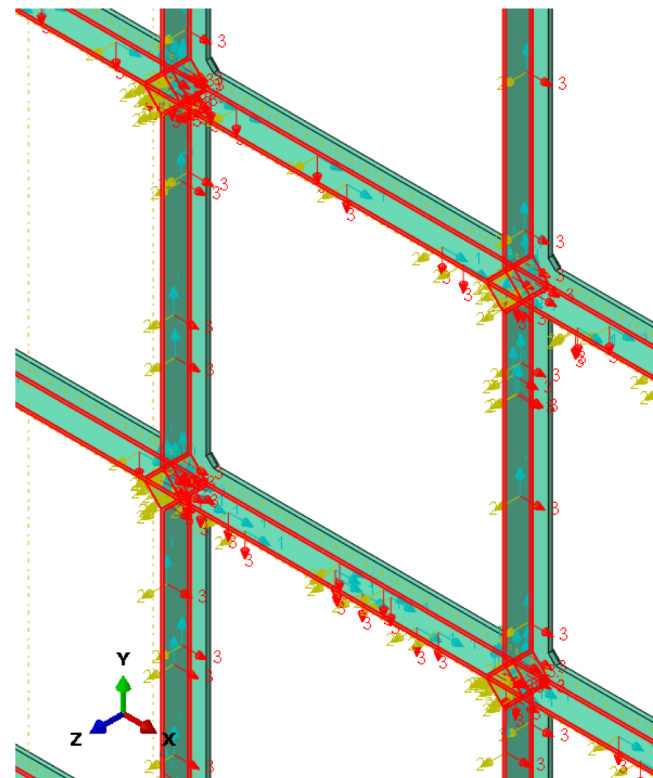
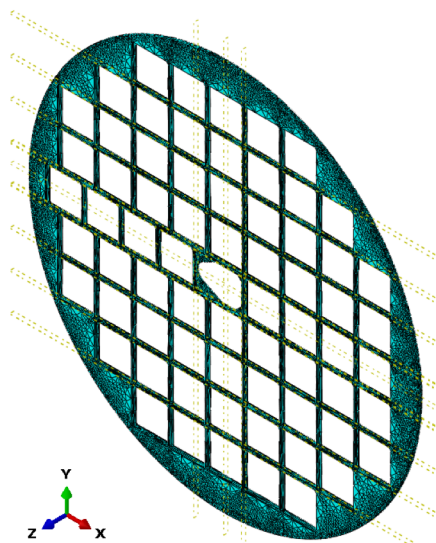


BC – edge
 $u_1=0$
 $u_2=0$
 $u_3=0$

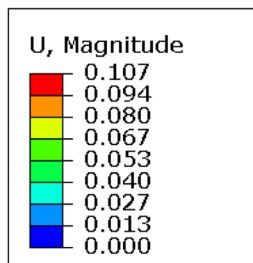


- ⬡ Each rib and flange and web has independent orientation definition for closest to actual manufacturing approximation
- ⬡ Base plate assumed to be a single layup and center hole cut from a single layup-
 - ⬡ This is a 638 mm radius disc – at Purdue we have the capability to layup a ~1.5 m diameter disc and machine out the center section
 - ⬡ Ribs, flanges and webs in the current model assume tie constraint (perfect load transfer) this approximation is okay for first order simulation results – needs to change to a kinematic coupling or constraint once the elaborate design is done.

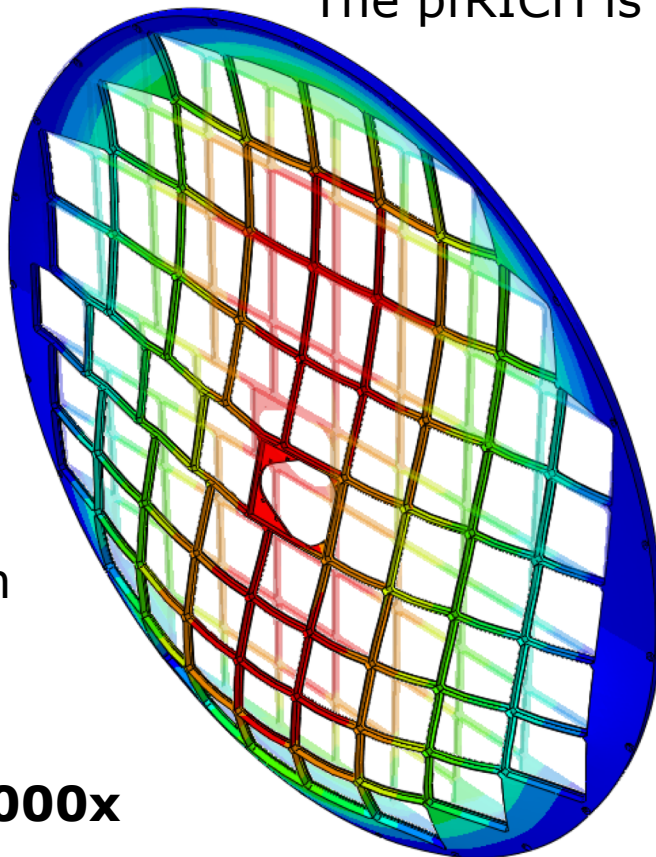
- ⬡ Tet-mesh used because of the intricate geometrical details
- ⬡ Linear elements used – at least 2 elements through thickness for each cell
- ⬡ 210390 linear tetrahedral elements of type C3D4



As installed configuration with web = 1mm and flange = 1.5 mm
 The pFRICH is assumed to be assembled vertical as shown here.



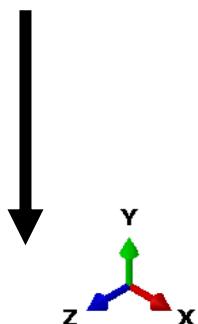
Unit mm



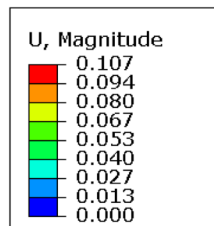
1000x

Step: LoadOnlyVerticle
 Increment 1: Step Time = 1.000
 Primary Var: U, Magnitude
 Deformed Var: U Deformation Scale Factor: +1.000e+03

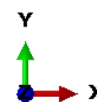
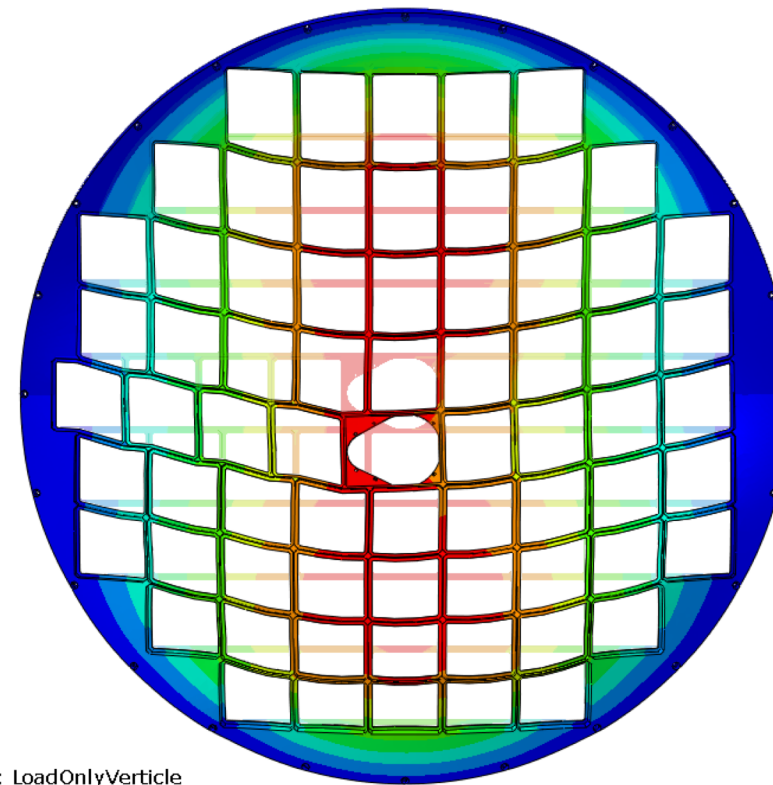
Gravity acting
 along -y direction



Caveat: this likely means the shape is held up by the sensor "elements" itself! An issue ?



Unit mm



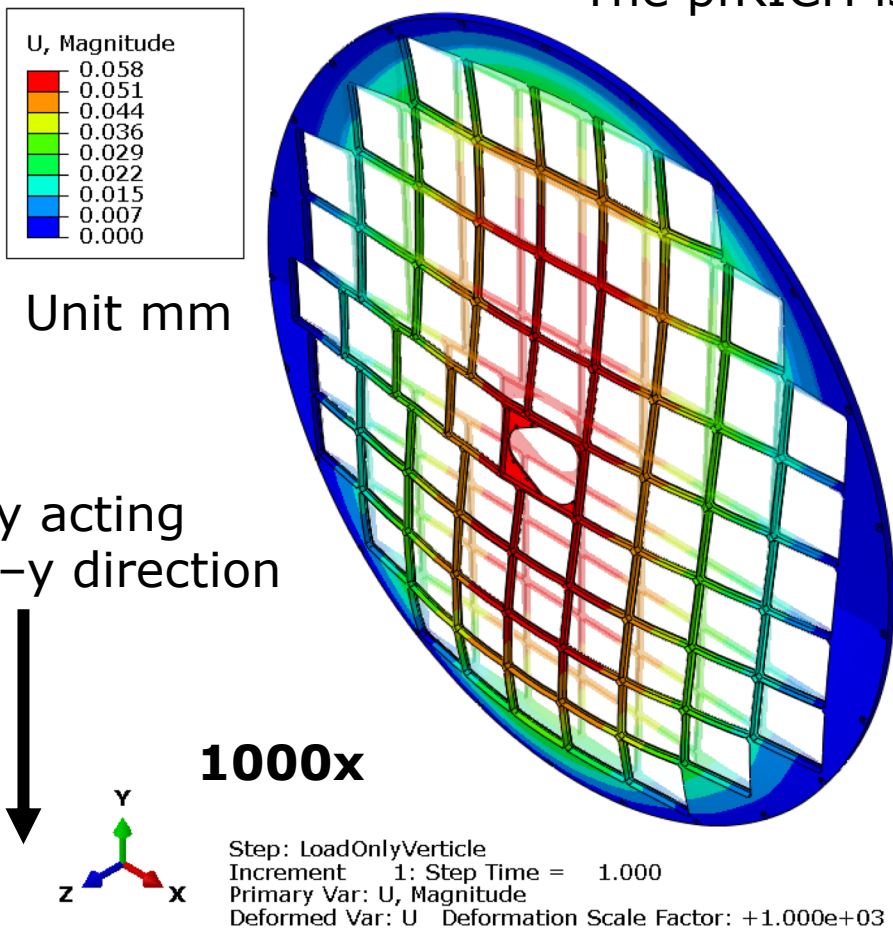
Step: LoadOnlyVerticle
 Increment 1: Step Time = 1.000
 Primary Var: U, Magnitude
 Deformed Var: U Deformation Scale Factor: +1.000e+03

1000x the deformation shown to understand the trend in deformation

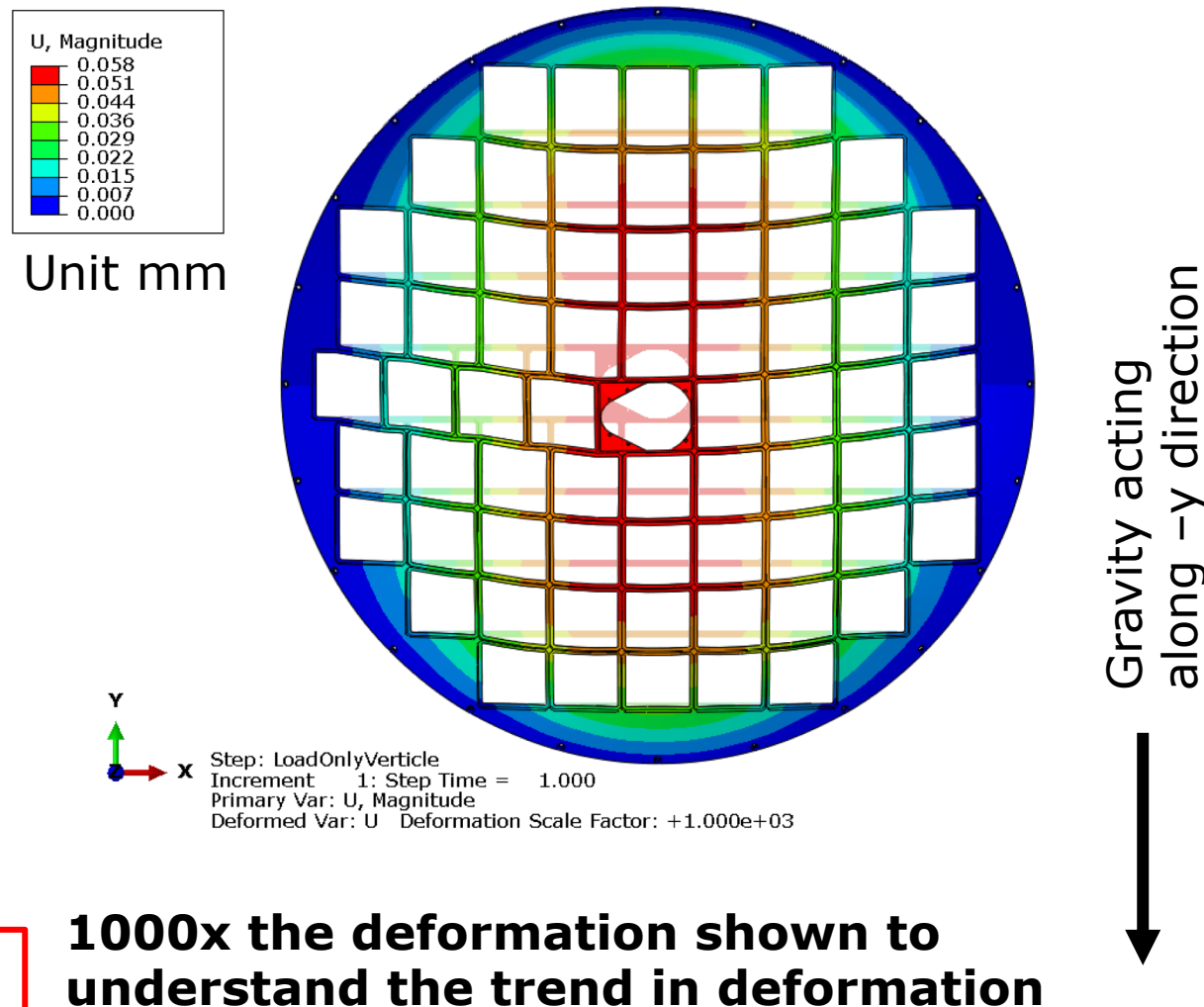
Gravity acting
 along -y direction



As installed configuration with web = 1mm and flange = 1.5 mm
 The pFRICh is assumed to be assembled vertical as shown here.

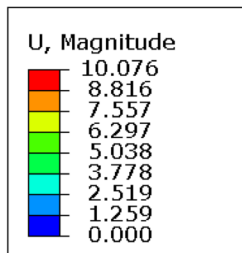


Caveat: this likely means the shape is held up by the sensor “elements” itself! An issue ?

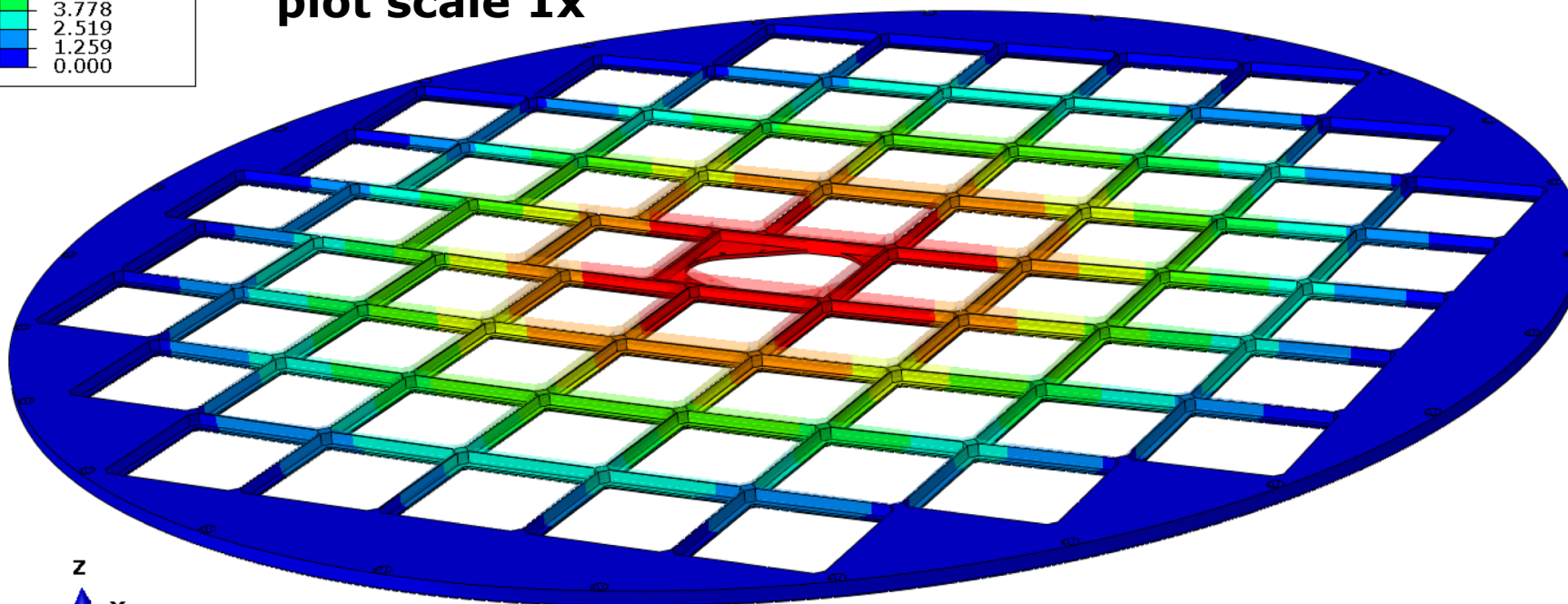


- Horizontal configuration with web = 1mm and flange = 1.5 mm. The pFRICH is assumed horizontal.
- **In this case the web and flange will break/snap**

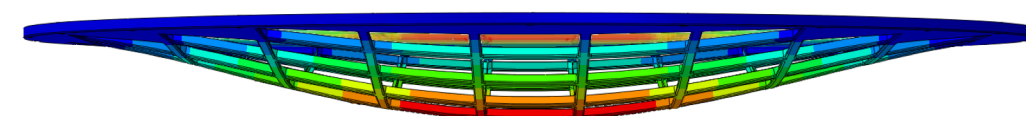
Unit mm



**Deformation
plot scale 1x**



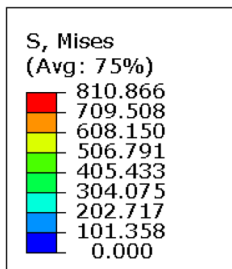
Step: LoadHorizontal
Increment 1: Step Time = 1.000
Primary Var: U, Magnitude
Deformed Var: U Deformation Scale Factor: +1.000e+00



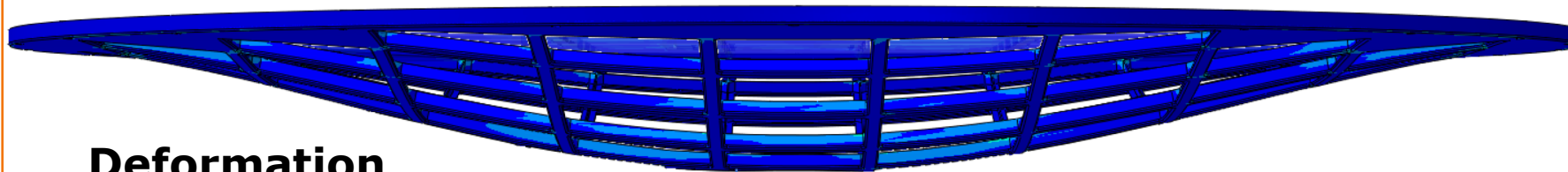
**10x the deformation shown to
understand the trend in deformation**

- Horizontal configuration with web = 1mm and flange = 1.5 mm
- The pfRICH is assumed horizontal. In this case the web and flange will break/snap. Flexural strength for M55j ~ 1000 MPa – this is close to the breaking point
- Question is will pfRICH see this configuration of loading during commissioning or test beam or transport ?
- If unsure or potential yes: we need to design differently!

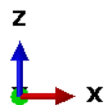
Unit mm



Gravity acting
along -z direction



**Deformation
plot scale 10x**



Step: LoadHorizontal
Increment 1: Step Time = 1.000
Primary Var: S, Mises
Deformed Var: U Deformation Scale Factor: +1.000e+01

1. Horizontal orientation is to weak a structure to support weight, vertical is ok-ish but pressure on sensor plates an issue ?
 - Horizontal configuration of loading during commissioning or test beam or transport ? If unsure or potential yes: we need to design differently
2. Creating CADs and FE models with web and flange thicknesses increased, ongoing:
 - ◈ Iterations on-going are as follows –
 - ◈ Web thickness = 2mm; flange = 1.5mm
 - ◈ Web thickness = 3.5mm; flange = 3 / 1.5mm ?!
3. Multiple option to stiffen the structure, e.g. more complicated ply layup – studies ongoing!
4. Emcal “wants” temps stable to 0.2C, no heating allowed! Room temp is ok ?! Light yield is best.

Caveats:

1. This simulation assumes perfect bonding between the vertical and horizontal rib structure. This is not true in reality – iterative FE model studies to understand effect of kinematic coupling on this will also be done simultaneously
2. Thermal simulation for 350 W and 500 W total heat from 68 sensor blocks being simulation with ambient temp assumed as -5 degree C and forced air convection cooling
 - Is active cooling even needed ? If really < 500 W for whole array it seems fairly low power density...might get away with dedicated paths in structure
 - Even easier if structure gets “stiffened” up