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U.S. DEPARTMENT OF  
**ENERGY**

Office of Science

# ePIC SVT Air Cooling

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# Workforce

This is a team effort 😊

## Graduate Students

- Mathias Labonte (UCD)
- Andrew Liggett (UCD)
- Ziyuan Zeng (UCD)

## Undergraduate Students

- Elijah Dolz (Berkeley City College)
- Jonathon Tordilla (UCB)
- Malika Golshan (UCB, *graduated*)

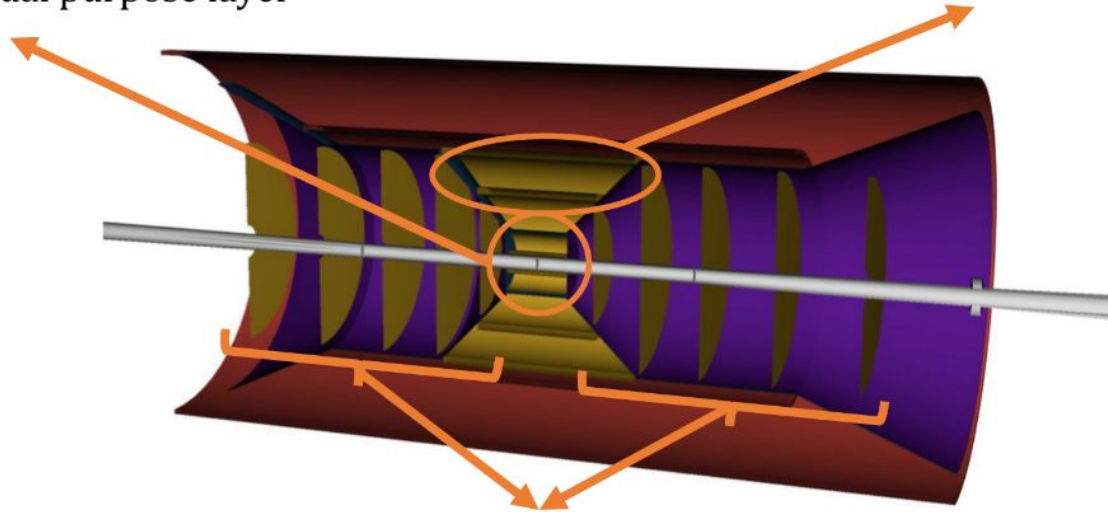
# The ePIC Silicon Vertex Tracker

## Inner Barrel (IB)

- 2 curved vertex layers
- 1 curved dual purpose layer

## Outer Barrel (OB)

- 1 stave-based sagitta layer
- 1 stave-based outer layer

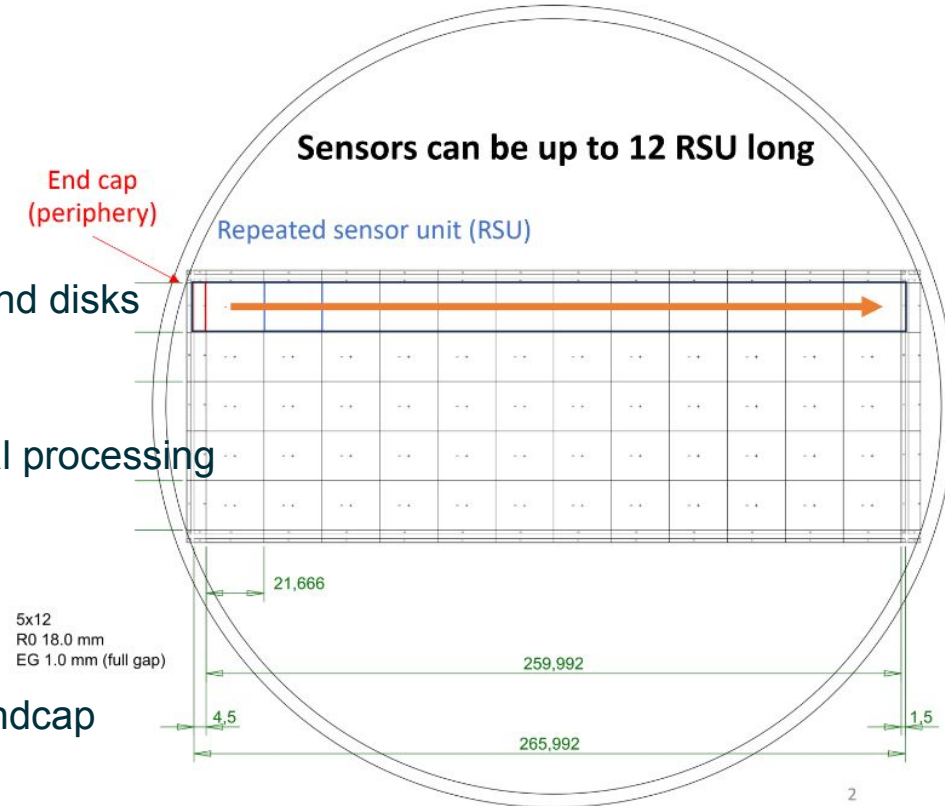


## Electron/Hadron Endcaps (EE/HE)

- 5 discs on either side of IP

# A few notes on terminology

- ITS3
  - Silicon sensor design used in ALICE
- LAS
  - Large Area Sensor for ePIC staves and disks
- Endcap
  - High power region of sensor
  - Used for power distribution and signal processing
- RSU
  - Repeated Sensor Unit
  - Sensitive area of detector
- Matrix
  - Multiple RSUs attached to a single endcap



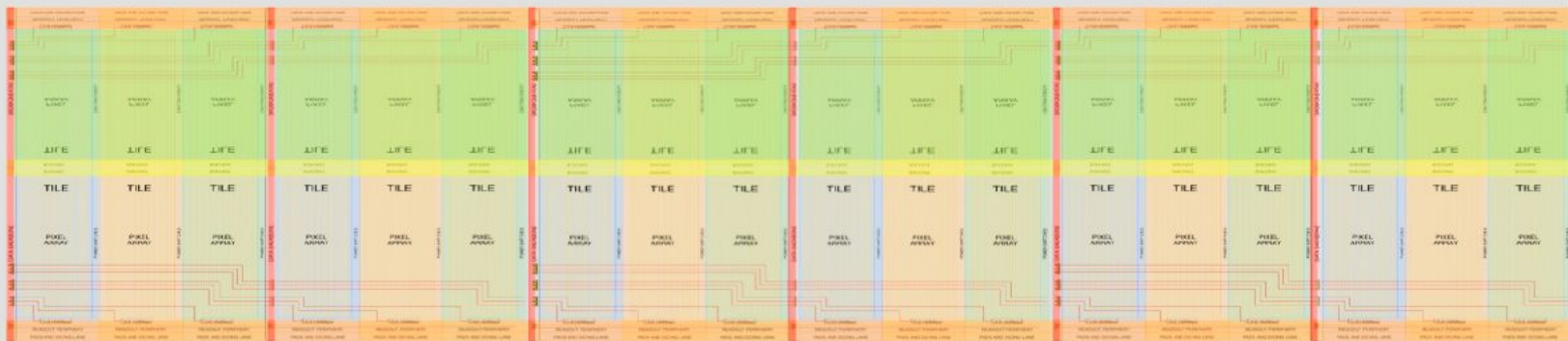
# Power Density

\*Slide from N. Apadula

	Power density [mW cm <sup>-2</sup> ]		
	Expected 25 °C	Max 25 °C	Max 45 °C
Left End Cap (LEC)		791	
Active area (RSU)	28	44	2
Pixel matrix	15	32	51
Biasing	168	168	168
Readout peripherics	432	457	496
Data backbone	719	719	719

LEC (aka periphery) ~0.8 W/cm<sup>2</sup>  
Matrix (total) ~20-40 mW/cm<sup>2</sup>

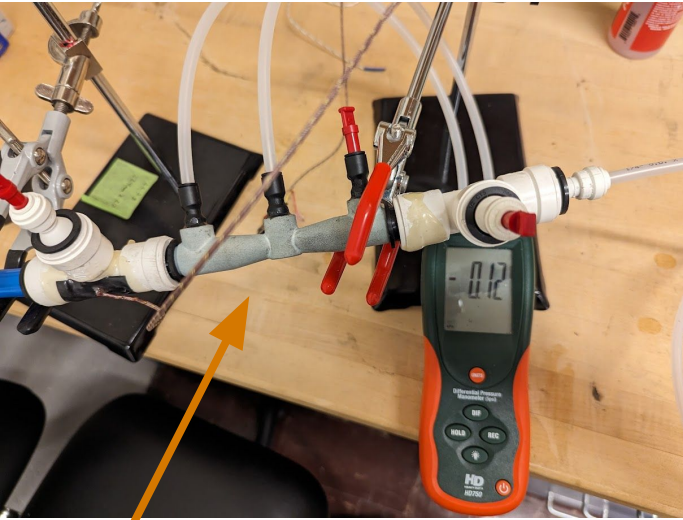
**Table 3.10:** Estimates of average power dissipation per unit area over the main blocks composing the sensor.



# Key points for cooling the SVT

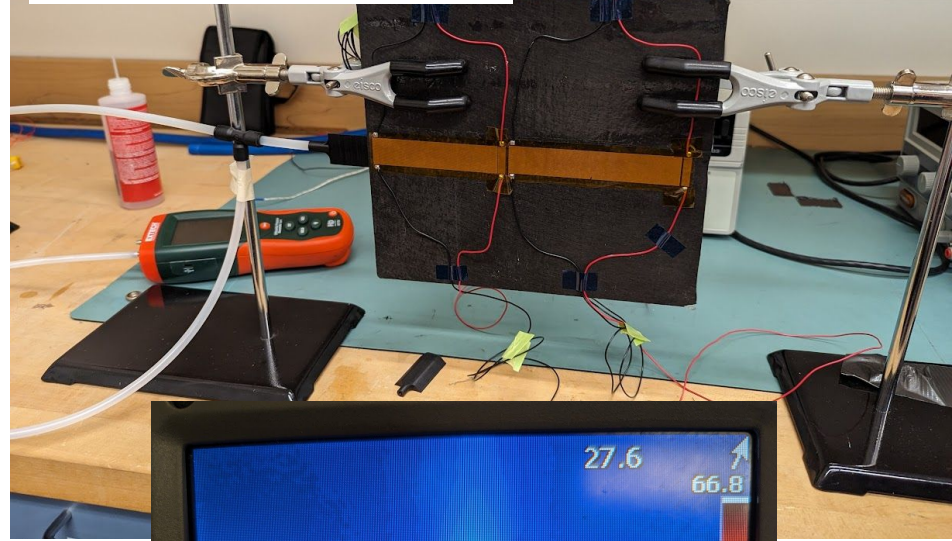
- While the sensor design is based on ALICE ITS3, the cooling system used in ALICE is too much material for ePIC
- Total Material Budget -  $X/X_0 < \sim 5\%$ 
  - Water cooling and associated services are readily available due to cooling other detectors, but water is high material budget
- Current estimate is  $\sim 1.6-2$  W of power to each sensor
- Need to dissipate  $\sim 6.4-8$  kW in total
- Aim is to limit temperature increase of sensors to  $< 15-20$  °C
  - $\Delta T = \text{Power on temperature} - \text{Power off temperature}$

# Test Setup

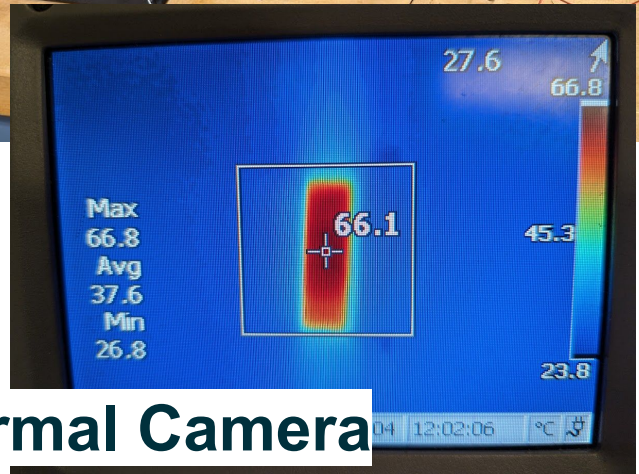


Air

# Cooling Material with Powered Heater



# Venturi for Air Flow Rate

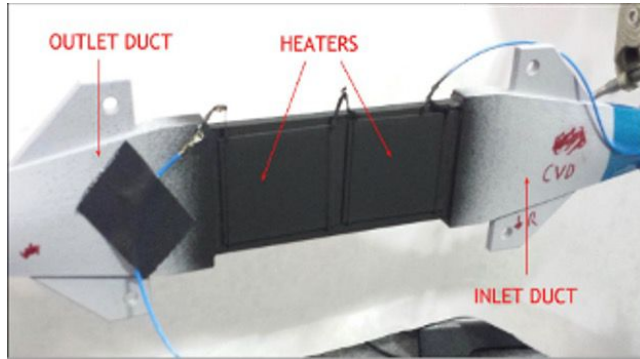


# Thermal Camera

# Test materials for simulating heat generated

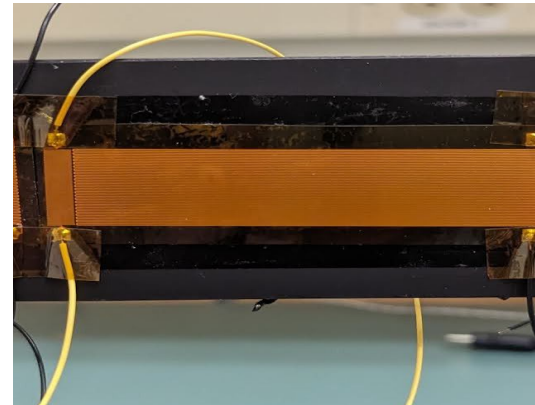
## Ceramic Heaters

- High heat output - good for stress testing
- Substantially higher heat output than real sensor
- No localized heating to simulate power regions



## Copper Trace Heaters

- More realistic power densities
- Simulates both Endcap and pixel matrix regions
- Fragile

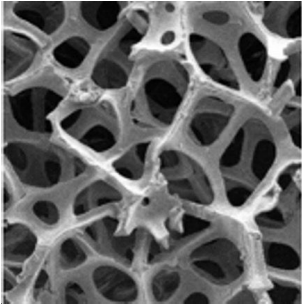




# Cooling Materials

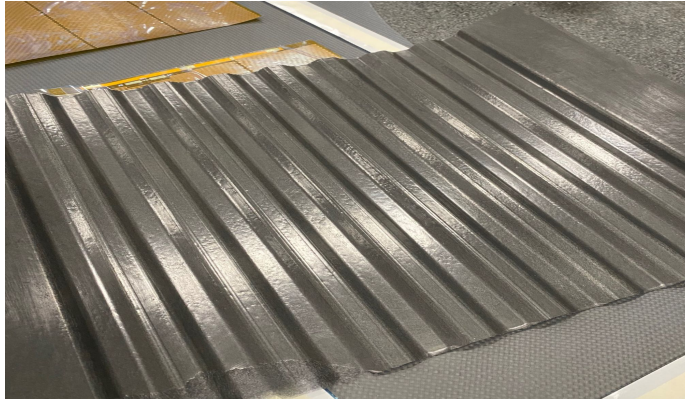
## Reticulated Vitreous Carbon

- Insulating carbon foam
- Lower material budget than CVD
- Lower cooling power, but possibly feasible depending on real power density



## Chemical Vapor Deposition

- Conducting carbon foam
- Higher material budget than RVC
- Clearly works for all realistic power densities



## Corrugated Carbon Fiber

- Carbon fiber that is bent to create corrugation channels (like cardboard) for directing air
- Even lower material budget
- Doesn't seem to work well on its own
  - Air flow is approximately laminar, reducing cooling power
  - Need to induce turbulence or increase contact area
  - Testing with foam added for heat conduction and turbulence

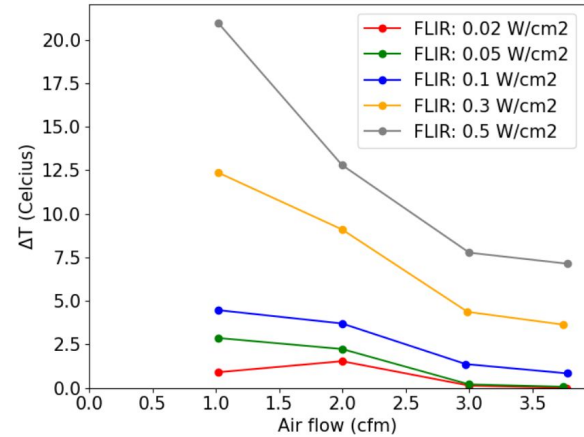


# What have we learned so far?

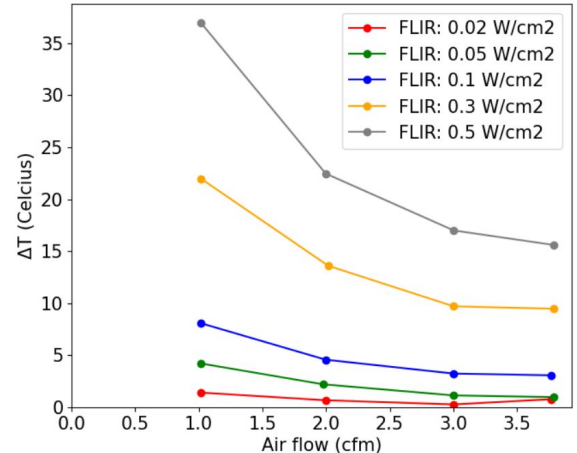
## CVD is better than RVC

- Expected, but good to quantify
- Data to right is from summer 2023 with ceramic heaters
- It is important to note that even with realistic power densities, the *total* power is substantially higher than realistic

$\Delta T$  FLIR as a function of air flow  
Heater: CVD 4mm



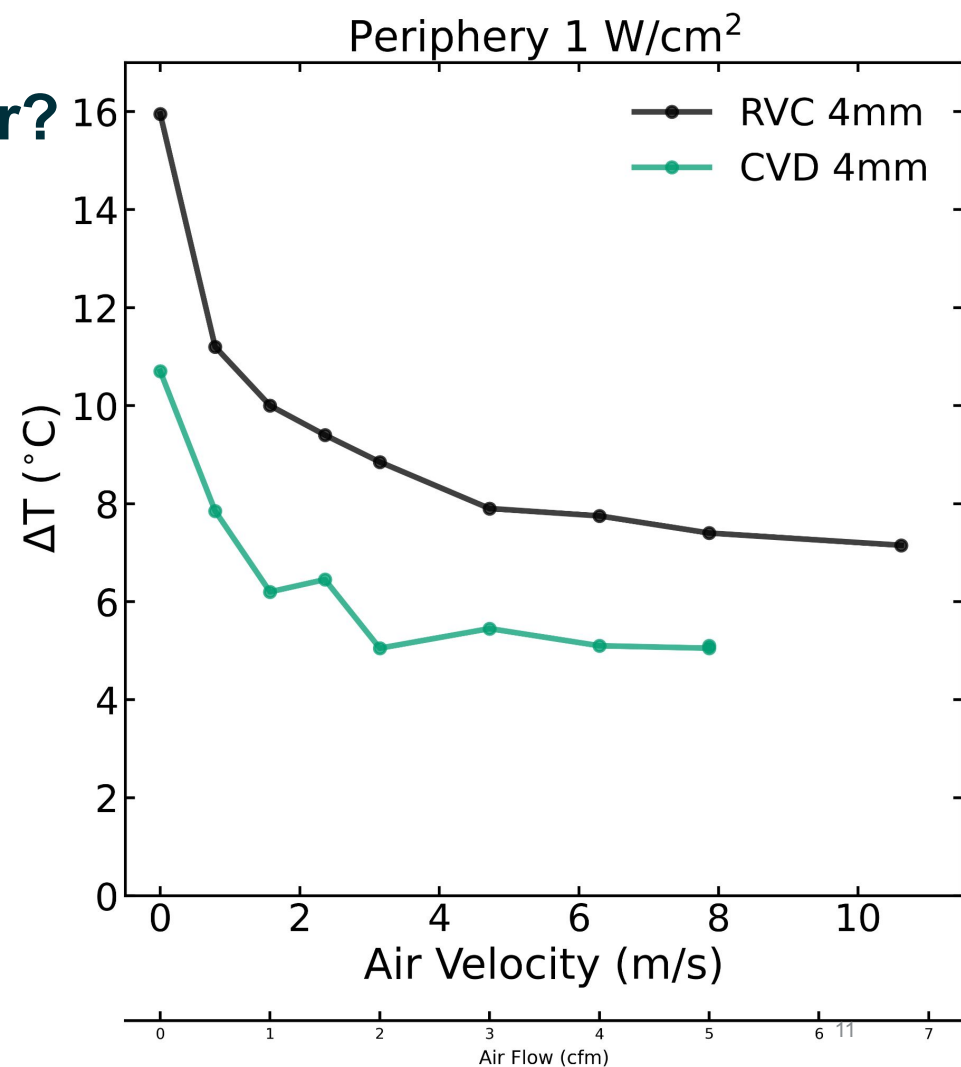
$\Delta T$  FLIR as a function of air flow  
Heater: RVC 4mm



# What have we learned so far?

## CVD is better than RVC

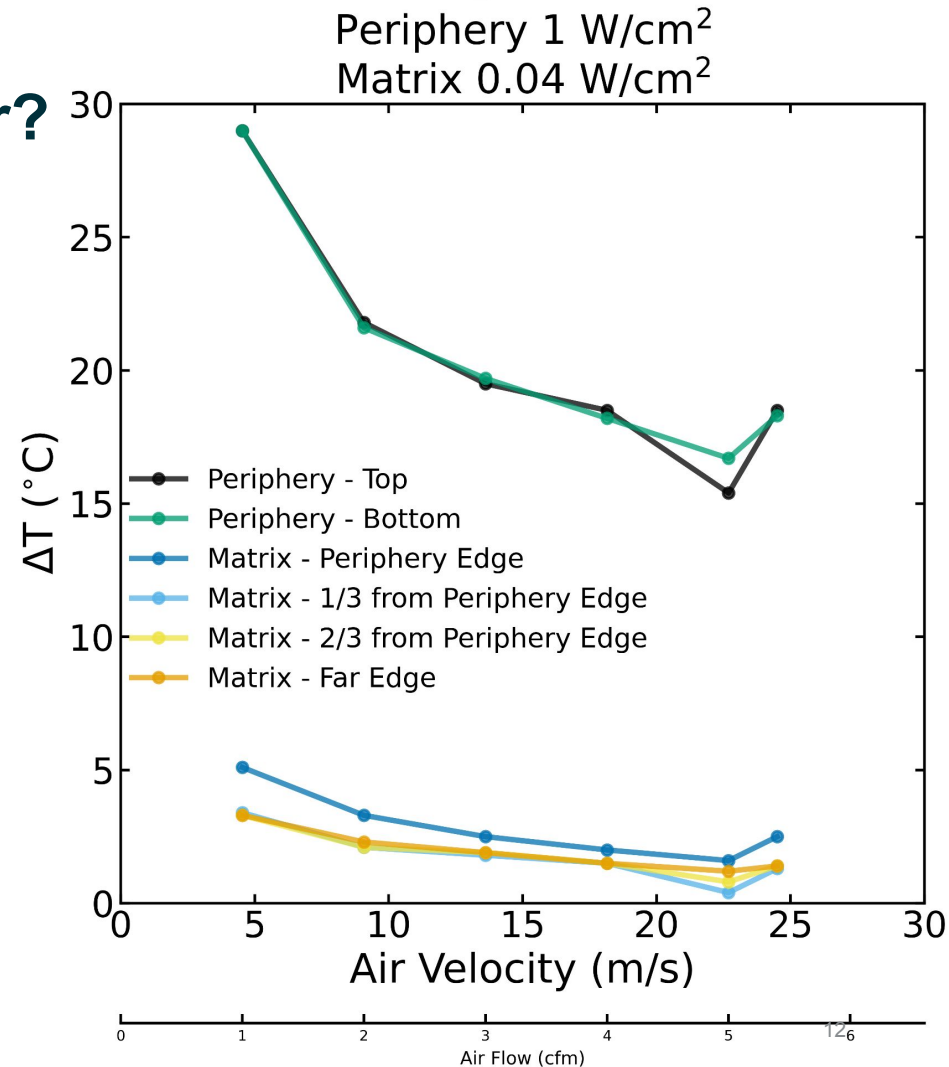
- Data on right uses realistic copper trace heater
- Due to spacing limitations (heater is larger than stave), only the periphery (high power density region) was used
- Shows that CVD is viable, even with *no air flowing*
- RVC becomes viable with only modest air flow
- Suggests that modest air flow quickly reaches a point of diminishing return



# What have we learned so far?

## Corrugated Carbon Fiber alone is insufficient

- When using the corrugated carbon fiber
  - The matrix is ok, due to low power
  - No air speed cools the periphery sufficiently
- Two leading theories as to why
  - The air flow is approximately laminar, so the heat isn't "mixed"
  - With only the fiber surface, there is comparably little contact with the air

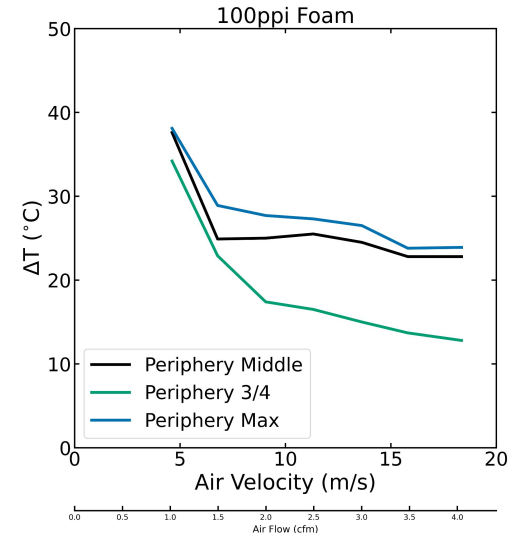
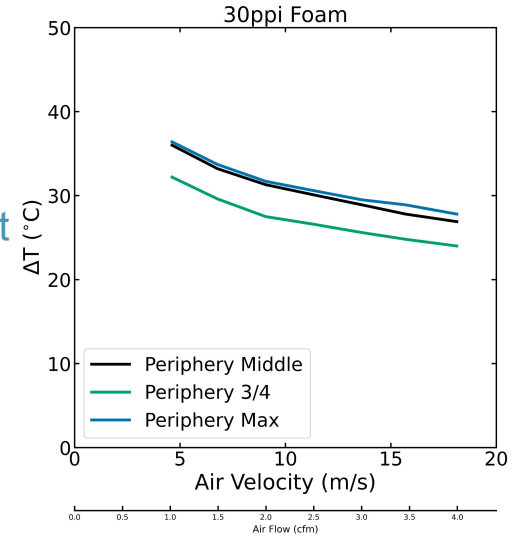


# What have we learned so far?

## Corrugated Carbon Fiber with a small foam piece is insufficient

- A small piece of RVC foam was placed\* beneath the periphery of the heater on the corrugated carbon fiber
  - To create turbulence
  - To allow for heat to be more readily pulled away
- A *slight* improvement is seen with 100ppi foam, but no improvement is seen with 30ppi foam
  - Neither case allows for sufficient cooling

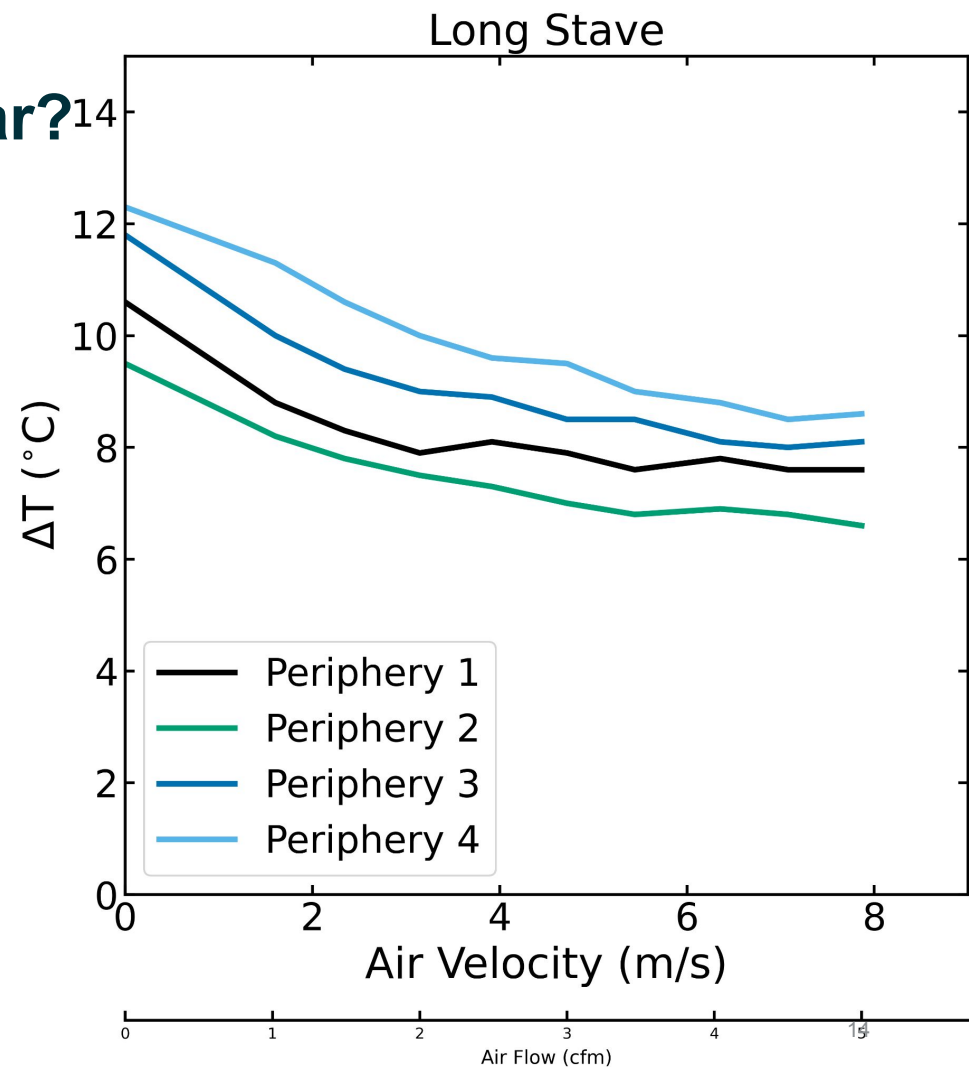
\*squeezed into the channel



# What have we learned so far?

## CVD likely works for several heaters

- A long 4mm CVD stave has 4 copper trace heaters attached
  - In this plot, only the periphery regions are heated
  - The matrix region will add about ~50% more power
  - The matrix region has been easier to cool due to the power being spread out (still need to check, of course)

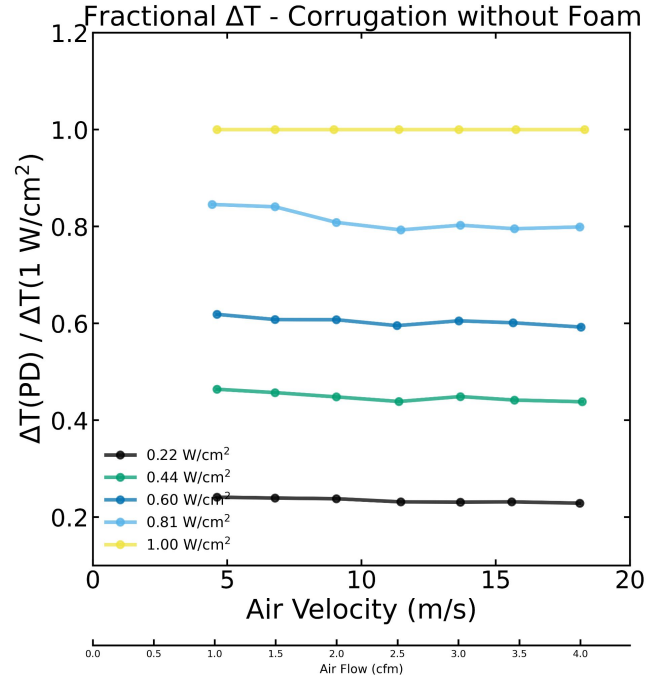
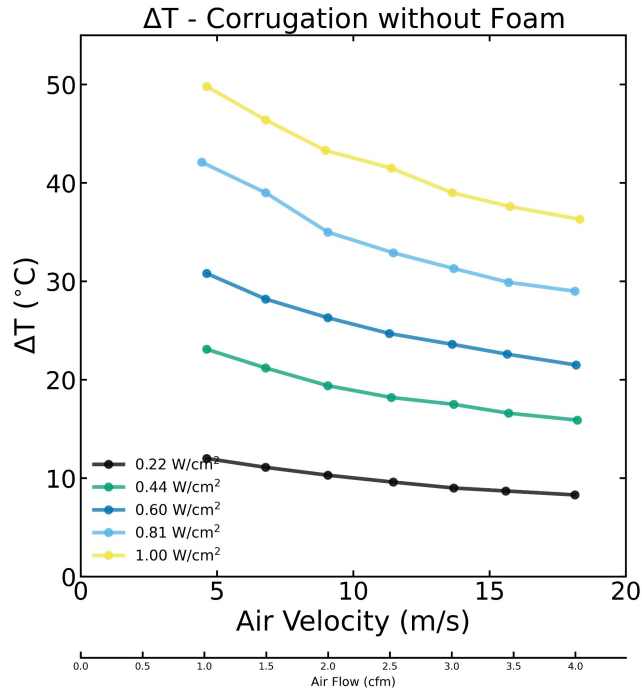


# A discussion of the power densities

- All plots shown so far have used a nominal 1 W/cm<sup>2</sup> for the endcap and 40 mW/cm<sup>2</sup> for the matrix
- We have recently been informed that 0.7-0.8 W/cm<sup>2</sup> is a more realistic number for the endcap
- It is good that we have tests at higher than nominal, but we also should have tests actually *at* nominal
- As designed for ITS3, each sensor endcap has 6 high bandwidth data lines, the dominant use of power
- ePIC does not need this much throughput
- The inner barrel will use this as designed
- There has been a suggestion that the endcap could possibly be redesigned for the staves and disks, *if we can show that it is worth it*
  - Estimates are that the endcap power density can be roughly halved

# Power Density Tests

## Corrugated Fiber without Foam

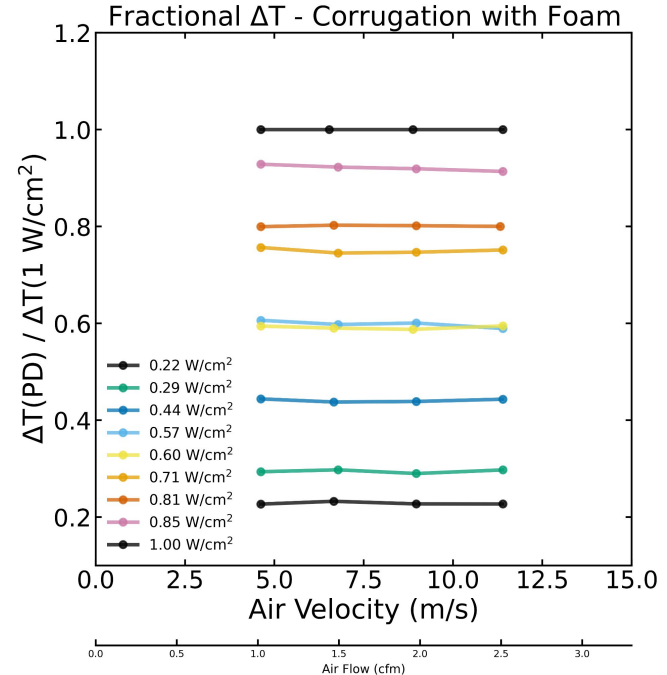
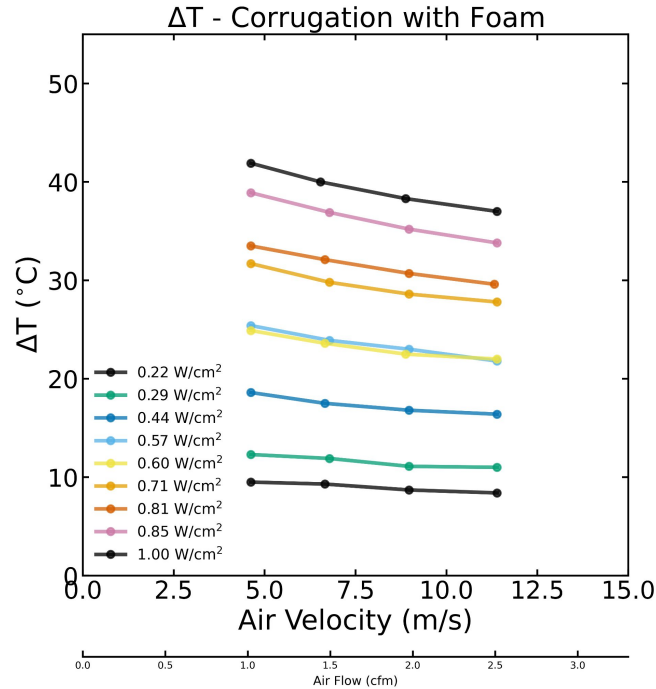


Delta T scales well with power density!



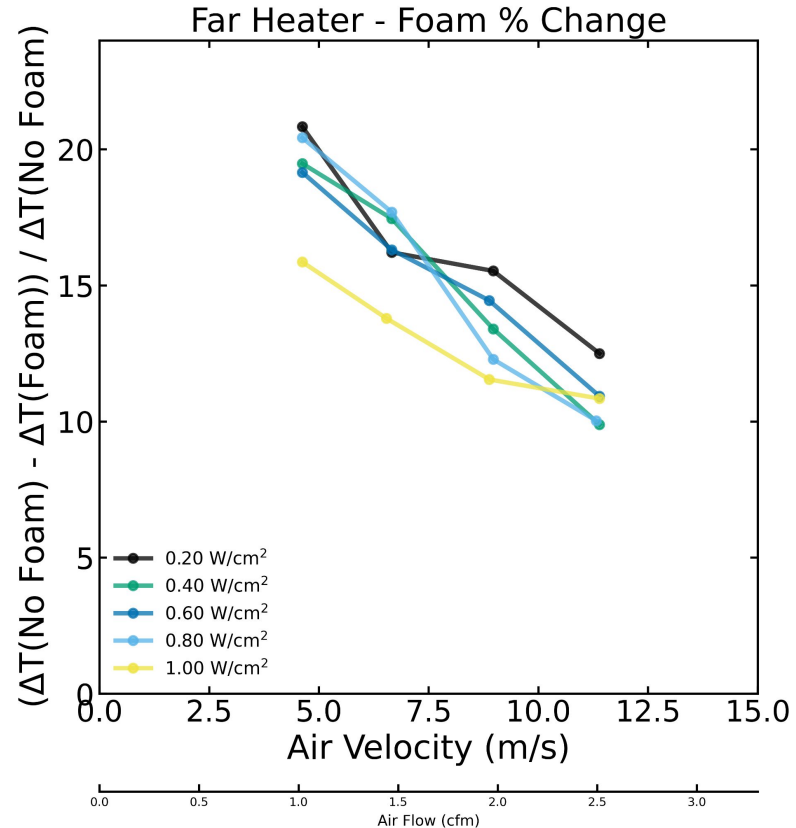
# Power Density Tests

Corrugated Fiber with Foam (30ppi RVC Foam glued with thermal epoxy)



Delta T scales well with power density!

# How much does the foam help?



- Biggest improvements are with low air speed, generally where we won't run it
- We expect to run around ~10 m/s
- Improvement drops with increased air speed
  - ~12% improvement at 10 m/s

# What comes next?

- Test cooling capabilities for with multiple sensors
- Test with silicon
- Test with smaller corrugations (currently being manufactured)
- Developing a pt100 (platinum resistance temperature detector) based measurement system for more accurate and reliable measurements
  - Raspberry Pi based readout
  - Had previously been worked on by Malika Golshan (UCB), but we ran into difficulties developing a repeatable sensor mounting workflow
    - Other measurement timelines necessitated putting this work on the backburner, but it is now moving up the priority list

# Thank You