



# ODH Analysis for Service and Auxiliary Buildings RHIC Recovery review

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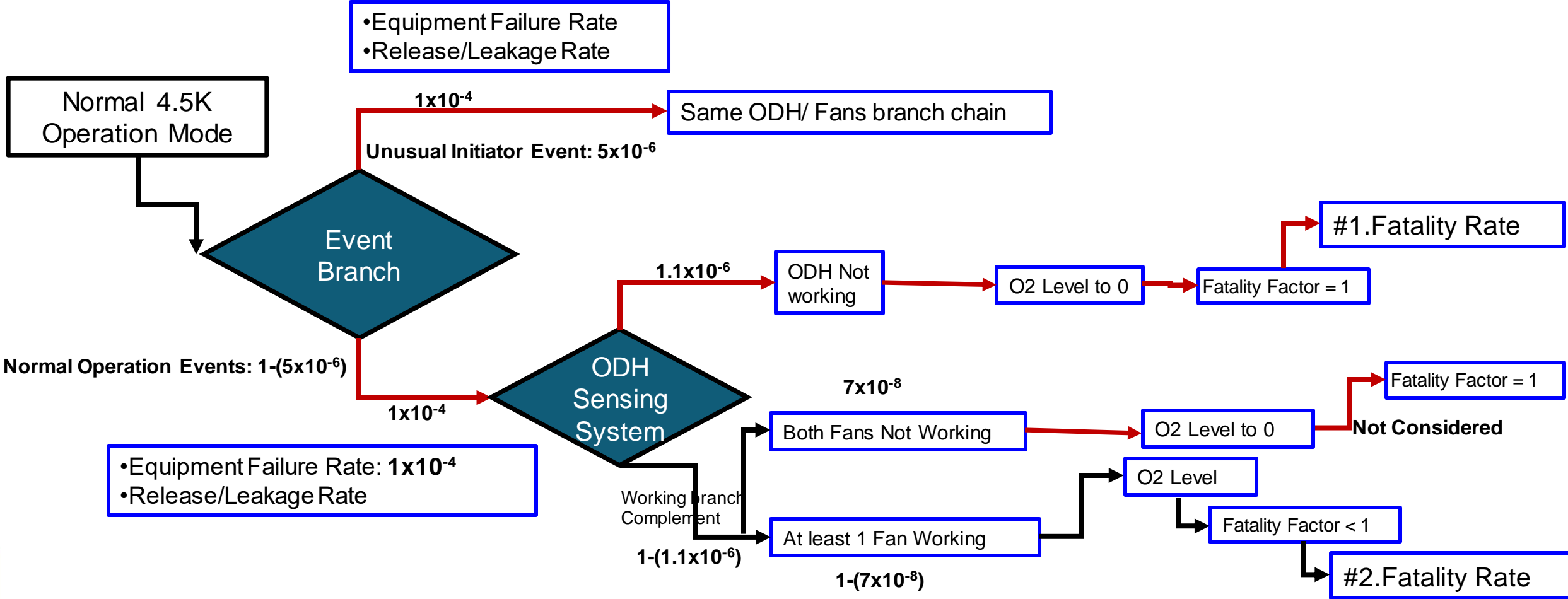
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# Outline

- Analysis methodology
- Calculation Inputs  
(Helium Inventory, Building info and components info)
- Normal operation/Unusual Events Initiator
- Components failure and release rate
- Results for different operating modes,  
with and without ventilation
- Conclusion

# Analysis Methodology

# Probability Tree



# Calculation Inputs

# Valve Stem & Valve bonnet



# Leakage during 1004B valve box event

- Man cover diameter 44.5"
- Assumed 16 Ruptures of 0.08" along the perimeter of the O-ring
- Total leak area 0.315 Inch<sup>2</sup>
- Bellow Rupture is result of sputtering.
- Bello hole is measured and found to be 0.5X0.25 Inch<sup>2</sup>





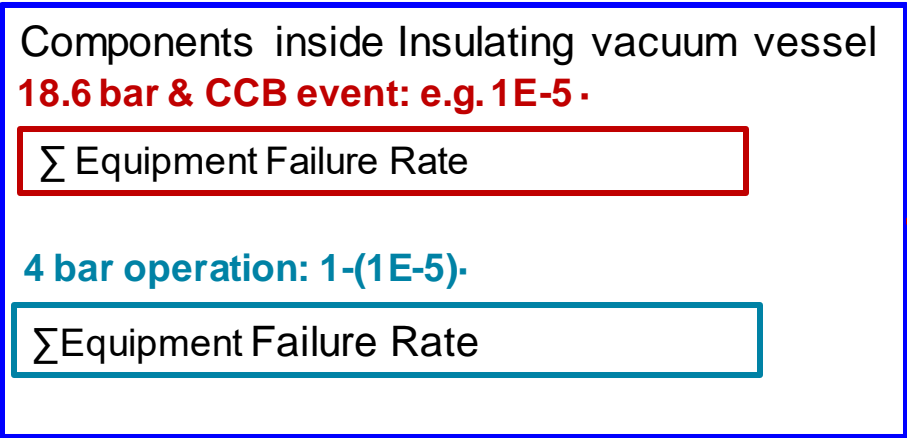


# Normal event and unusual events leak rates

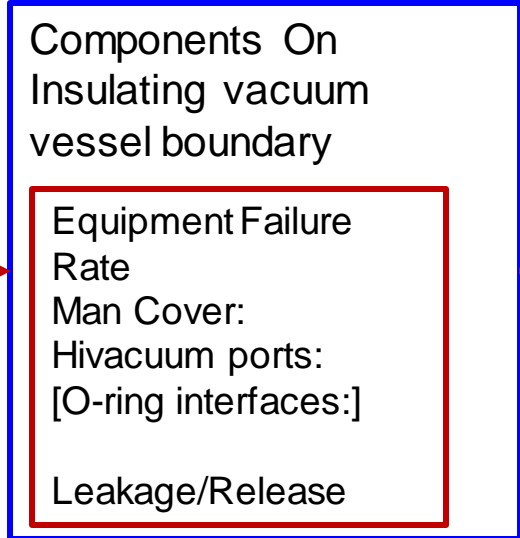
Line	Components	Leak Area Inch <sup>2</sup>	Molar Flow Release Rate	
			Normal operation event	Unusual initiator event
			SCFM	SCFM
M Line	Valve stem seal Leak 0.5" dia and 0.002" gap	3.14E-03	135.3	210.1
	Valve Bonnet Flange leak, 2.5" dia with 0.002: gap	1.57E-02	676.4	1050.7
	150 Lead Ceramic/SS304Cap Rupture	6.65E-03	286.4	444.8
	12x150 Lead helium line rupture	6.65E-03	286.4	444.8
	1600A Lead Leak: Flange Interface Norel/G10 Insulator	1.80E-03	77.5	120.4
	1600A Lead Flange o-ring failure: Flange gap: 0.002" x 2.5 inch diameter (3.38" Flange), oring dia 1.786	1.12E-02	483.2	750.7
	1600A Lead: Helium lead cooling return tube rupture: 3/8" OD x 0.035" WT	1.80E-03	77.5	120.4
	6300A Lead Leak: Norel/G10 Insulator flange	1.88E-02	807.4	1254.2
	6300A Lead Flange o-ring failure: Flange gap: 0.002" x 2.5 inch diameter (3.38" Flange) oring dia 1.86	1.17E-02	503.2	781.8
	6300A Lead: Helium lead cooling return tube rupture: 3/8" OD x 0.035" WT	1.32E-02	568.4	883.0
	Relief valve flange connection	1.32E-02	568.2	882.6
1/4" Tube Instrument Line	1.57E-03	67.6	105.1	
Ball Valve	3.14E-03	135.3	210.1	
H Line	Valve stem seal	3.14E-03	59.8	66.3
	Valve Bonnet	1.57E-02	298.8	331.3
	Relief valve flange connection	1.32E-02	251.0	278.3
	1/4" Tube Instrument Line	1.57E-03	29.9	33.1
	Ball Valve	3.14E-03	59.8	66.3
S Line	Valve stem seal	3.14E-03	120.6	210.1
	Valve Bonnet	1.57E-02	602.8	1050.7
	Capped Bayonet (0.75" NPS ) with small 250 psig relief	4.71E-03	180.9	315.2
	Relief valve flange connection	1.32E-02	506.4	882.6
	1/4" Tube Instrument Line	1.57E-03	60.3	105.1
U Line	Ball Valve	3.14E-03	120.6	210.1
	Valve stem seal	3.14E-03	15.4	210.1
	Valve Bonnet	1.57E-02	77.2	1050.7
	Relief valve flange connection	1.32E-02	64.8	882.6
	1/4" Tube Instrument Line	1.57E-03	7.7	105.1
R Line	Ball Valve	3.14E-03	15.4	210.1
	Valve stem seal	3.14E-03	15.4	210.1
	Valve Bonnet	1.57E-02	77.2	1050.7
	Relief valve flange connection	1.32E-02	64.8	882.6
	1/4" Tube Instrument Line	1.57E-03	7.7	105.1
INSULATING VESSEL	Ball Valve	3.14E-03	15.4	210.1
			SCFM	SCFM
	Mancover+Bellow	0.44	1769	1769
	HiVacuum Pumpout Port: Turbo and vacuum gages ports	0.057	227.4	227.4

# Normal operation/Unusual Events Initiator

# Probability Tree

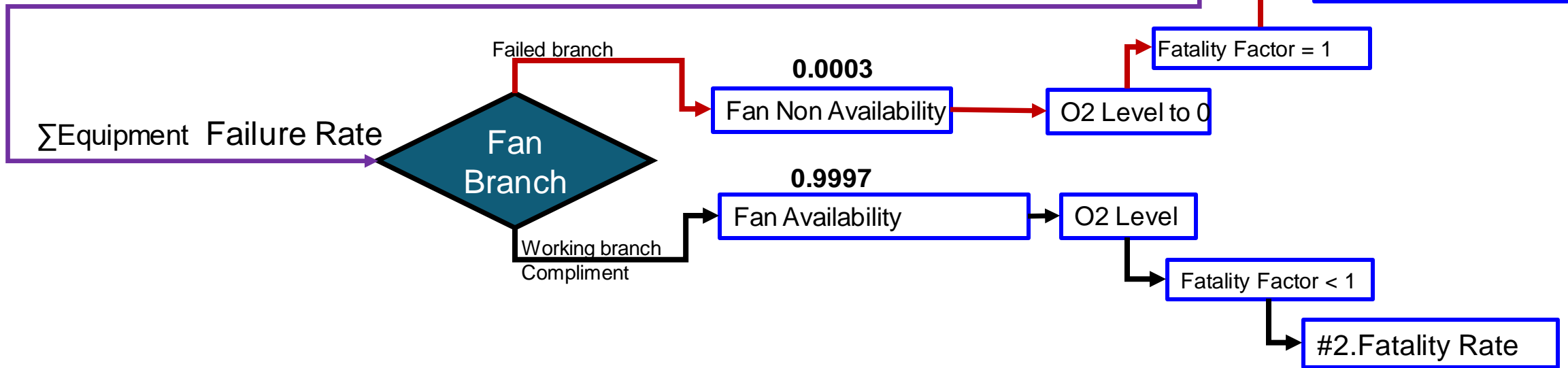


$\Sigma$  Equipment Failure Rate



Components inside Insulating vacuum vessel failing and leading to releasing via components failing on the insulating vacuum boundaries

#1. Fatality Rate



# Results

# 4.5K case, Fatality rate without ODH Fan

Building	Gross [Feet <sup>3</sup> ]	Equipment [Feet <sup>3</sup> ]	Net [Feet <sup>3</sup> ]	Min O2 level	Fatality rate	ODH class
1004B	86433	13309	73124	0	6.34E-04	2
1006B	71176	2280	68896	0	8.81E-04	2
1008B	57843	3345	54498	0	5.75E-04	2
1010A	85877	4885	80991	0	6.57E-04	2
1012A	86128	2614	83514	0	6.47E-04	2
1002B	74362	3310	71052	0	5.75E-04	2
Auxiliary Buildings for largest leak						
1004E	3000	20	2980	0	1.3E-8	0
1010Mez	10500	1200	9300	0	2E-8	0

# 4.5K case, 1 ODH fan is working at 80% capacity

Building	Gross [Feet <sup>3</sup> ]	Equipment [Feet <sup>3</sup> ]	Net [Feet <sup>3</sup> ]	ODH capacity for Fan 0.8 capacity	Leak rate SCFM	Min O2 level	Fatality rate	ODH class
1004B	86433	13309	73124	12264	1769.0	18.0%	7.75E-10	0
1006B	71176	2280	68896	13040	1769.0	18.2%	1.08E-09	0
1008B	57843	3345	54498	12960	1769.0	18.1%	7.02E-10	0
1010A	85877	4885	80991	8144	1769.0	16.4%	8.25E-10	0
1012A	86128	2614	83514	7608	1769.0	16.1%	8.09E-10	0
1002B	74362	3310	71052	10312	1769.0	17.4%	7.04E-10	0

# 4.5K case, 2 ODH fans are working at 80% capacity

Building	Gross [Feet <sup>3</sup> ]	Equipment [Feet <sup>3</sup> ]	Net [Feet <sup>3</sup> ]	ODH capacity for 2 Fan 0.8 capacity	Leak rate SCFM	Min O2 level	Fatality rate	ODH class
1004B	86433	13309	73124	24528	1769.0	18.9%	7.74E-10	0
1006B	71176	2280	68896	26080	1769.0	18.9%	1.08E-09	0
1008B	57843	3345	54498	25920	1769.0	18.7%	7.02E-10	0
1010A	85877	4885	80991	16288	1769.0	18.7%	8.03E-10	0
1012A	86128	2614	83514	15216	1769.0	18.6%	7.90E-10	0
1002B	74362	3310	71052	20624	1769.0	18.9%	7.02E-10	0
Auxiliary Buildings with 1 ODH fan								
1004E	3000	20	2980	3000	128	9.0%	1.0E-8	0
1010Mez	10500	1200	9300	--	128	0%	2.0E-8	0

# For 45K Cooldown mode without ODH fan

Building	Gross [Feet3]	Equipment [Feet3]	Net [Feet3]	Min O2 level	Fatality rate	ODH class
1004B	86433	13309	73124	1.5%	6.34E-04	2
1006B	71176	2280	68896	1.2%	8.81E-04	2
1008B	57843	3345	54498	0.6%	5.75E-04	2
1010A	85877	4885	80991	1.9%	6.57E-04	2
1012A	86128	2614	83514	2.0%	6.47E-04	2
1002B	74362	3310	71052	1.4%	5.75E-04	2
Auxiliary Buildings for largest leak						
1004E	3000	20	2980	0%	1.3E-8	0
1010Mez	10500	1200	9300	0%	2.0E-8	0



# For 270K scrub mode without ODH fan

Building	Gross [Feet <sup>3</sup> ]	Equipment [Feet <sup>3</sup> ]	Net [Feet <sup>3</sup> ]	Min O2 level	Fatality rate	ODH class
1004B	86433	13309	73124	15.0%	6.0E-10	0
1006B	71176	2280	68896	14.7%	1.4E-09	0
1008B	57843	3345	54498	13.4%	9.4E-09	0
1010A	85877	4885	80991	15.5%	2.6E-10	0
1012A	86128	2614	83514	15.7%	2.0E-10	0
1002B	74362	3310	71052	14.9%	7.1E-10	0
Auxiliary Buildings for largest leak						
1004E	3000	20	2980	0.0%	1.3E-8	0
1010Mez	10500	1200	9300	1.6%	2E-8	0

# Conclusion

# Conclusion

- ODH evaluation has been re-done for the Service Buildings
- The service buildings require credited controls of ODH sensing & ventilation to get ODH 0 classification for 4.5K normal operational mode and 45K cooldown mode.
- During room temperature scrub service buildings falls in category of ODH 0 but O<sub>2</sub> concentration is between 13% to 16% without any ODH fan hence do not require credited controls of ODH system.
- The auxiliary buildings are in ODH 0 classification for 4.5K normal operational mode, 45K cooldown mode and room temperature scrub but O<sub>2</sub> concentration can fall to 0%.
- During room temperature scrub auxiliary buildings falls in category of ODH 0 but O<sub>2</sub> concentration is between 2% to 0%.

Thank you

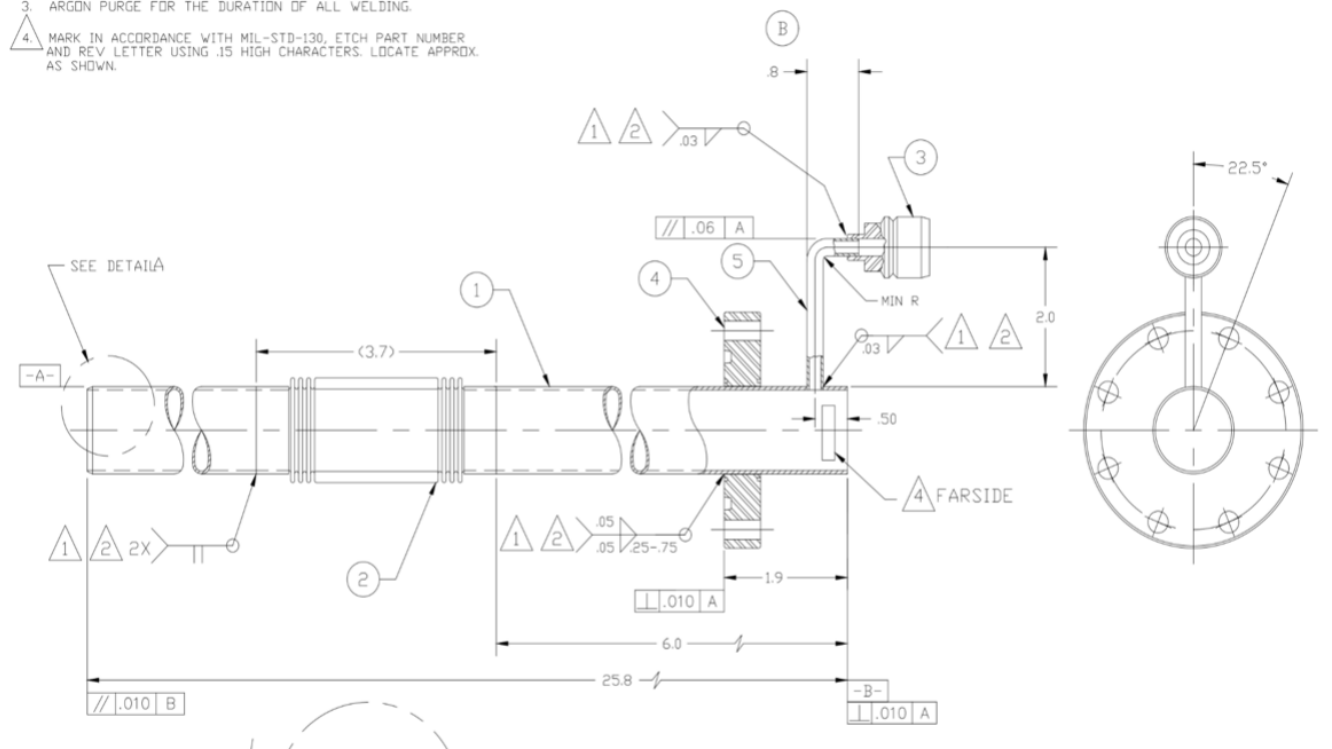
# Backup Slides

# 1600 Amp Current Lead

NOTES:

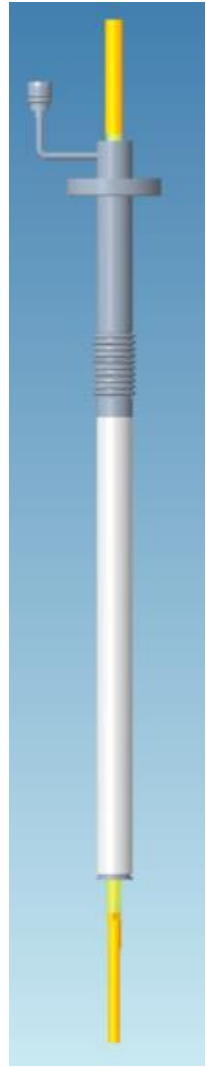
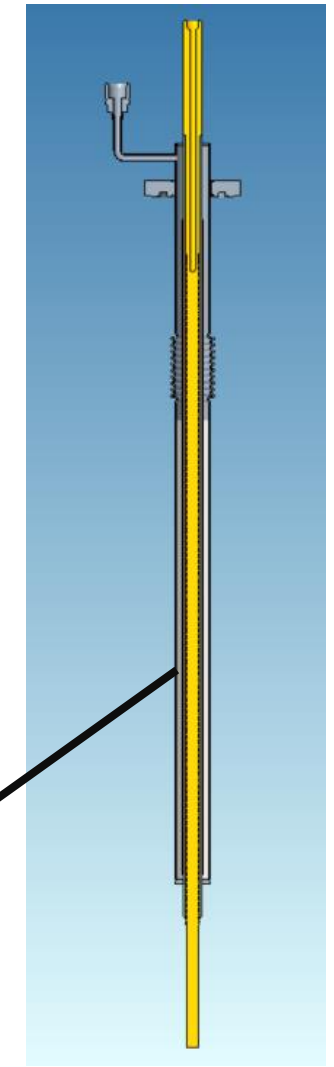
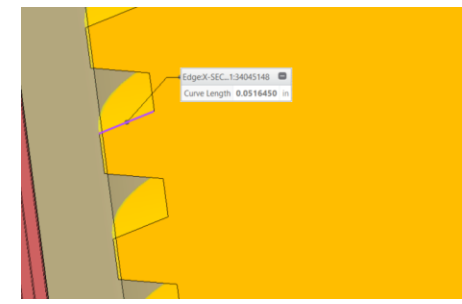
1. ALL WELDS TO BE VACUUM TIGHT, LEAK RATE NOT TO EXCEED  $1 \times 10^{-9}$  cc He/sec.
2. WELDS TO BE IN ACCORDANCE WITH ASME BOILER AND PRESSURE VESSEL CODE SECTION IX PART QW.
3. ARGON PURGE FOR THE DURATION OF ALL WELDING.
4. MARK IN ACCORDANCE WITH MIL-STD-130, ETCH PART NUMBER AND REV LETTER USING .15 HIGH CHARACTERS. LOCATE APPROX. AS SHOWN.

REVISIONS							
REV	ZONE	ECN NO.	DESCRIPTION	BY	DATE	CHK	APP
A			INITIAL RELEASE	AA	1/22/96	SN	MI
B	D	CR309	AS PER ECN	HRK	12/29/97	SN	AN



SEE SEPARATE PARTS LIST PL34045137

OUTSTANDING ECN NUMBERS	INTERPRET IN GENERAL ACCORDANCE WITH ASME Y14.24M-1989	<b>RHIC</b>	BROOKHAVEN NATIONAL LABORATORY ASSOCIATED UNIVERSITIES, INC. UPTON, N.Y. 11973
	UNLESS OTHERWISE SPECIFIED	DESIGN BY A. ARNO III 12/1/96	TITLE: POWER LEAD ASSY, TUBE VACUUM
	DIMENSIONS ARE IN INCHES DECIMAL TOLERANCES X # 26 XX # 22 XXX # 205 ANGULAR TOLERANCE ± 1°	CHECKED BY A. Nicoletti 1/17/96	SIZE C
	125/ FINISH	DESIGNED BY S. Norton 1/17/96	DRAWING NUMBER: 34045137
	BREAK SHARP EDGES MAX. 0.3 MIN. .01	APPROVED BY M. Iarocci 1/19/96	REV. B
		SA T.R. Muller 1/22/96	SA R. Alforque 1/22/96
			SA CATEGORY: A-3 SCALE: 1/1 WEIGHT: NA SHEET 1 of 1

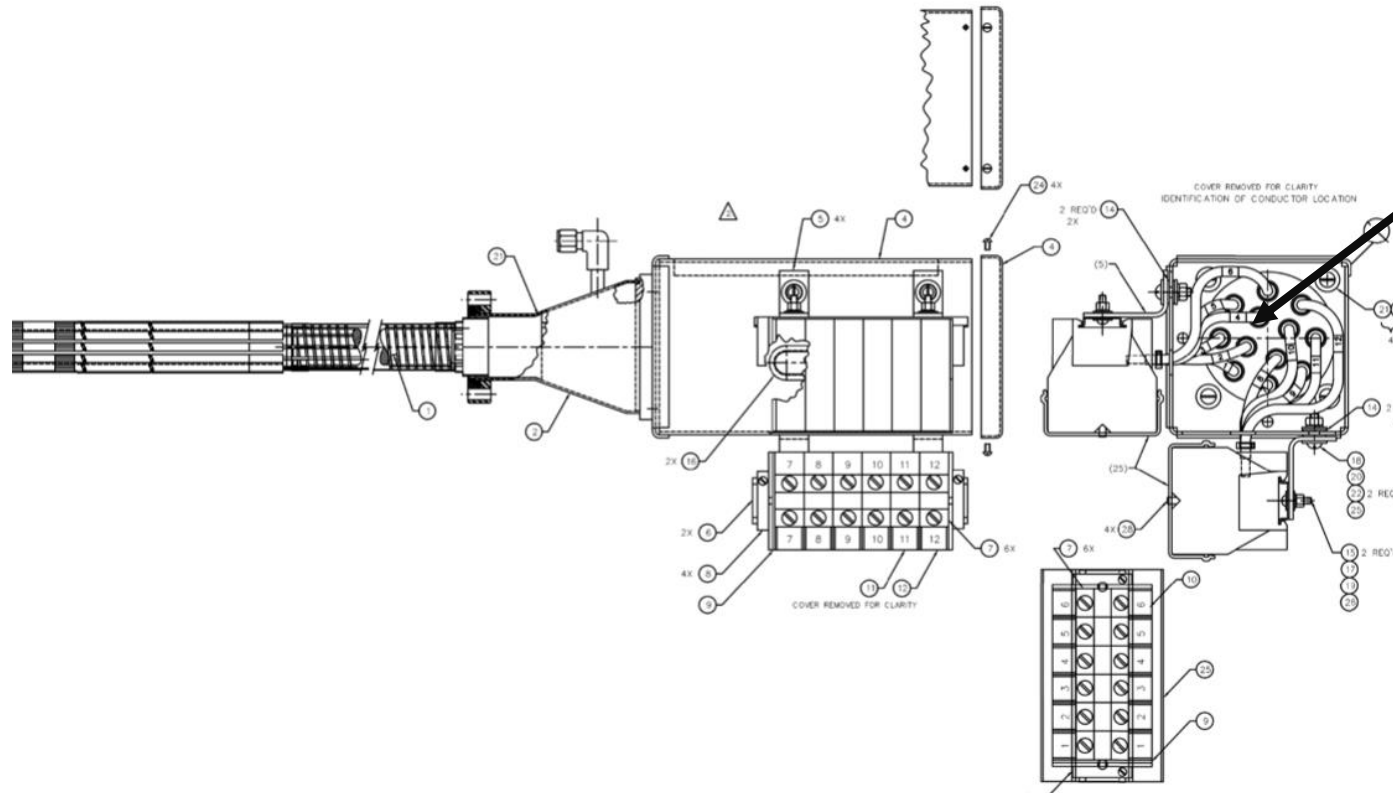


Spiral Leak  
Cross Sectional Area:  
 $0.036" \times 0.052" =$   
 $0.00187in^2$

# 150 Amp Current Lead

NOTES:  
 1. BUILD IN ACCORDANCE WITH RHIC SPEC. NO., RHIC-CR-E-3404-0082.  
 2. WELDS TO BE VACUUM TIGHT, LEAK RATE NOT TO EXCEED 10<sup>-5</sup> M TO 14/440.  
 3. APPLY ITEM 21 TO ITEM 1 APPROX AS SHOWN, BEFORE INSERTING ITEM 2 INTO ITEM 1.  
 4. MARK IN ACCORDANCE WITH MIL-STD-133, AND TAG WITH PART NO. AND APPLICABLE REV LETTER.

REV	DATE	DESCRIPTION	BY	CHKD
1		ISSUED FOR FAB		

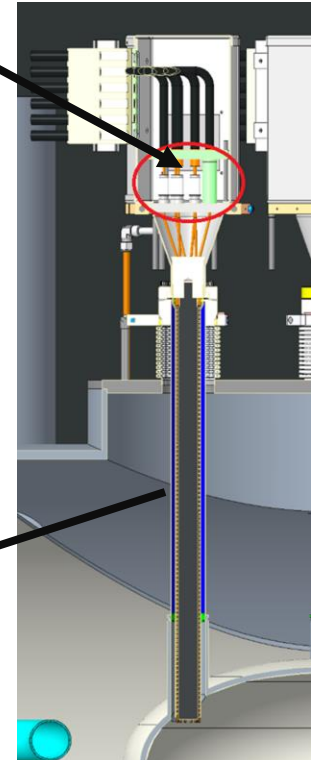
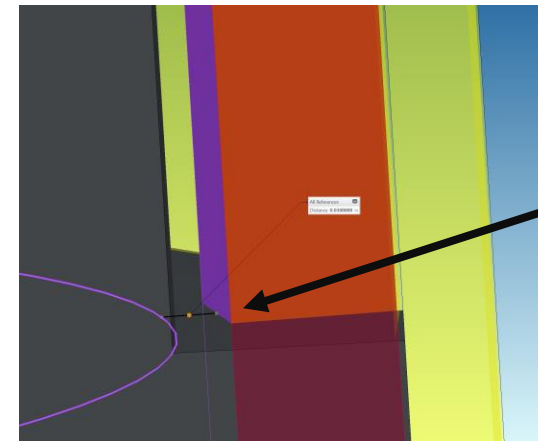


REV	DATE	DESCRIPTION	BY	CHKD
1		ISSUED FOR FAB		

REV	DATE	DESCRIPTION	BY	CHKD
1		ISSUED FOR FAB		

Leak through ceramic break will see same amount of He flow as the Spiral Leak since they share the same flow path.



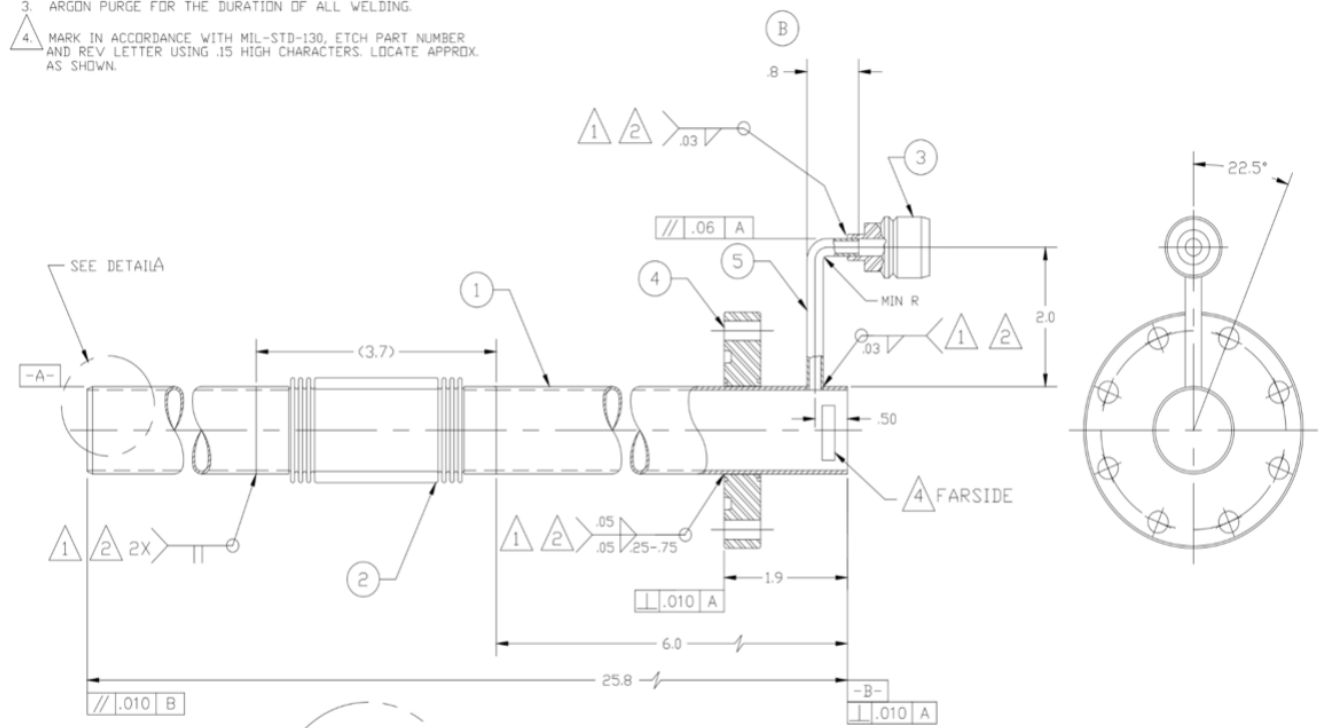
Spiral Leak  
 Cross Sectional Area:  
 $0.035'' \times 0.19'' = 0.00665 \text{in}^2$

# 1600 Amp Current Lead

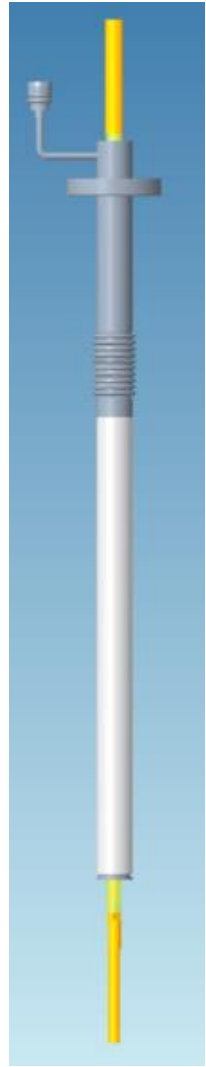
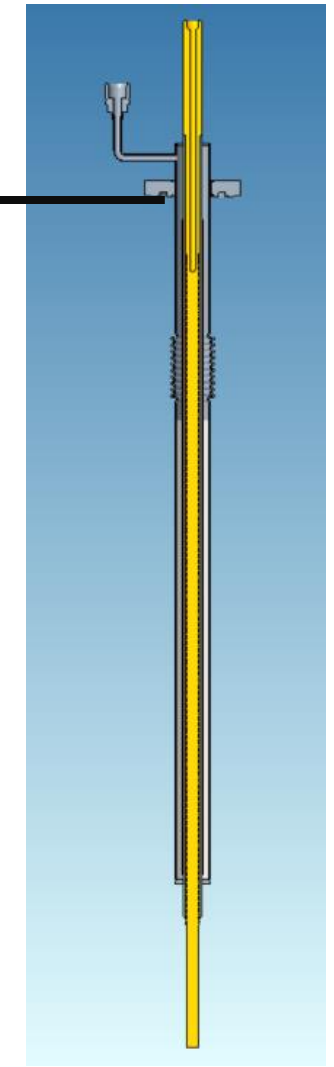
NOTES:

1. ALL WELDS TO BE VACUUM TIGHT, LEAK RATE NOT TO EXCEED  $1 \times 10^{-9}$  cc He/sec.
2. WELDS TO BE IN ACCORDANCE WITH ASME BOILER AND PRESSURE VESSEL CODE SECTION IX PART QW.
3. ARGON PURGE FOR THE DURATION OF ALL WELDING.
4. MARK IN ACCORDANCE WITH MIL-STD-130, ETCH PART NUMBER AND REV LETTER USING .15 HIGH CHARACTERS. LOCATE APPROX. AS SHOWN.

REVISIONS					
REV	ZONE	ECN NO.	DESCRIPTION	BY	DATE
A			INITIAL RELEASE	AA	1/22/96
B	D	CR309	AS PER ECN	HRK	10/29/97



Flange Leak  
 Dia 1.786", Gap 0.002"  
 Leak Area 0.012 Inch<sup>2</sup>



SEE SEPARATE PARTS LIST PL34045137

OUTSTANDING ECN NUMBERS	INTERPRET IN GENERAL ACCORDANCE WITH ASME Y14.24M-1989	<b>RHIC</b>	BROOKHAVEN NATIONAL LABORATORY ASSOCIATED UNIVERSITIES, INC. UPTON, N. Y. 11973
	UNLESS OTHERWISE SPECIFIED	DESIGN BY A. ARNO III 12/1/96	TITLE: POWER LEAD ASSY, TUBE VACUUM
	DIMENSIONS ARE IN INCHES DECIMAL TOLERANCES X # 26 XX # 22 XXX # 20 ANGULAR TOLERANCE ± 1°	CHECKED BY S. Norton 1/17/96	SIZE C
	125/ FINISH	DESIGNED BY A. Nicoletti 1/17/96	DRAWING NUMBER: 34045137
	BREAK SHARP EDGES MAX .03 MIN .01	APPROVED BY M. Iarocci 1/19/96	REV. B
		SA APPROVAL T.R. Muller 1/22/96	SA CATEGORY: A-3
		R. Alforque 1/22/96	SCALE: 1/1
			WEIGHT: NA
			SHEET 1 of 1







# Flanges {Relief pipe}

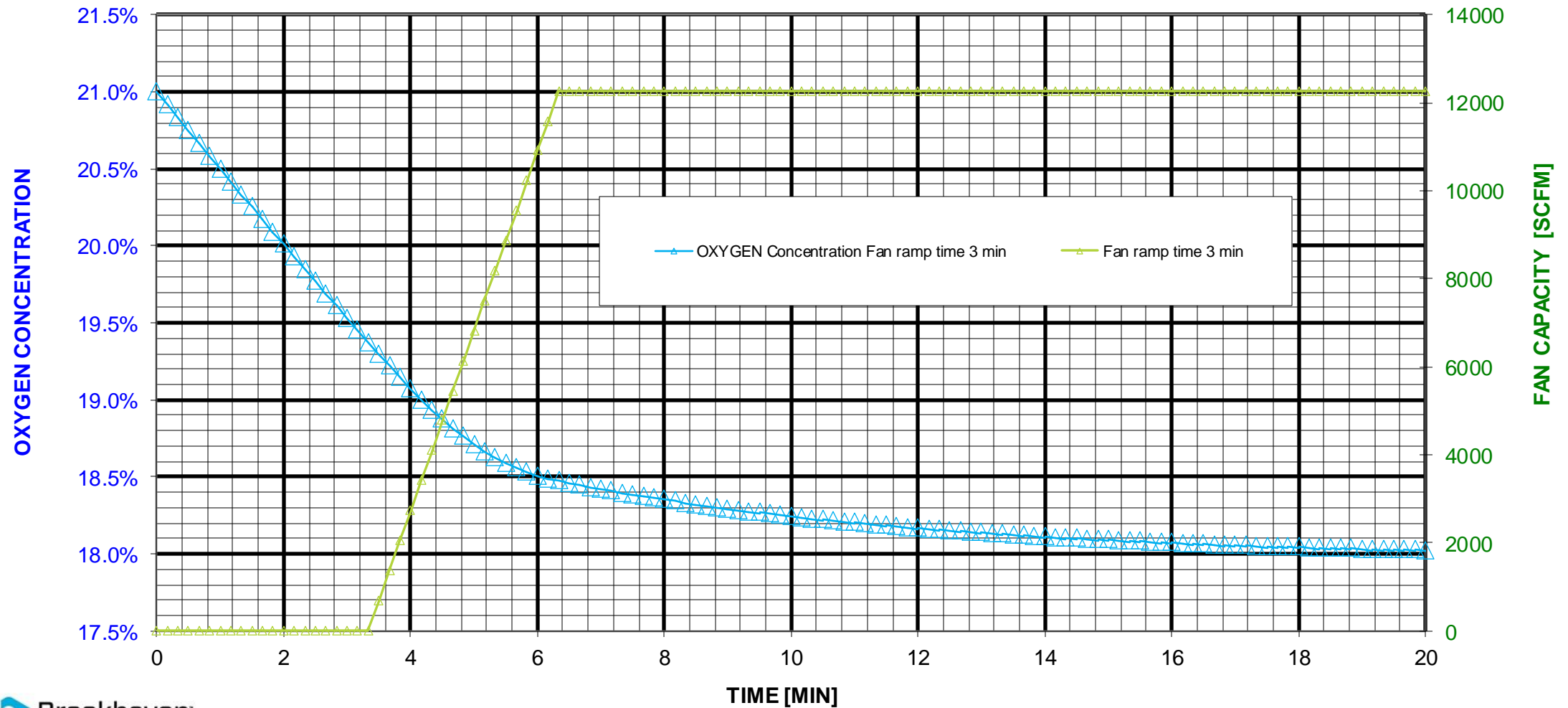
Dia 2.1" Gap 0.002"

Relief Area 0.0132 Inch<sup>2</sup>



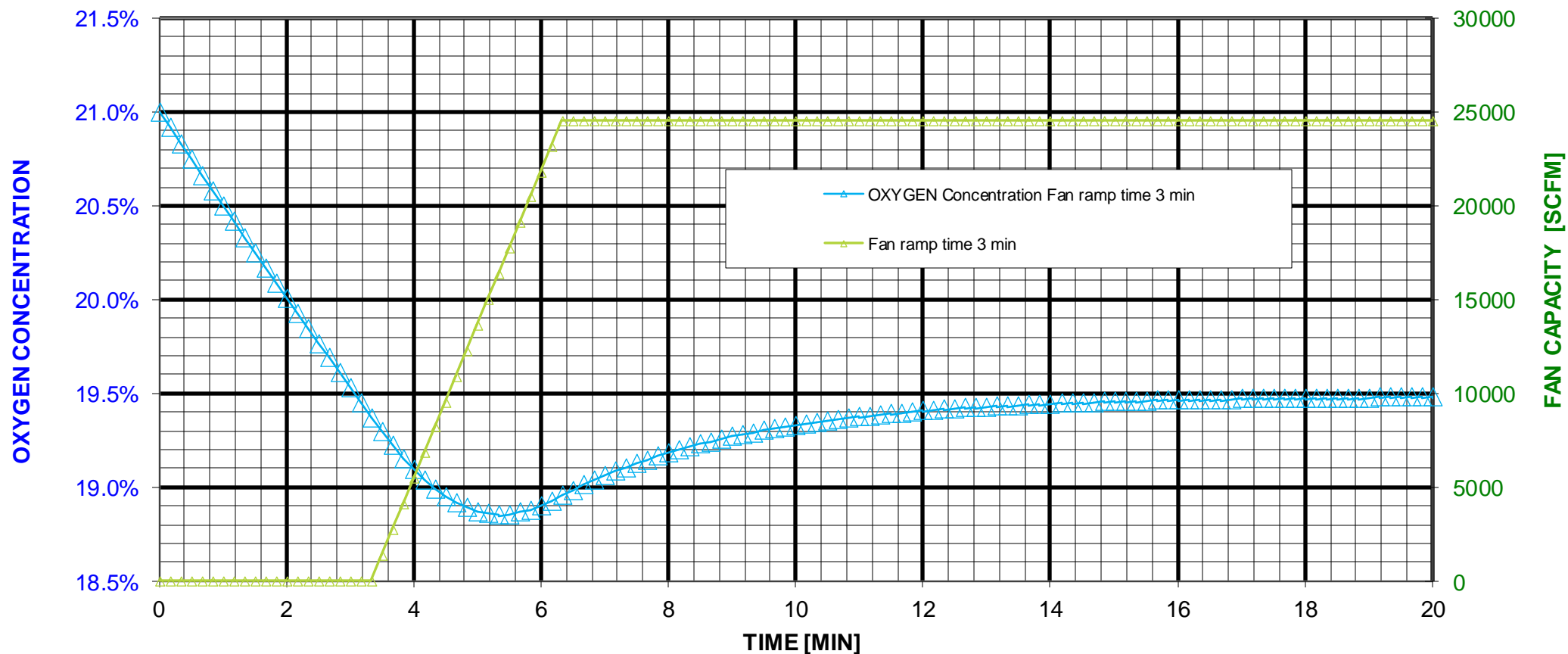
# 1004B transient for 1 ODH fan

Minimum O2 concentration: 17.97 %

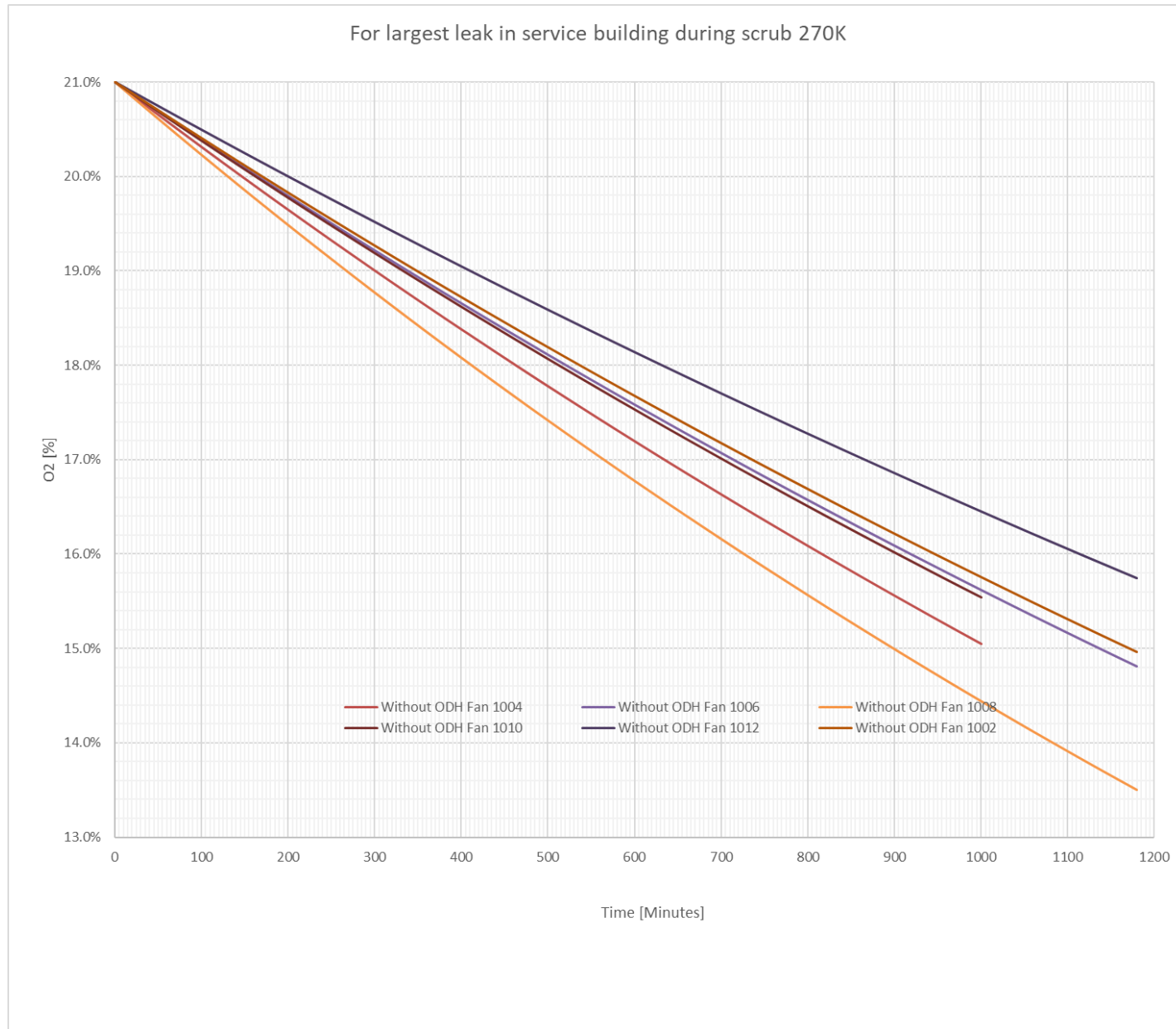


# 1004B transient for 2 ODH fan

Minimum O2 concentration: 18.86 %

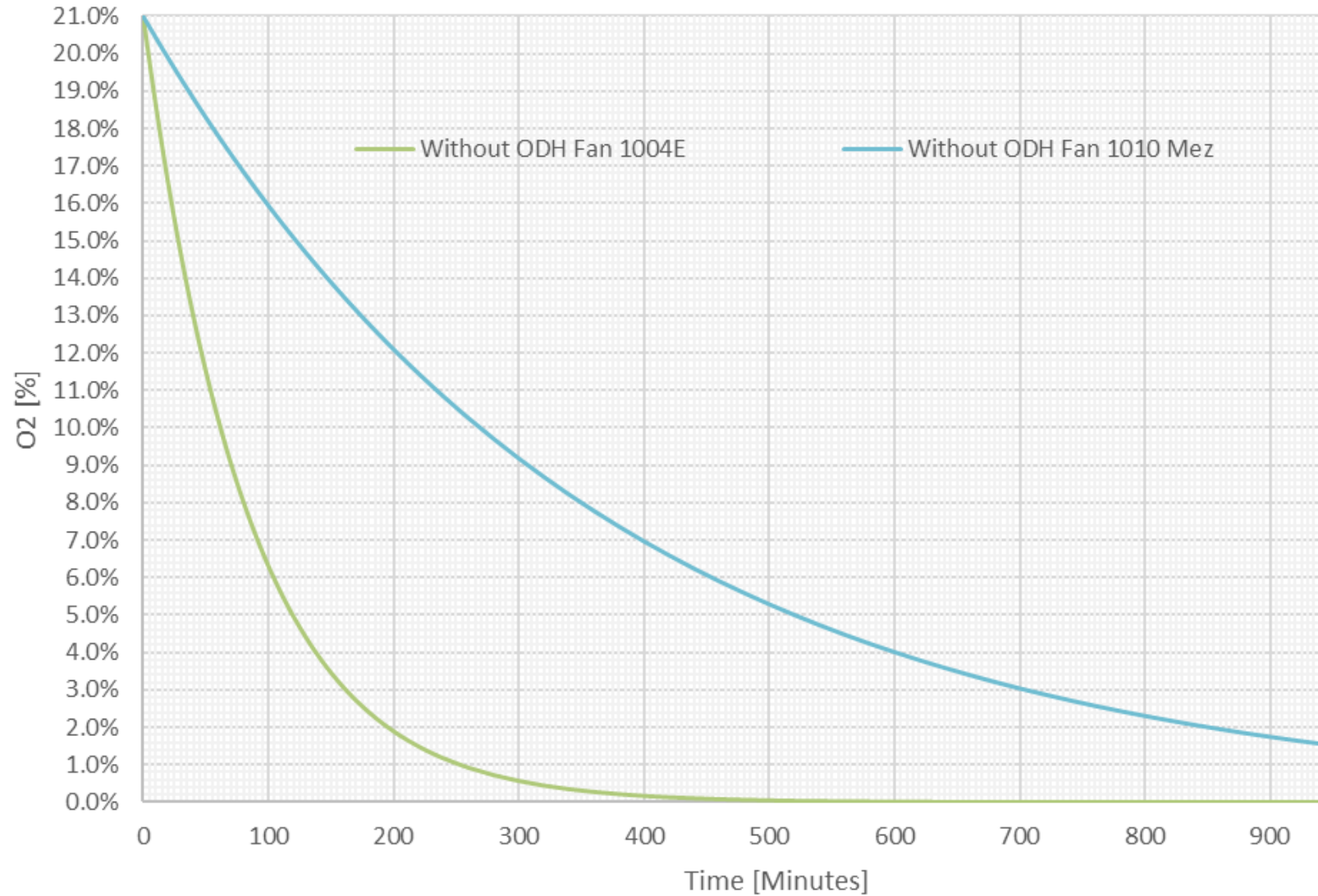


# For 270K scrub mode without ODH fan



Maximum leak rate is  
24.4 SCFM  
Total inventory  
24,394 CF.

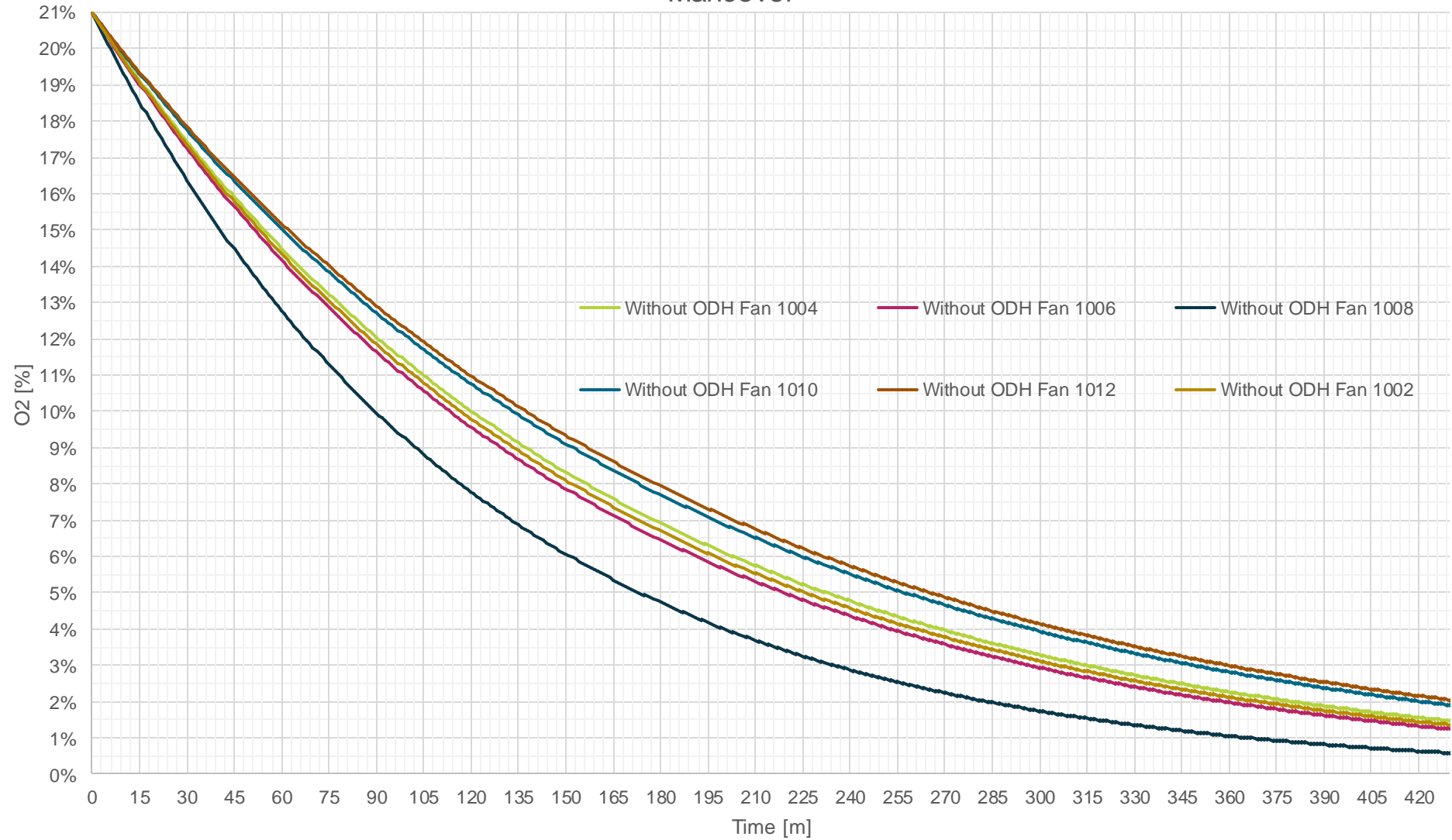
### For largest leak in auxiliary building during scrub 270K



Maximum leak rate is 25.6 SCFM  
Total inventory 24,394 CF

# 45 K cooldown mode ODH Results

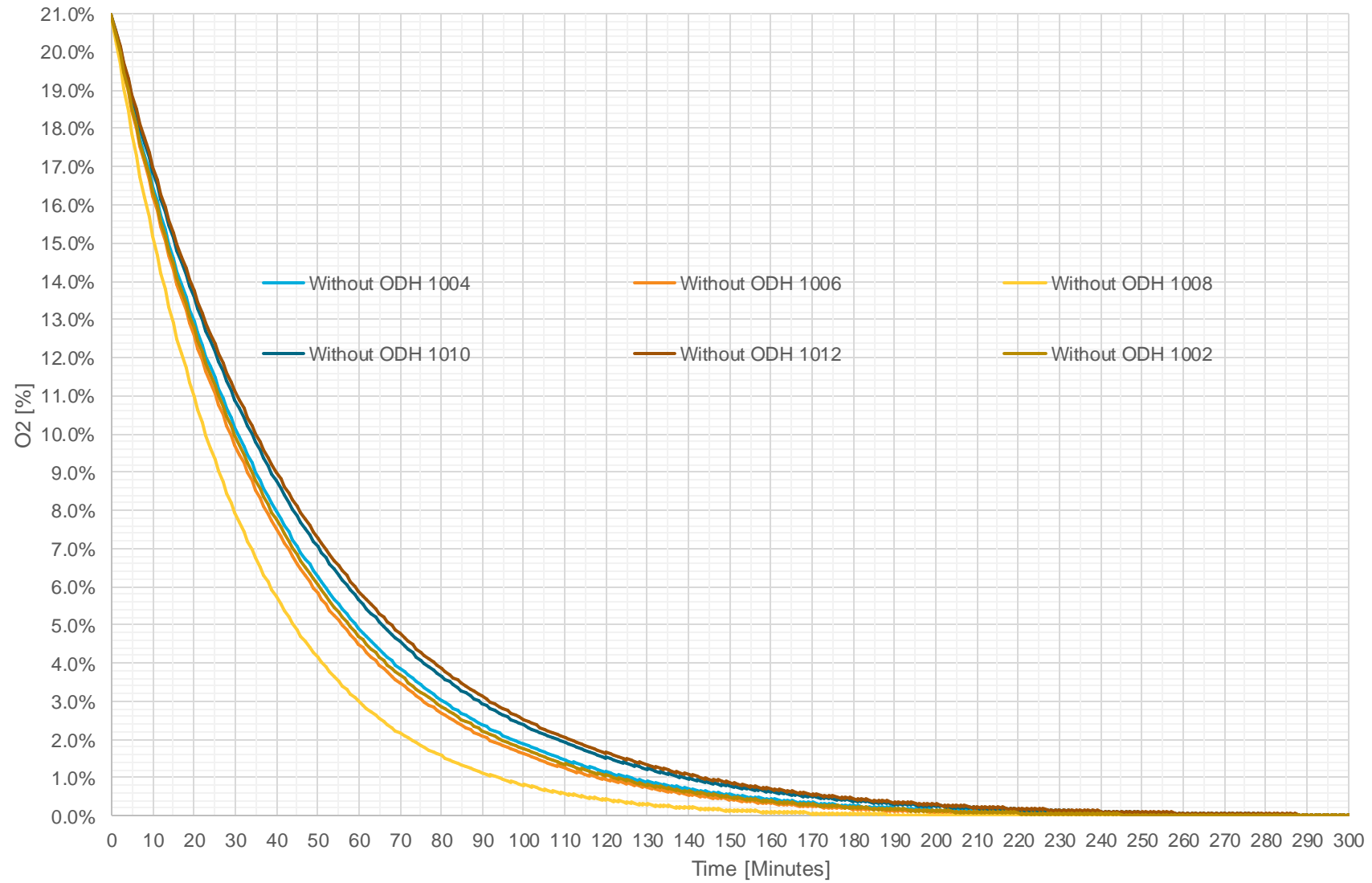
Mancover





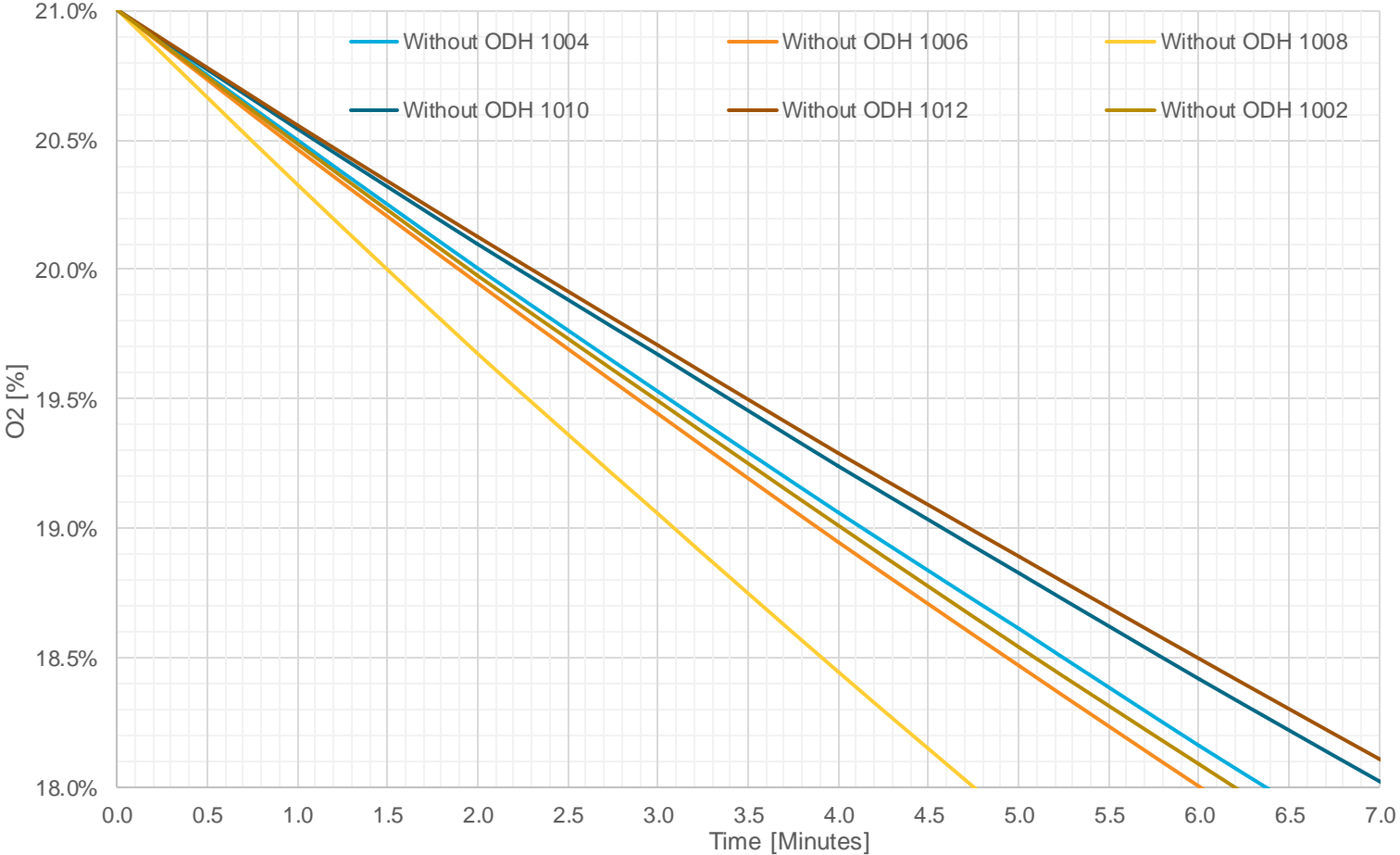
# O2 concentration without ODH fan

Mancover+Bellow



# O2 concentration without ODH fan

Mancover+Bellow

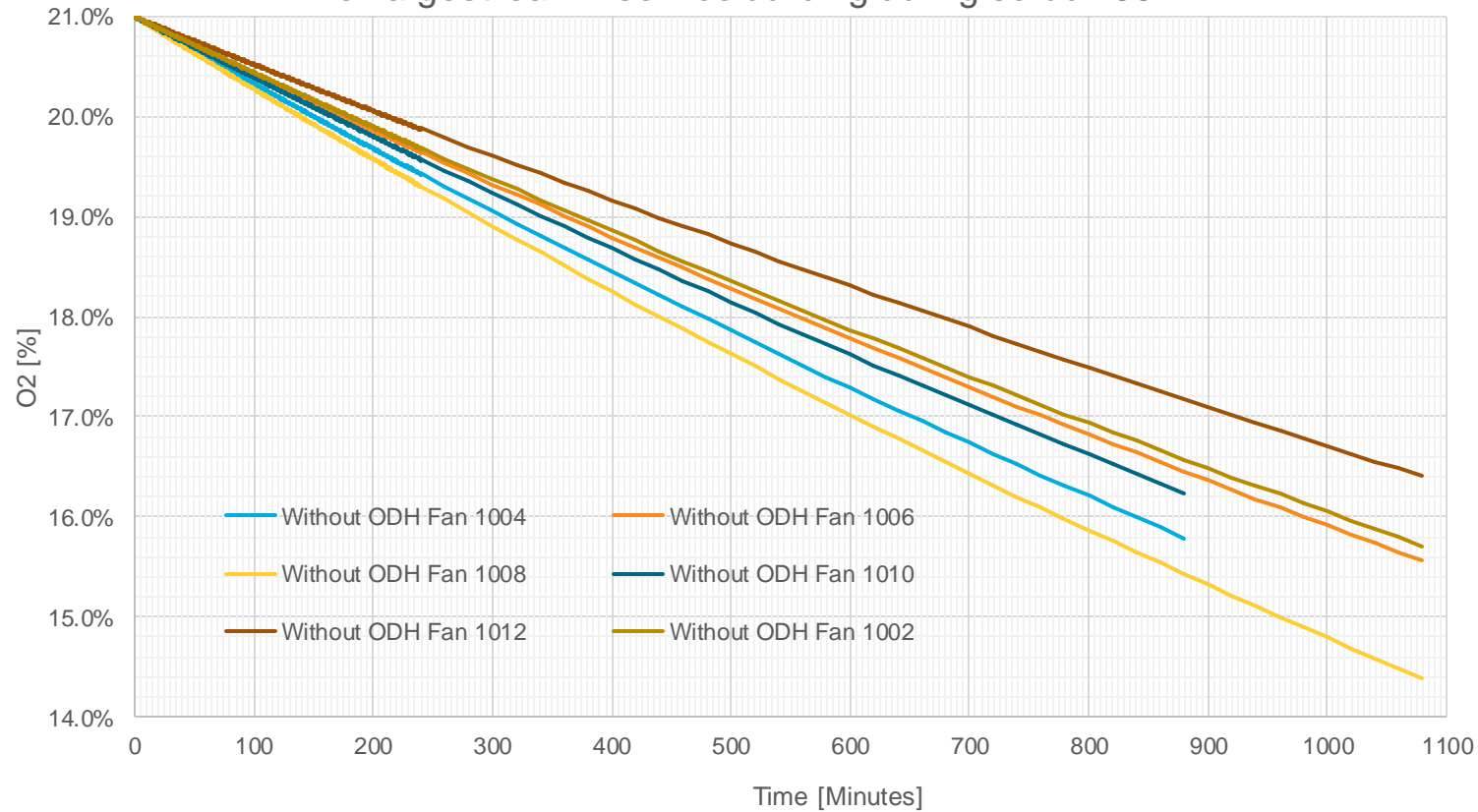


# For 285K scrub mode without ODH fan

Building	Gross [Feet <sup>3</sup> ]	Equipment [Feet <sup>3</sup> ]	Net [Feet <sup>3</sup> ]	Min O2 level	Fatality rate	ODH class
1004B	86433	13309	73124	15.0%	1.7E-10	0
1006B	71176	2280	68896	15.3%	3.9E-10	0
1008B	57843	3345	54498	14.1%	2.1E-09	0
1010A	85877	4885	80991	16.1%	8.1E-11	0
1012A	86128	2614	83514	16.2%	6.5E-11	0
1002B	74362	3310	71052	15.5%	2.0E-10	0
Auxiliary Buildings for largest leak						
1004E	3000	20	2980	0.02%	1.3E-8	0
1010Mez	10500	1200	9300	1.86%	2E-8	0

# For 285K scrub mode without ODH fan

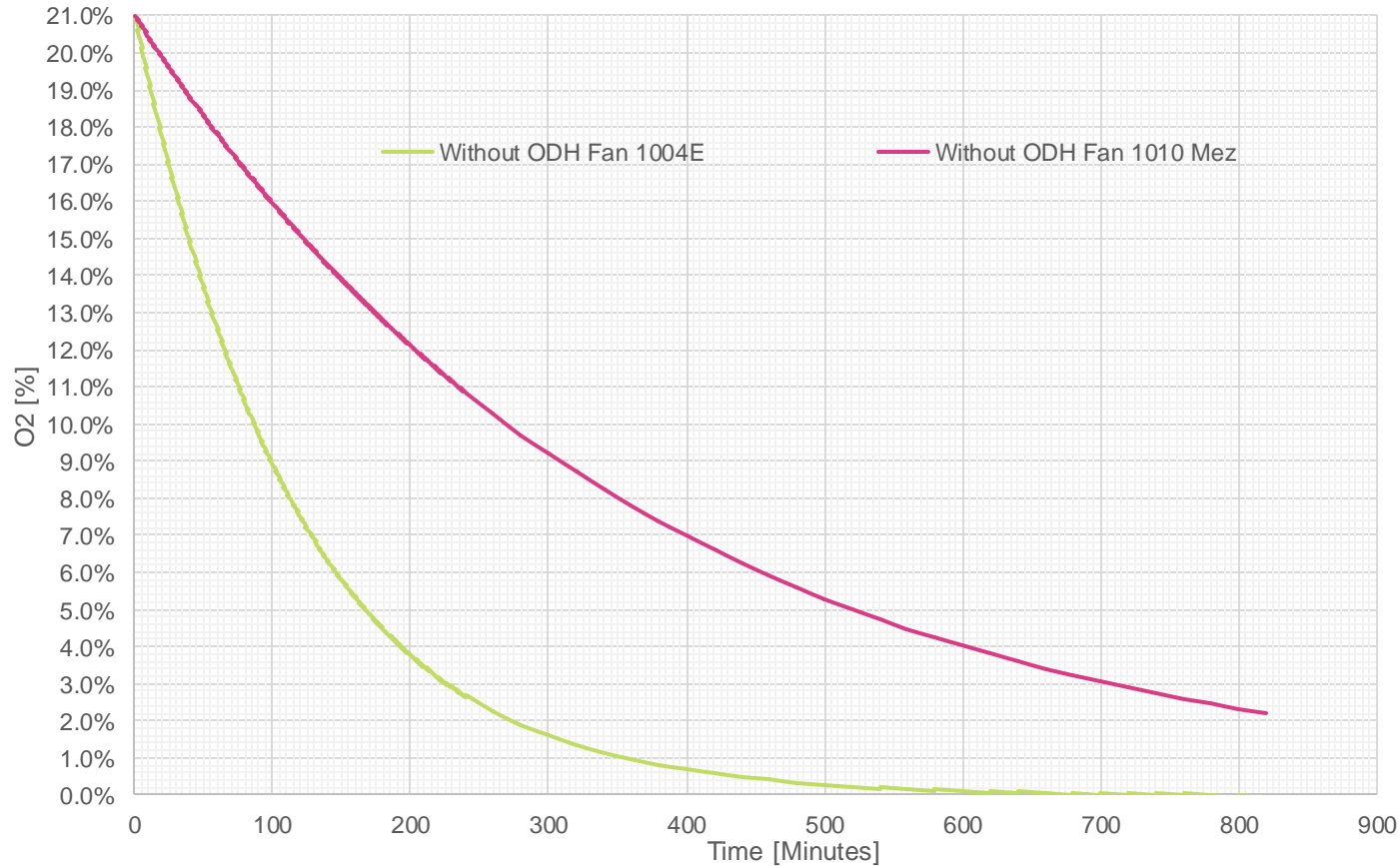
For largest leak in service building during scrub 285K



Maximum leak rate is  
23.7 SCFM  
Total inventory  
21,000 CF.

# For Auxiliary building without ODH fan

For largest leak in auxiliary building during scrub 285K



Maximum leak rate is  
25.6 SCFM  
Total inventory  
21,000 CF.

# Probability of failure of vacuum insulation

<b># of Components</b>	<b>200</b>
Failure Probability	1.00E-09
SC bus short probability	5.00E-05
<b>Event Probability</b>	<b>5.02E-05</b>

# ODH Classifications

Fatality Rate less than  $< 10^{-7}$  /hr

O<sub>2</sub> Concentration  $\geq 14\%$

ODH 0: Posting & training

Based on the ODH Classification, the Department Chair /Division Manager or designee establishes and maintains the minimum controls required as follows:

ODH Classification	Controls
0	Postings Training
1	Postings Training (including practical demonstration of personal protective equipment [PPE]) PPE: <ul style="list-style-type: none"> <li>• Personal Oxygen Monitor</li> <li>• Self-Rescue Respirator (Supplied Atmosphere)</li> </ul>

**Step 1** Based on the minimum oxygen concentration, the Department Chair /Division Manager or designee establishes and maintains the minimum controls required as follows:

Oxygen Concentration	Controls
$\geq 14\%$	Controls Required by ODH Classification (step 2).
$\geq 10\% < 14\%$	Controls Required by ODH Classification (step 2) plus ODH Monitoring (either fixed area or POM) that alarms locally.
$< 10\%$	Controls Required by ODH Classification (step 2) plus ODH Monitoring that provides alarms/indication both locally and before entering the area.

Alarms must be perceptible in the environment used (e.g., visual or vibration in high noise areas).

**Note:** Ensure to incorporate the impact from added monitoring to the ODH Classification process.

Fatalities / Hr.	ODH Classification
$10^{-9}$ (i.e., Oxygen concentration not less than 18%)	No Classification Required
$>0$ but $<10^{-7}$ (Note 1)	0
$\geq 10^{-7}$ but $<10^{-5}$	1
$\geq 10^{-5}$ but $<10^{-3}$	2
$\geq 10^{-3}$ but $<10^{-1}$	3
$\geq 10^{-1}$	4

# Helium Inventory in RHIC

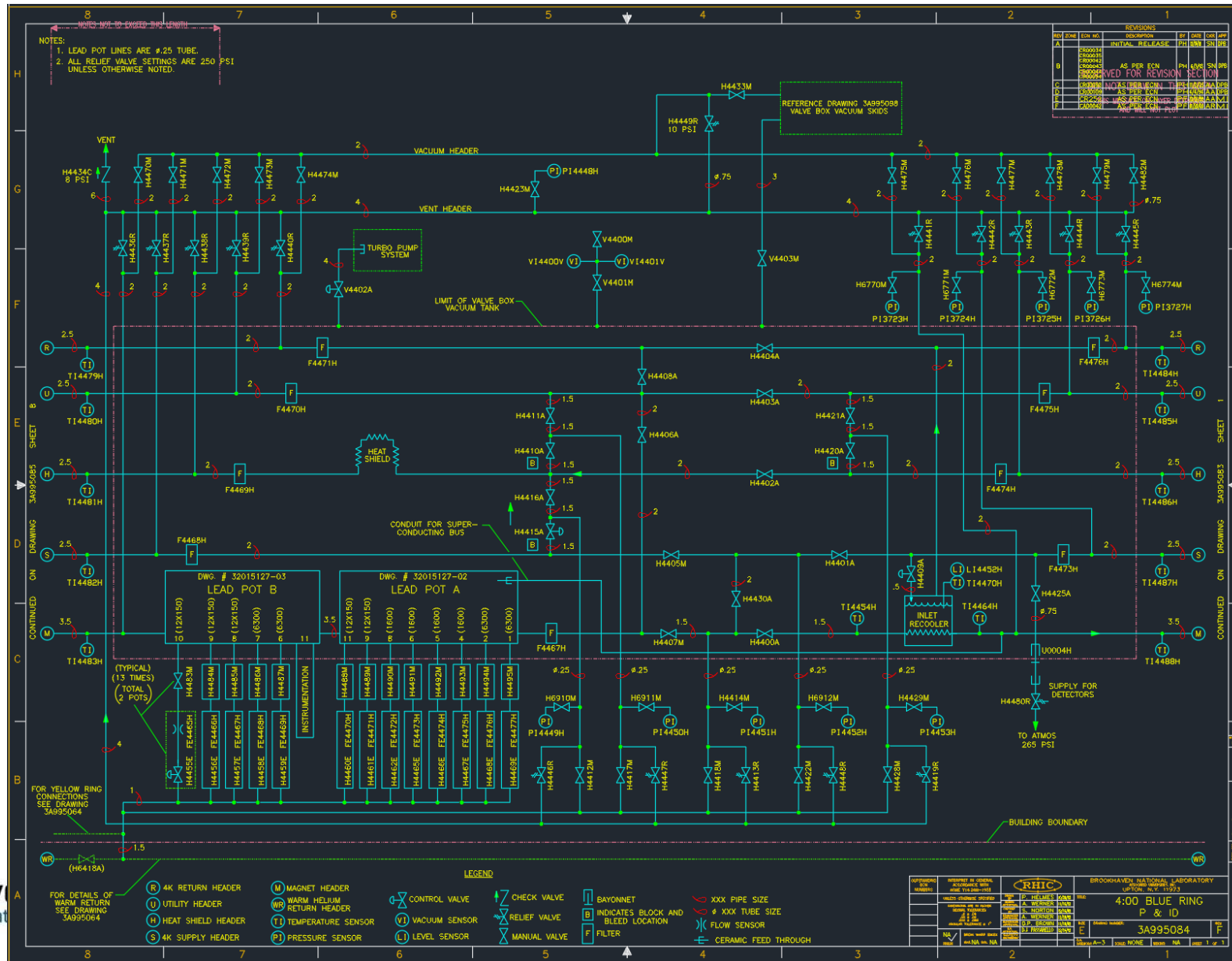
Mode	Magnet Circuit [SCF]	R, U, S, H [SCF]	1-Ring [SCF]	2-Rings [SCF]	Plant [SCF]	Total [SCF]
Scrub	525	385	5,463	10,927	13,467	24,394
45K Wave	9,844	7,219	102,381	204,763	54,615	259,378
4.5K Mode	302,717	55,498	2,149,294	4,298,588	286,381	4,584,969
Warmup Drift 45K	756	555	7,866	15,732	0	15,732



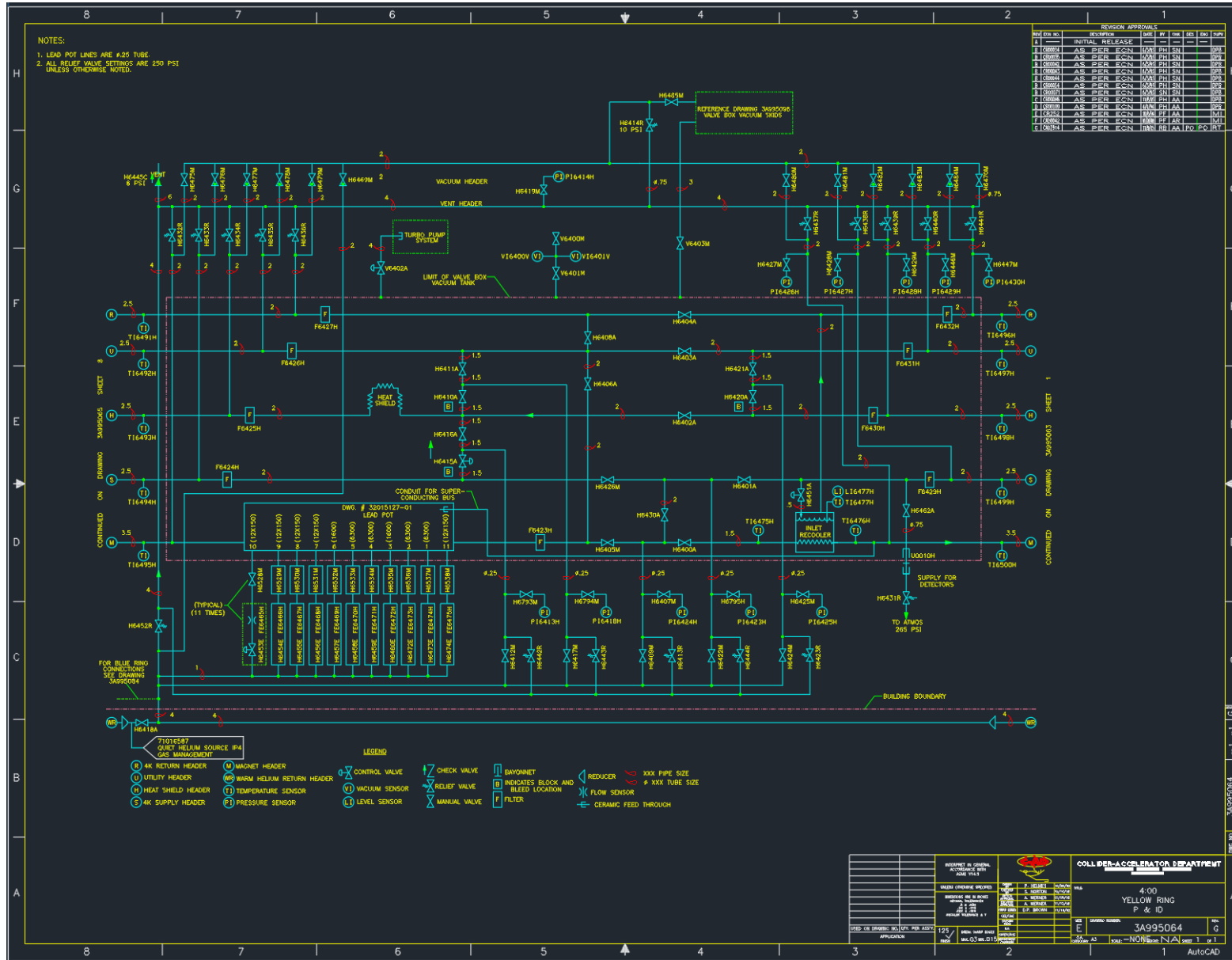
# Normal event and unusual events process parameters

	Conditions during failure events under Normal Operational Mode branch		Conditions during failure events under Unusual Initiator Mode branch	
Process circuit	Normal Pressure (Bar)	Normal Temperature (K)	Event Pressure (Bar)	Event Temperature (K)
M Line	4	4.8	18.6	10
H Line	15	45	18.6	56
S Line	3.5	4.8	18.6	10
U Line	1.3	4.8	18.6	10
R Line	1.3	4.8	18.6	10

# 1004B – Blue Valve Box P&ID



# 1004B – Yellow Valve Box P&ID



# 1006B transient for 1 ODH fan

CASE: HELIUM MODE

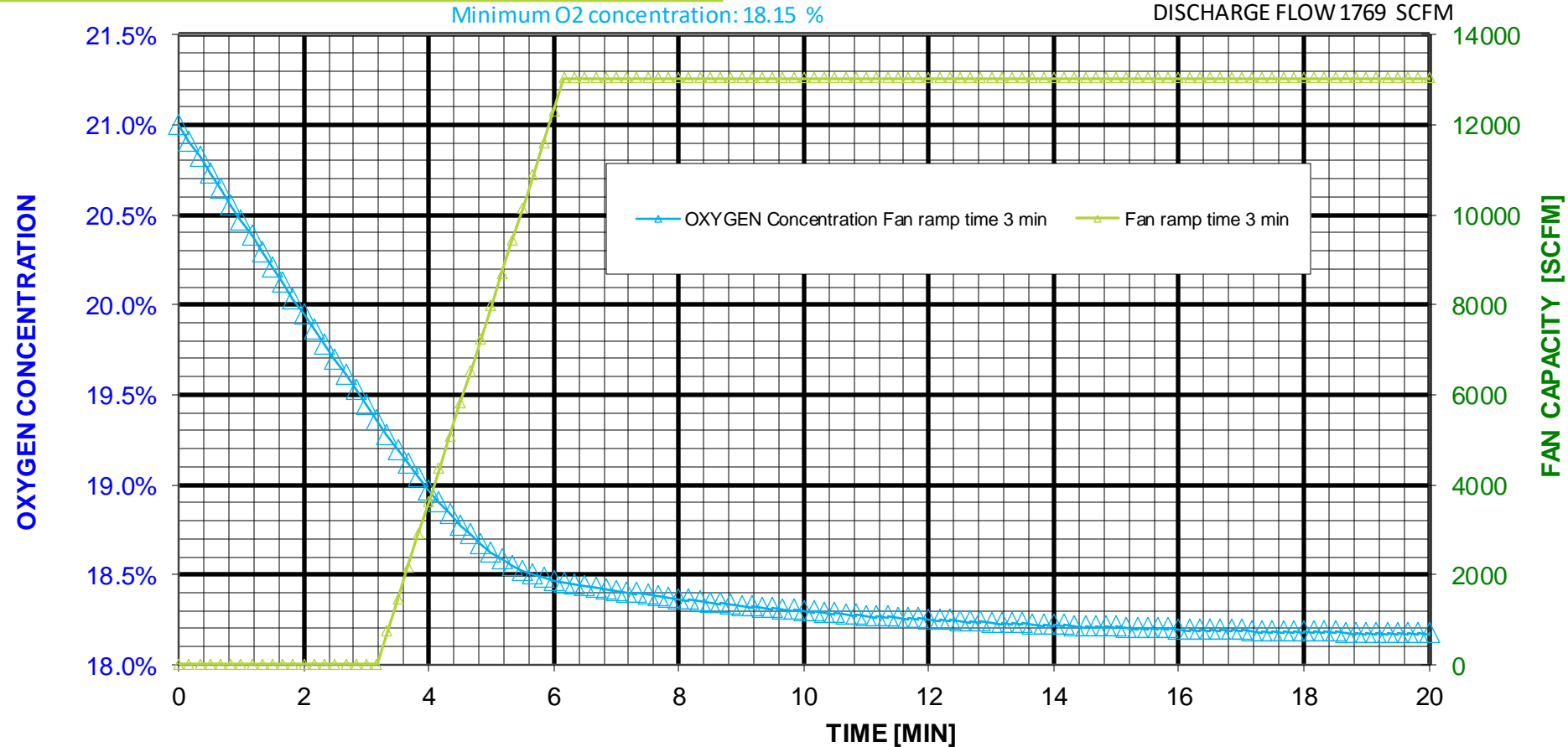
FAN CAPACITY: 13040 CFM

4.5K case, Service buildings

BUILDING VOLUME: 68895.973680555 CF

Fan triggers at: 19.5% Concentration 3 minute ramp duration

DISCHARGE FLOW 1769 SCFM



# 1008B transient for 1 ODH fan

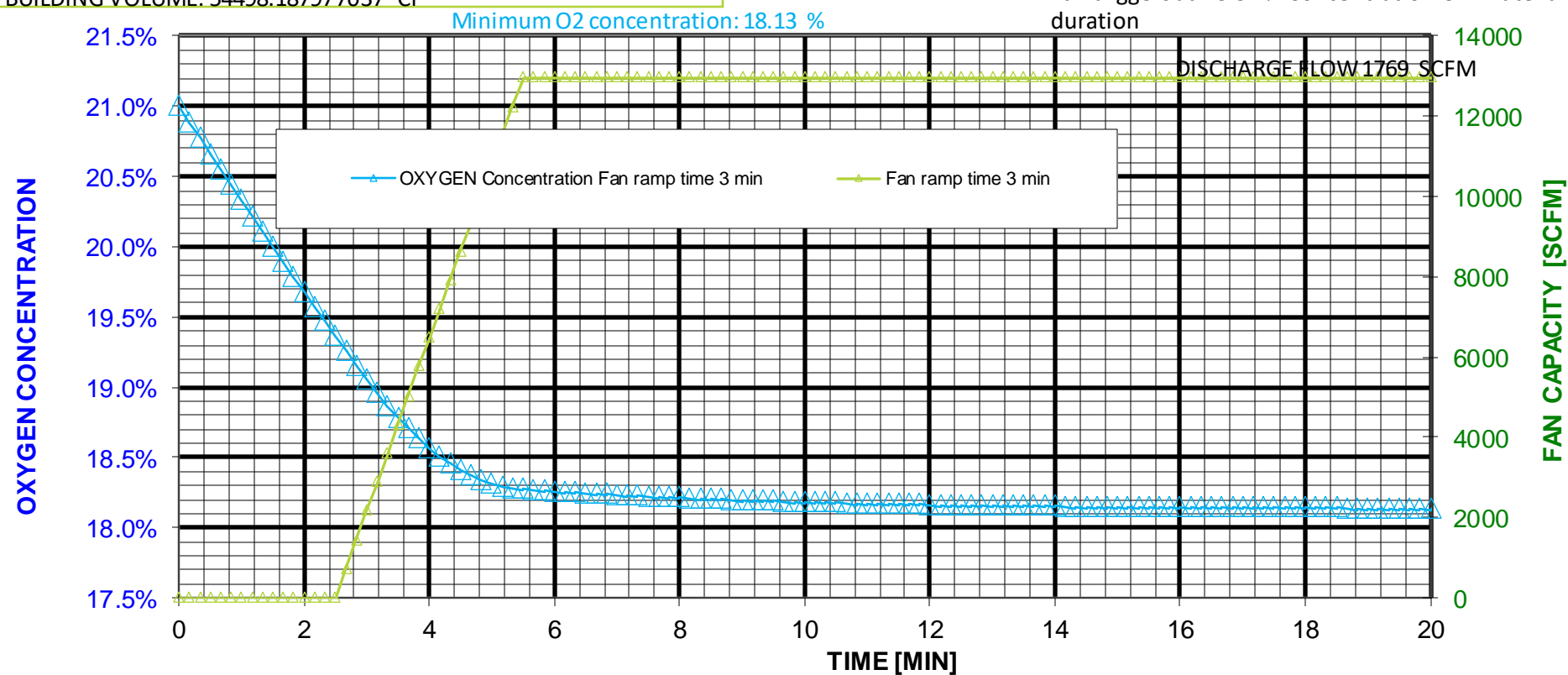
CASE: HELIUM MODE

FAN CAPACITY: 12960 CFM

4.5K case, Service buildings

BUILDING VOLUME: 54498.187977037 CF

Fan triggers at: 19.5% Concentration 3 minute ramp duration



# 1010A transient for 1 ODH fan

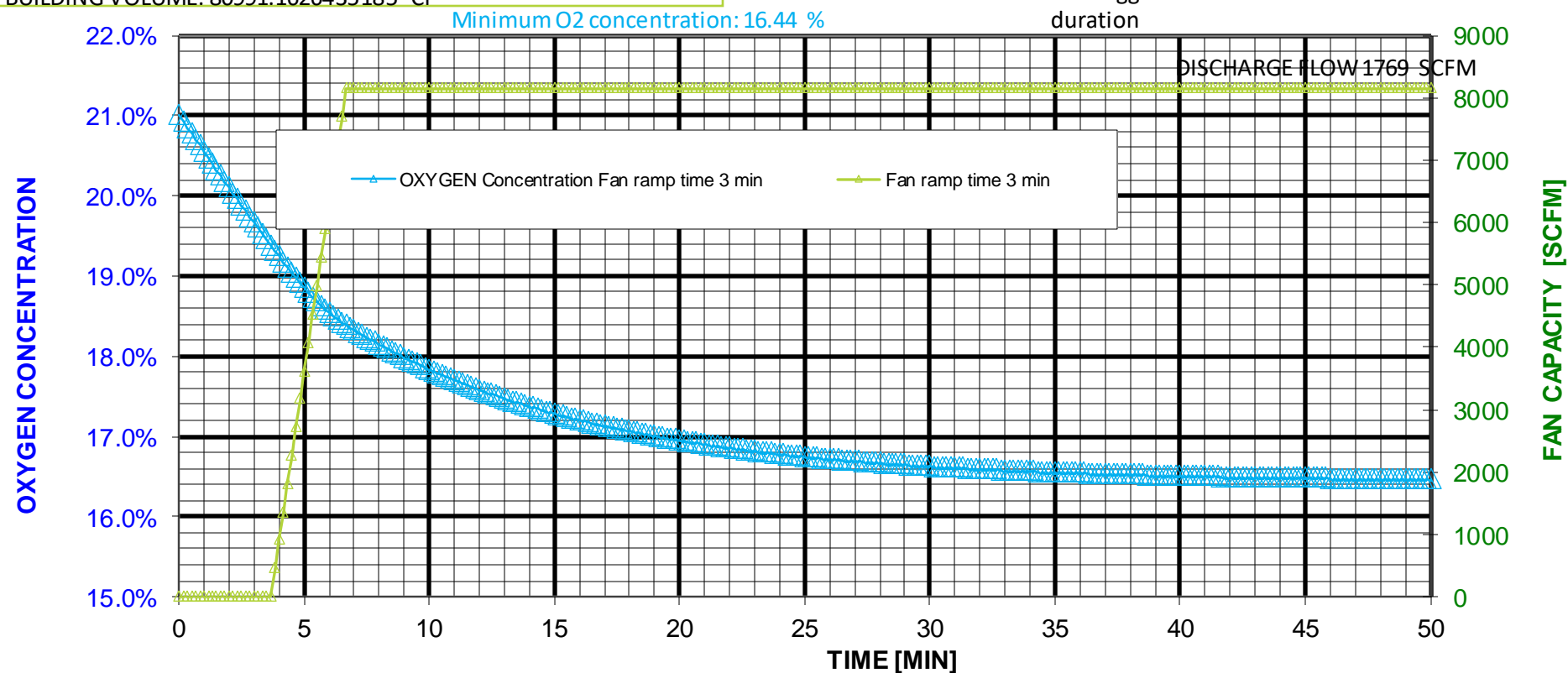
CASE: HELIUM MODE

FAN CAPACITY: 8144 CFM

4.5K case, Service buildings

BUILDING VOLUME: 80991.1626435185 CF

Fan triggers at: 19.5% Concentration 3 minute ramp duration



# 1012A transient for 1 ODH fan

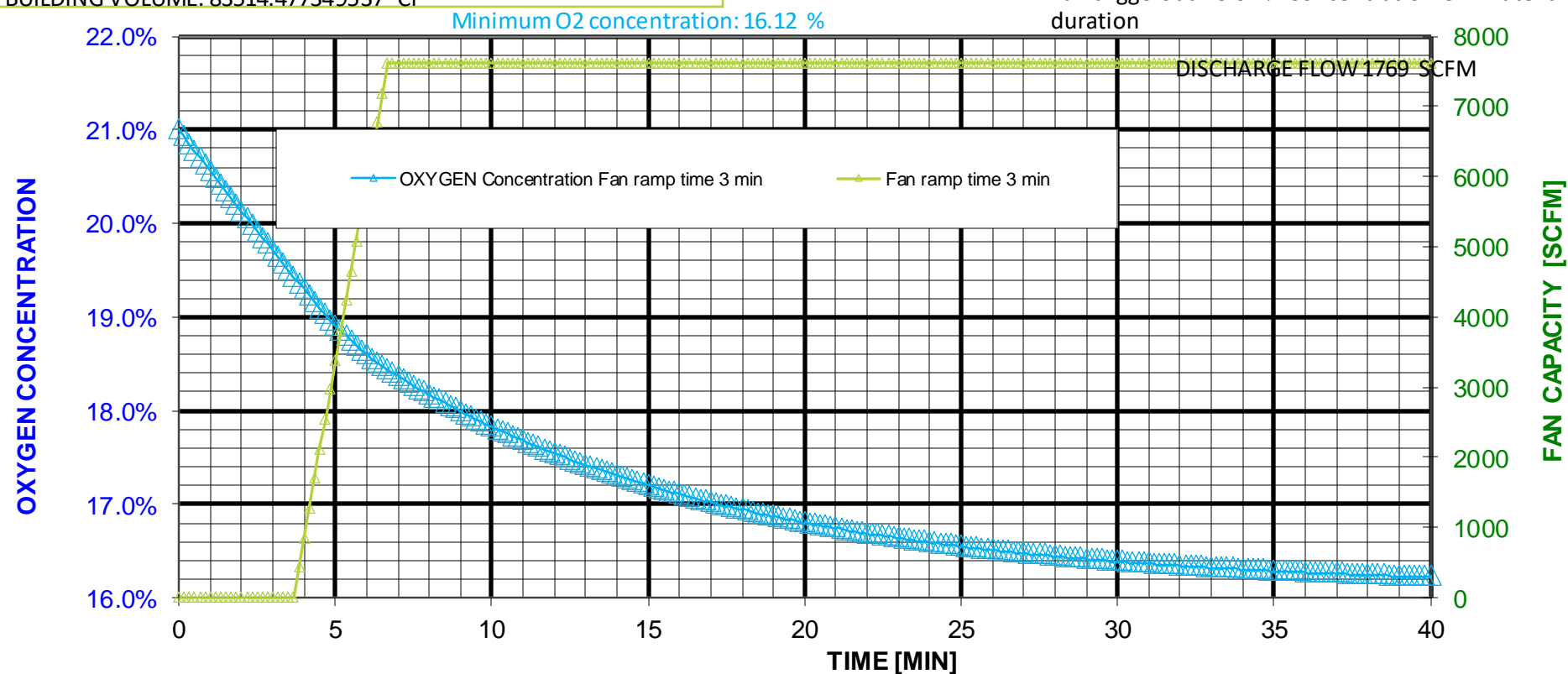
CASE: HELIUM MODE

FAN CAPACITY: 7608 CFM

4.5K case, Service buildings

BUILDING VOLUME: 83514.477349537 CF

Fan triggers at: 19.5% Concentration 3 minute ramp duration



# 1002B transient for 1 ODH fan

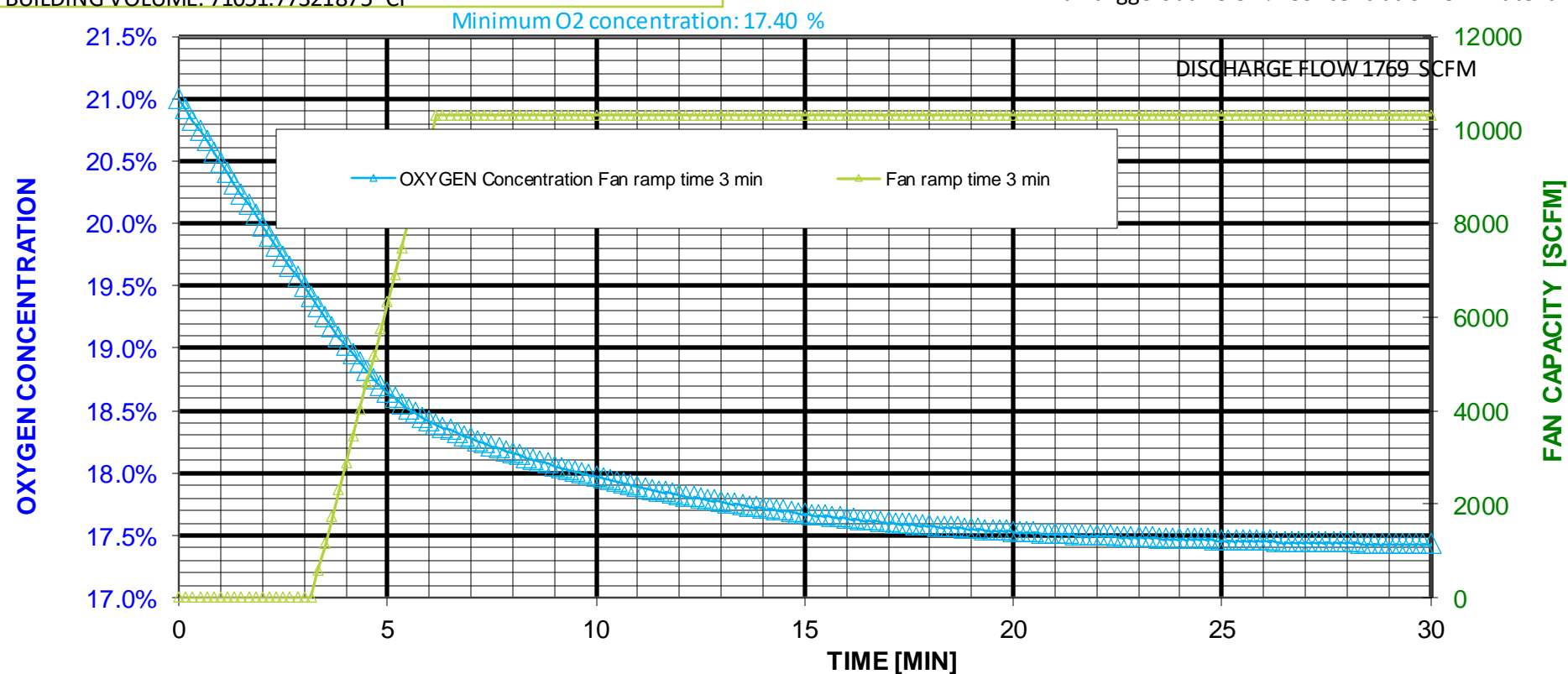
CASE: HELIUM MODE

FAN CAPACITY: 10312 CFM

4.5K case, Service buildings

BUILDING VOLUME: 71051.77321875 CF

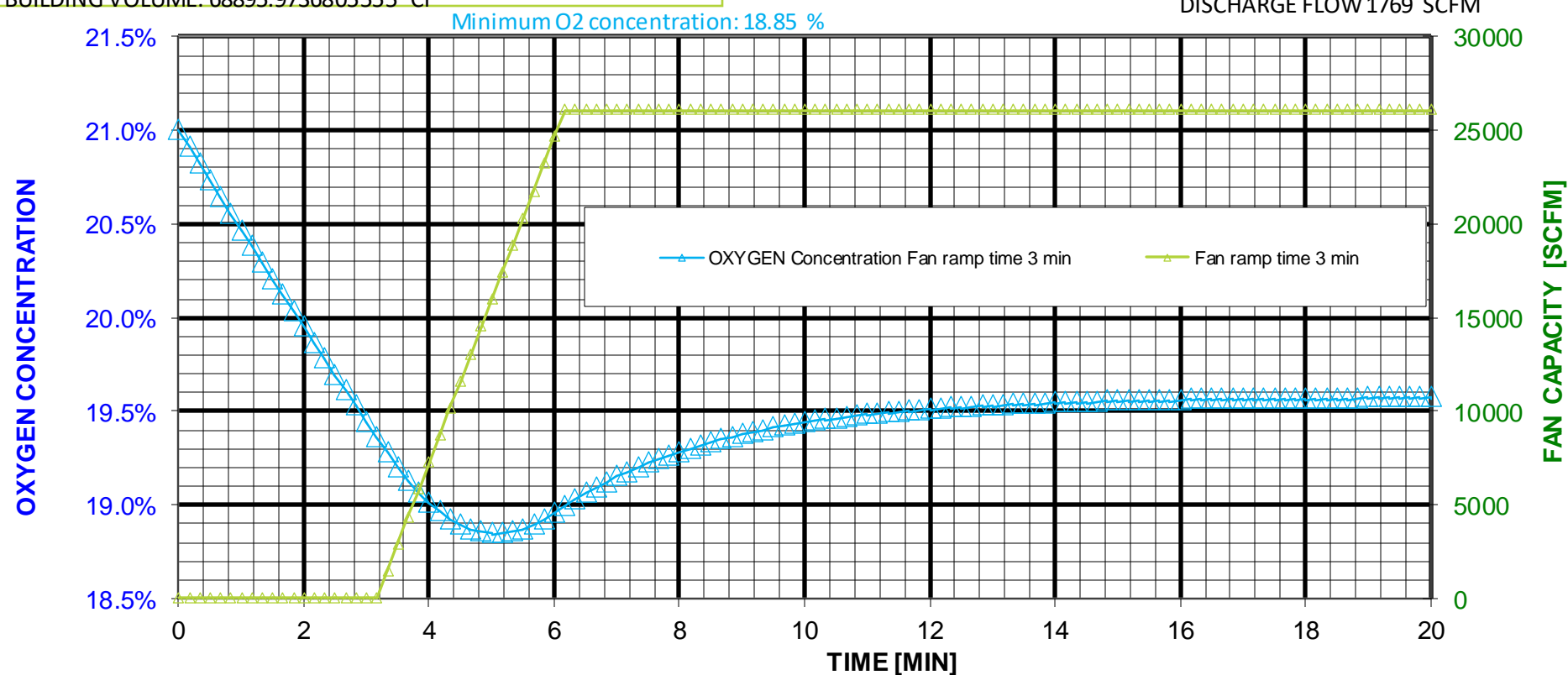
Fan triggers at: 19.5% Concentration 3 minute ramp duration





# 1006B transient for 2 ODH fan

CASE: HELIUM MODE FAN CAPACITY: 26080 CFM 4.5K case, Service buildings Fan triggers at: 19.5% Concentration 3 minute ramp duration  
BUILDING VOLUME: 68895.9736805555 CF DISCHARGE FLOW 1769 SCFM



# 1008B transient for 2 ODH fan

CASE: HELIUM MODE

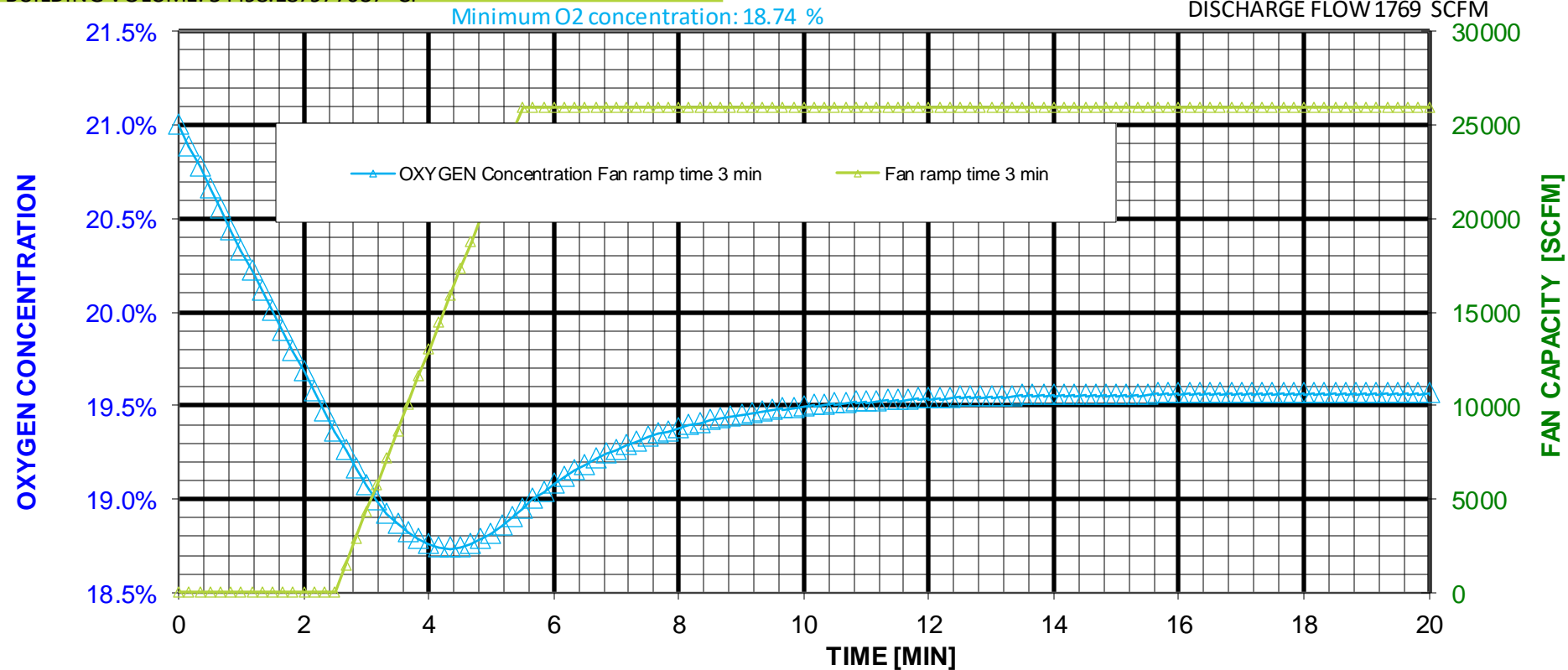
FAN CAPACITY: 25920 CFM

4.5K case, Service buildings

Fan triggers at: 19.5% Concentration 3 minute ramp duration

BUILDING VOLUME: 54498.187977037 CF

DISCHARGE FLOW 1769 SCFM



# 1010A transient for 2 ODH fan

CASE: HELIUM MODE

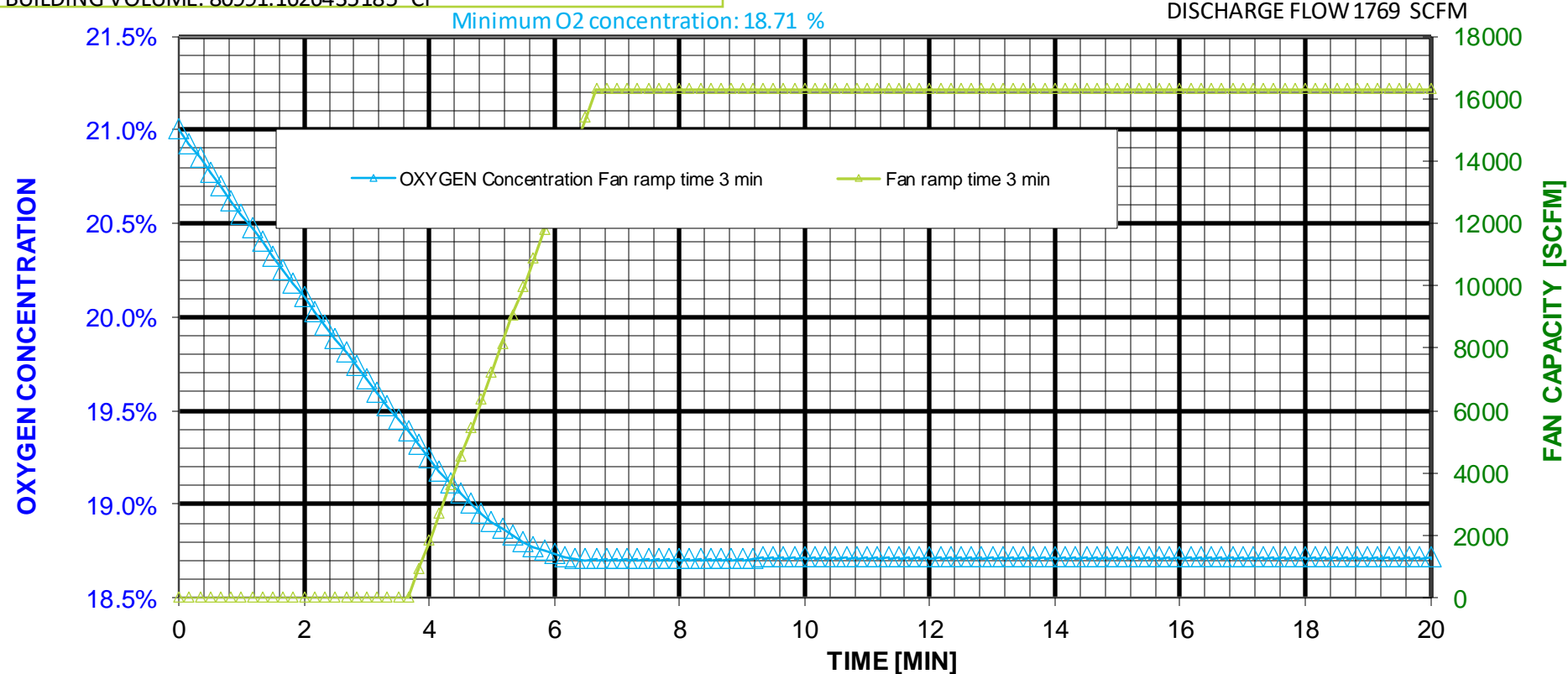
FAN CAPACITY: 16288 CFM

4.5K case, Service buildings

Fan triggers at: 19.5% Concentration 3 minute ramp duration

BUILDING VOLUME: 80991.1626435185 CF

DISCHARGE FLOW 1769 SCFM



# 1012A transient for 2 ODH fan

CASE: HELIUM MODE

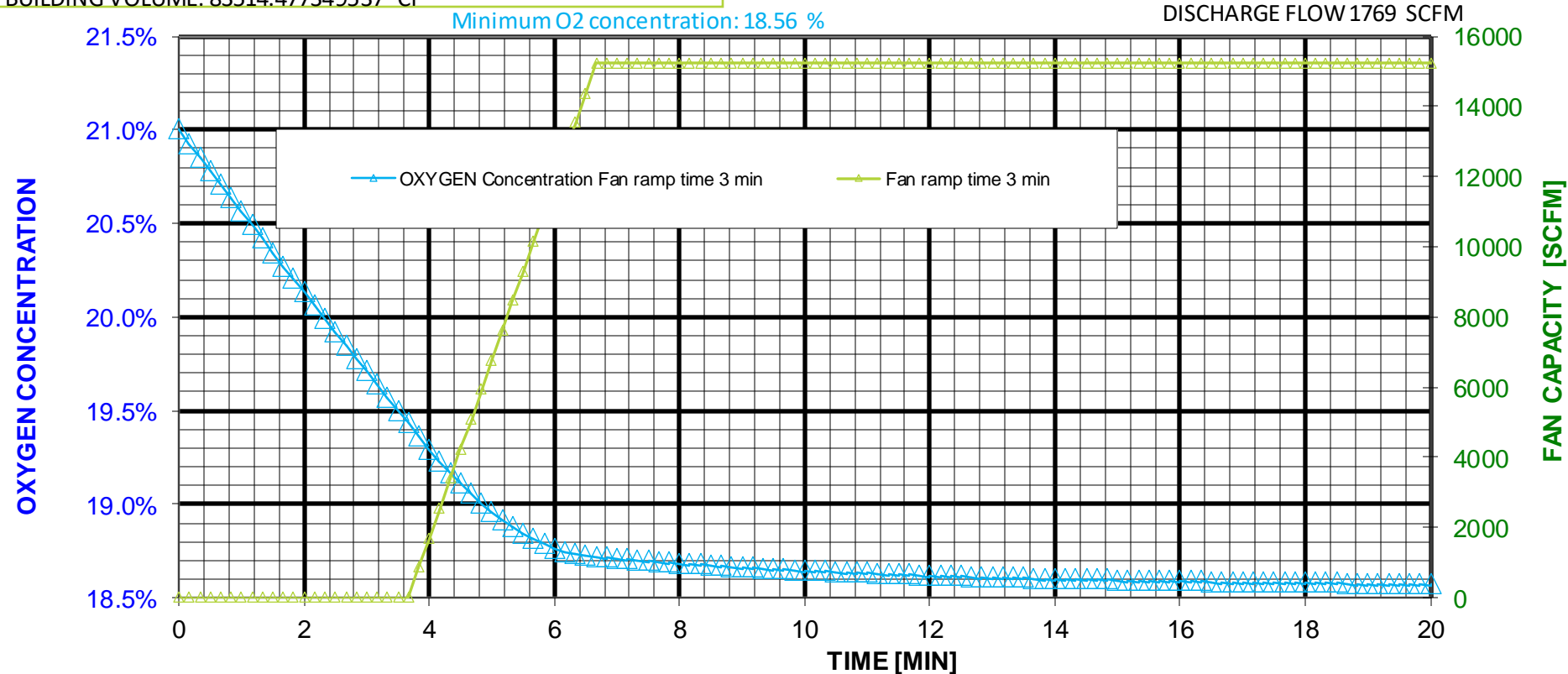
FAN CAPACITY: 15216 CFM

4.5K case, Service buildings

Fan triggers at: 19.5% Concentration 3 minute ramp duration

BUILDING VOLUME: 83514.477349537 CF

DISCHARGE FLOW 1769 SCFM



# 1002B transient for 2 ODH fan

CASE: HELIUM MODE

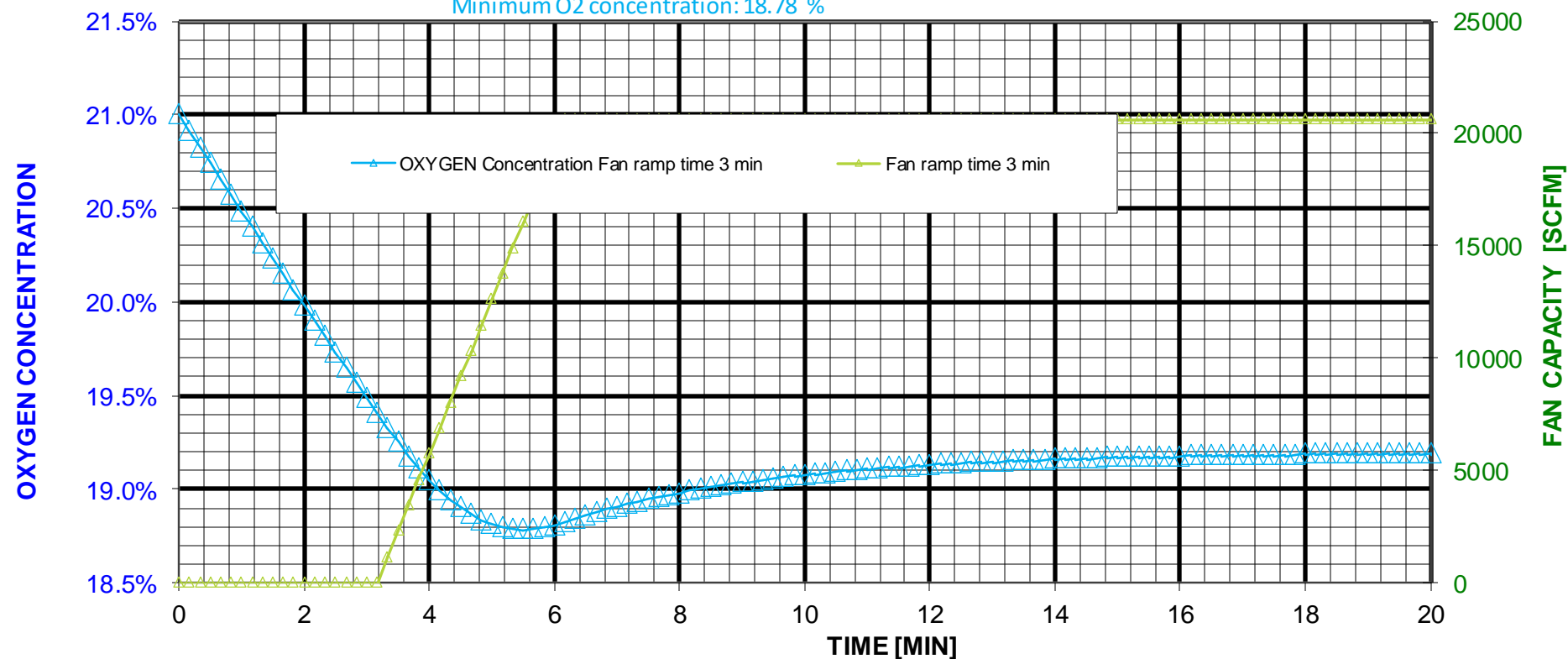
FAN CAPACITY: 20624 CFM

4.5K case, Service buildings

Fan triggers at: 19.5% Concentration 3 minute ramp duration  
DISCHARGE FLOW 1769 SCFM

BUILDING VOLUME: 71051.77321875 CF

Minimum O2 concentration: 18.78 %



The oxygen concentration in the building during a release of a gas is approximated by solving the following differential equations:

$$\frac{dC}{dt} = \frac{O_{2\_in} - O_{2\_out}}{V}$$

$$\frac{dC}{dt} = \frac{0.21 \cdot Q_{in} - C \cdot Q_{out}}{V} = \frac{0.21 \cdot Q_{in}}{V} - \frac{C \cdot Q_{out}}{V}$$

Where
V = building volume (CF)
C = oxygen concentration (mole fraction)
t = time (minutes)
Q <sub>out</sub> = the flow rate out of building
Q <sub>in</sub> = the flow rate into building of fresh air
Q = exhaust fan(s) flow rate (CFM)
R = inert gas spill rate into building (CFM)

When fans are drawing from the volume.
Q <sub>out</sub> = Q
Q <sub>in</sub> = Q-R
For the case where R>Q the effective Q <sub>in</sub> becomes zero and the Q <sub>out</sub> becomes R
When fans are blowing into the volume.
Q <sub>in</sub> = Q
Q <sub>out</sub> = Q+R

Substituting for Q<sub>in</sub> and Q<sub>out</sub> using Q and R one can come up with the following equations.

#### Minimum Oxygen concentration without ventilation

This assumes the air gets displaced by the release gas, with the resulting remaining air mixing with the released gas resulting in the calculated concentration.

$$C_{\min\_no\_ventilation} = 0.21 \frac{V - R}{V}$$

#### CASE 1 Ventilation fan(s) blowing into the confined volume.

$$V \frac{dC}{dt} = 0.21Q - (R + Q)C$$

$$C(\tau)_{case\_1} = \frac{0.21}{Q + R} \left[ Q + R \cdot e^{-\frac{(Q+R)\tau}{V}} \right]$$

#### CASE 2 Ventilation fan(s) drawing and the spill rate of inert gas (R) is less than the exhaust fan capacity (Q):

$$V \frac{dC}{dt} = 0.21(Q - R) - QC$$

$$C(\tau)_{case\_2} = 0.21 \left[ 1 - \frac{R}{Q} \cdot \left( 1 - e^{-\frac{Q\tau}{V}} \right) \right]$$

#### CASE 3 If the exhaust fan is off or if the inert gas spill rate (R) is greater than the exhaust fan capacity (Q)

$$V \frac{dC}{dt} = -RC$$

$$C(\tau)_{case\_2} = 0.21 \cdot e^{-\frac{R\tau}{V}}$$

# Isentropic nozzle equation:

DIM involves evaluating thermodynamic properties of the relieving stream at a number of state points and then numerically integrating the nozzle equation to determine the maximum mass flux

$$G^2 = -2\rho_i^2 \int_{p_0}^p v dp$$
$$\int_{p_i}^{p_{i+1}} v dp = \frac{(v_{i+1} + v_i)}{2} * (p_{i+1} - p_i)$$

Cd=0.65

```
Const atmpa As Double = 101325#
Const pie As Double = 3.14159265
Const Bar_Pascal As Double = 100000#
Dim He_entropy As Double
Dim He_spv As Double

Dim p_il As Double
Dim pi As Double
Dim g As Double

Function helium_leakflux(Temp_K As Double, Pres_pa_in As Double, Pres_pa_out As Double, nloop As Integer)

He_entropy = hecalc(8, 0, 1, Pres_pa_in, 2, Temp_K, 1)
He_spv = hecalc(4, 0, 8, He_entropy, 1, Pres_pa_in, 1)

Dp = (Pres_pa_in - Pres_pa_out) / nloop
pi = Pres_pa_in
intl = 0

g = 0
For i = 1 To nloop
p_il = pi - Dp
He_spvl = hecalc(4, 0, 8, He_entropy, 1, p_il, 1)
He_spvavg = (He_spv + He_spvl) / 2

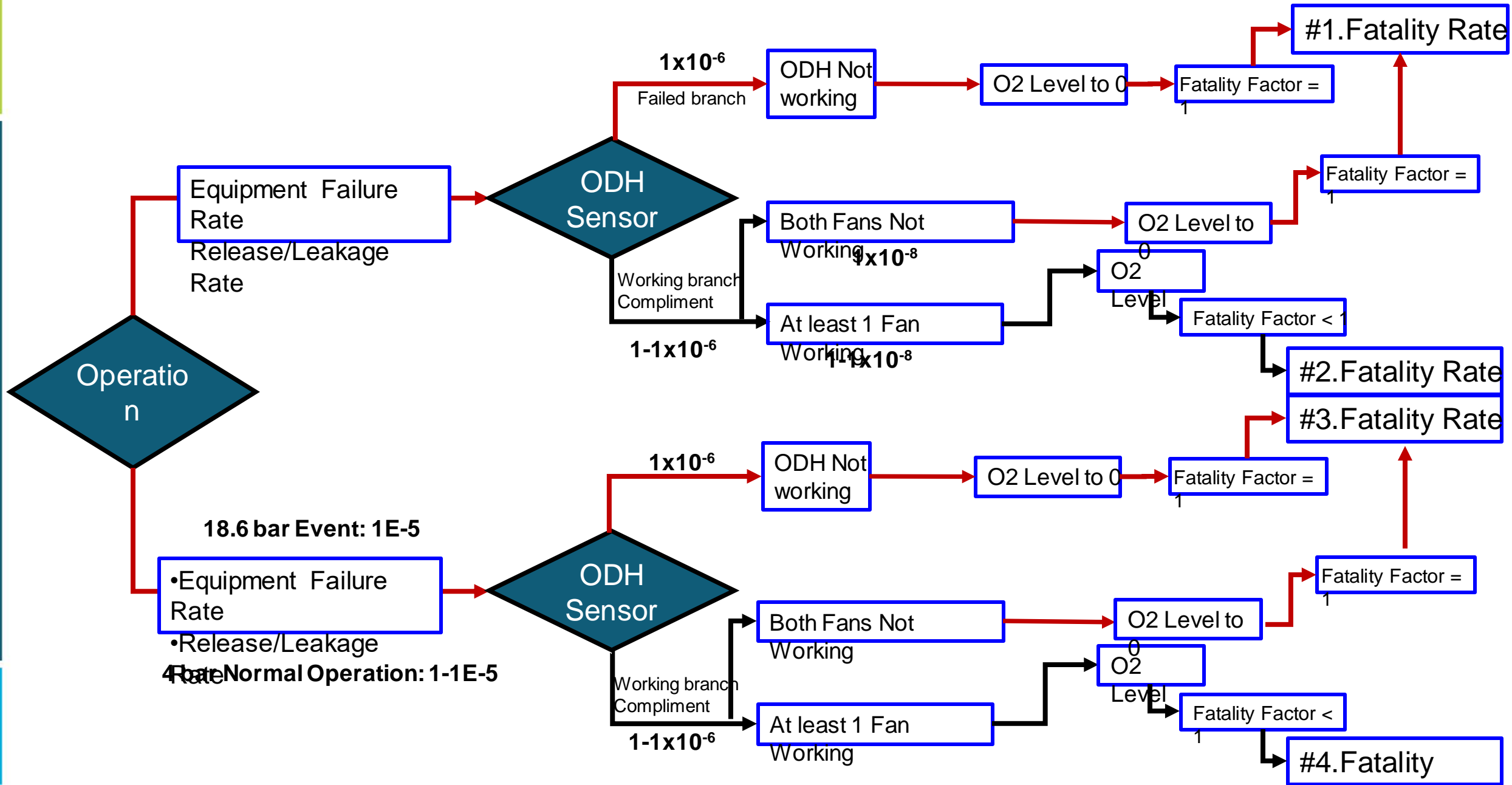
intl1 = He_spvavg * Dp + intl
intl = intl1
g1 = (2 * (1 / He_spv) ^ 2 * intl1) ^ 0.5

If (g1 < g) Then Exit For

g = g1
pi = p_il
He_spv = He_spvl
If (p_il <= Pres_pa_out) Then Exit For

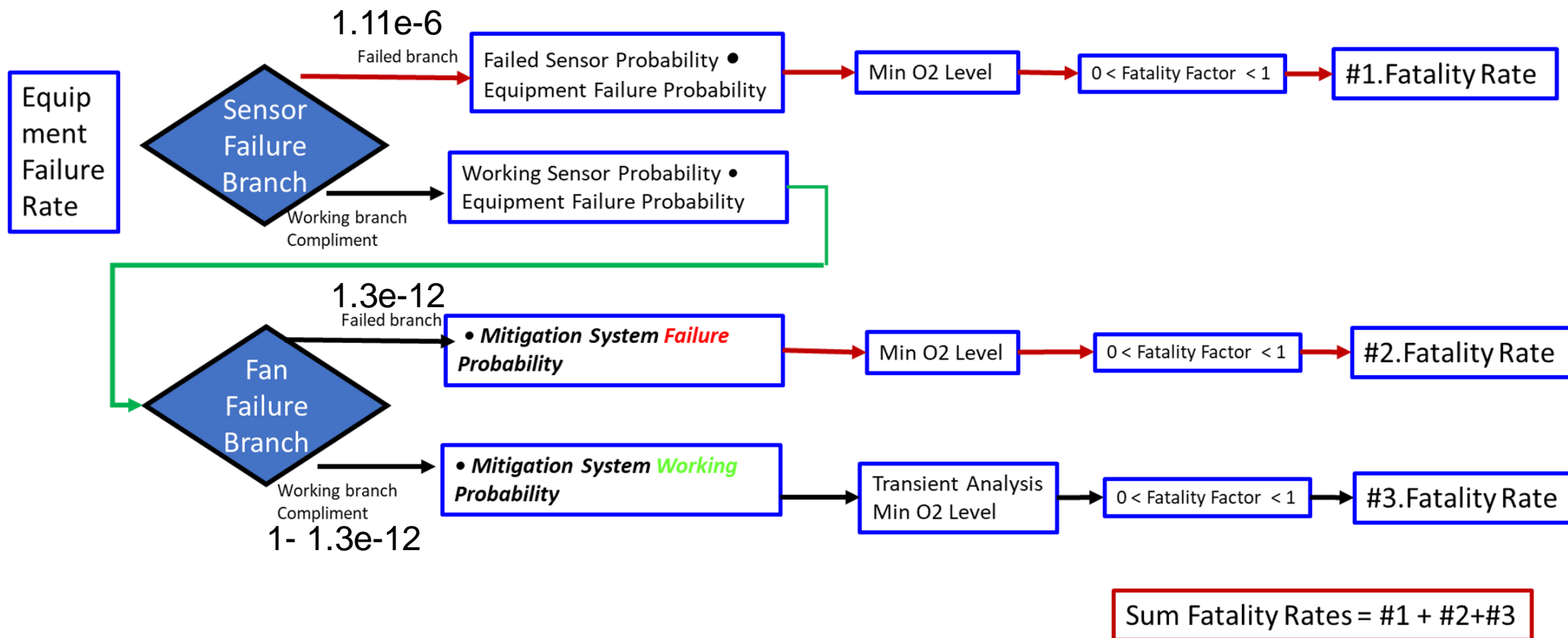
Next i
helium_leakflux = g

End Function
```





# GENERAL FAILURE TREE DIAGRAM



# Auxiliary Buildings

Auxiliary Buildings with 1 ODH fan								
Location	Volume	Equipment	Net Free Volume	Fan SCFM	Release Flow SCFM	O2 Concentration	Fatality rate 1/hr	ODH class
1004E	3000	20	2980	3000	128	9.0%	1.0E-8	0
1002A	22500	--	22500	3000	230	16.9%	9.0E-12	0
1010Mez	10500	1200	9300	--	128	0%	2.0E-8	0

Auxiliary Buildings							
Location	Volume	Equipment	Net Free Volume	Failure rate 1/hr	O2 Concentration	Fatality rate 1/hr	ODH class
1004E	3000	20	2980	1.3E-8	0%		0
1002A	22500	--	22500	3E-8	0%		0
1010Mez	10500	1200	9300	2E-8	0%		0