

SBND TPC Electronics Pulser Calibrations

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WireCell Meeting
September 5, 2024



Overview

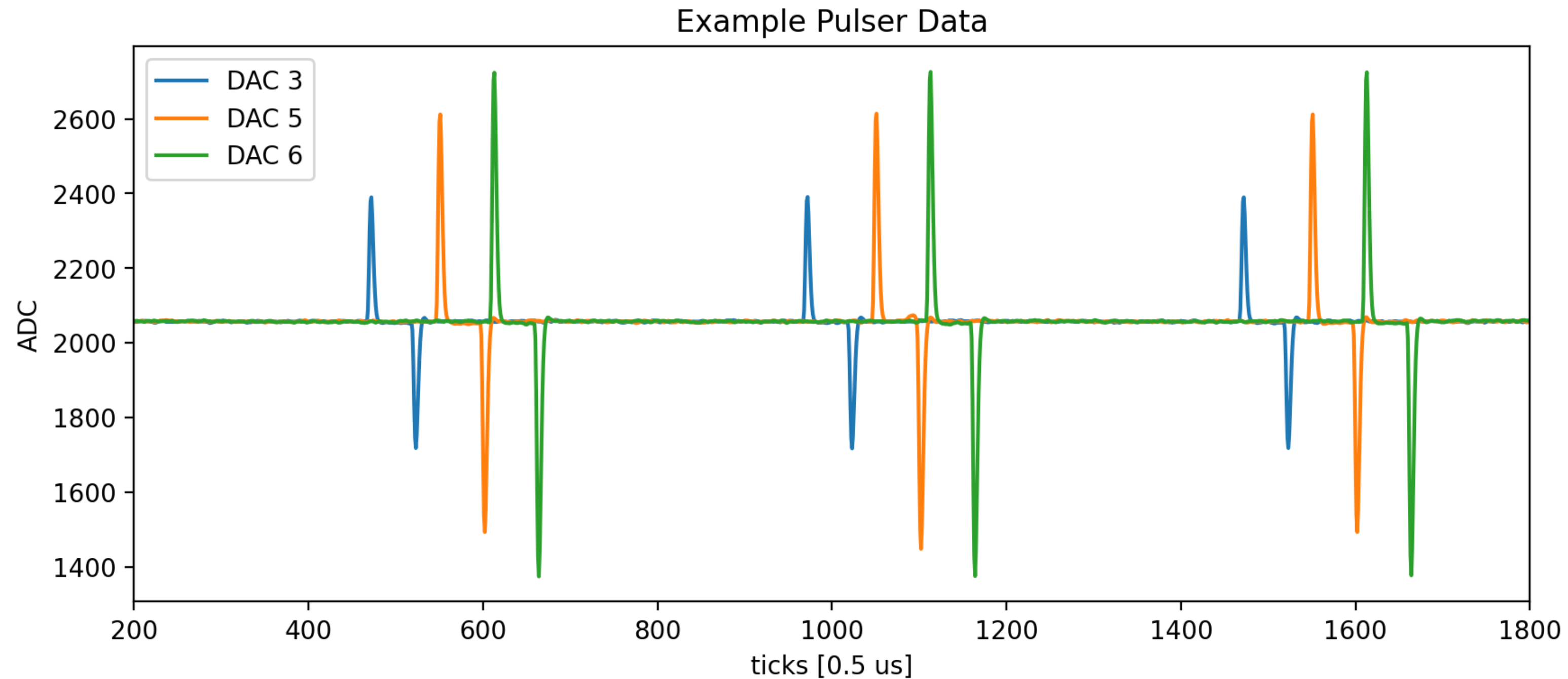
- Electronics response pulser calibrations procedure
 - Calibration Results
 - Calibration Validation
- Using the updated model
 - RC Filter tuning
 - debugging

Electronics Response Calibration Procedure

1. Obtain pulser data for charge-injection values within the linear region (DAC 1-10)
2. Within a single charge-injection value (one run):
 - A. Perform peak finding for many waveforms, results in 60-70 pulses
 - B. Obtain the “average pulse response” to remove noise/cosmic signals
 - median waveform is used, less sensitive to cosmic ionization signals
 - the error of each data point = quartile deviation (less sensitive to outliers)
 - C. Obtain the amplitude and shaping time from fitting the electronics response function
3. Extract the **gain** from the DAC vs. fitted amplitude
4. Extract the **shaping time** as a weighted average from all DAC values

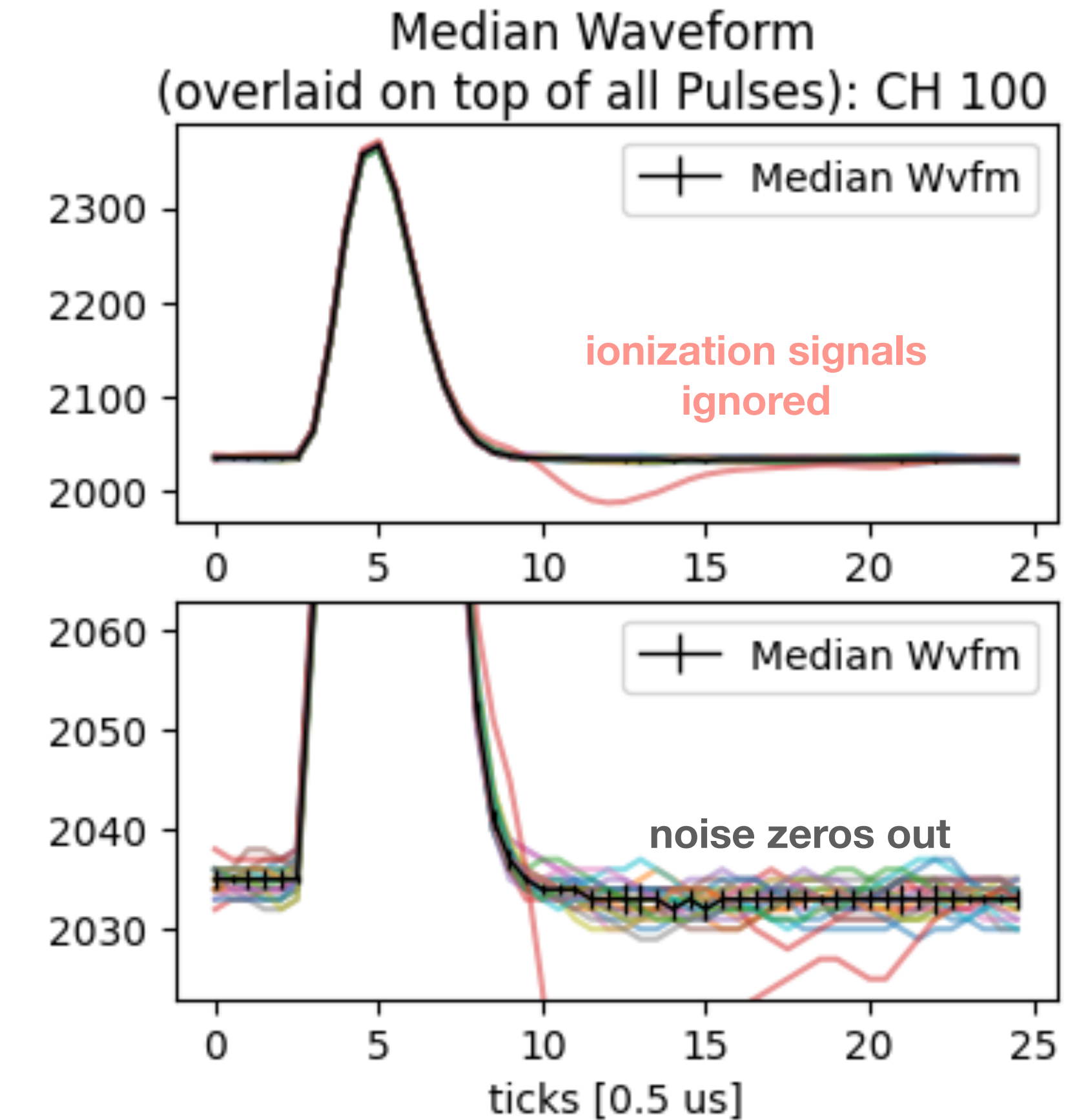
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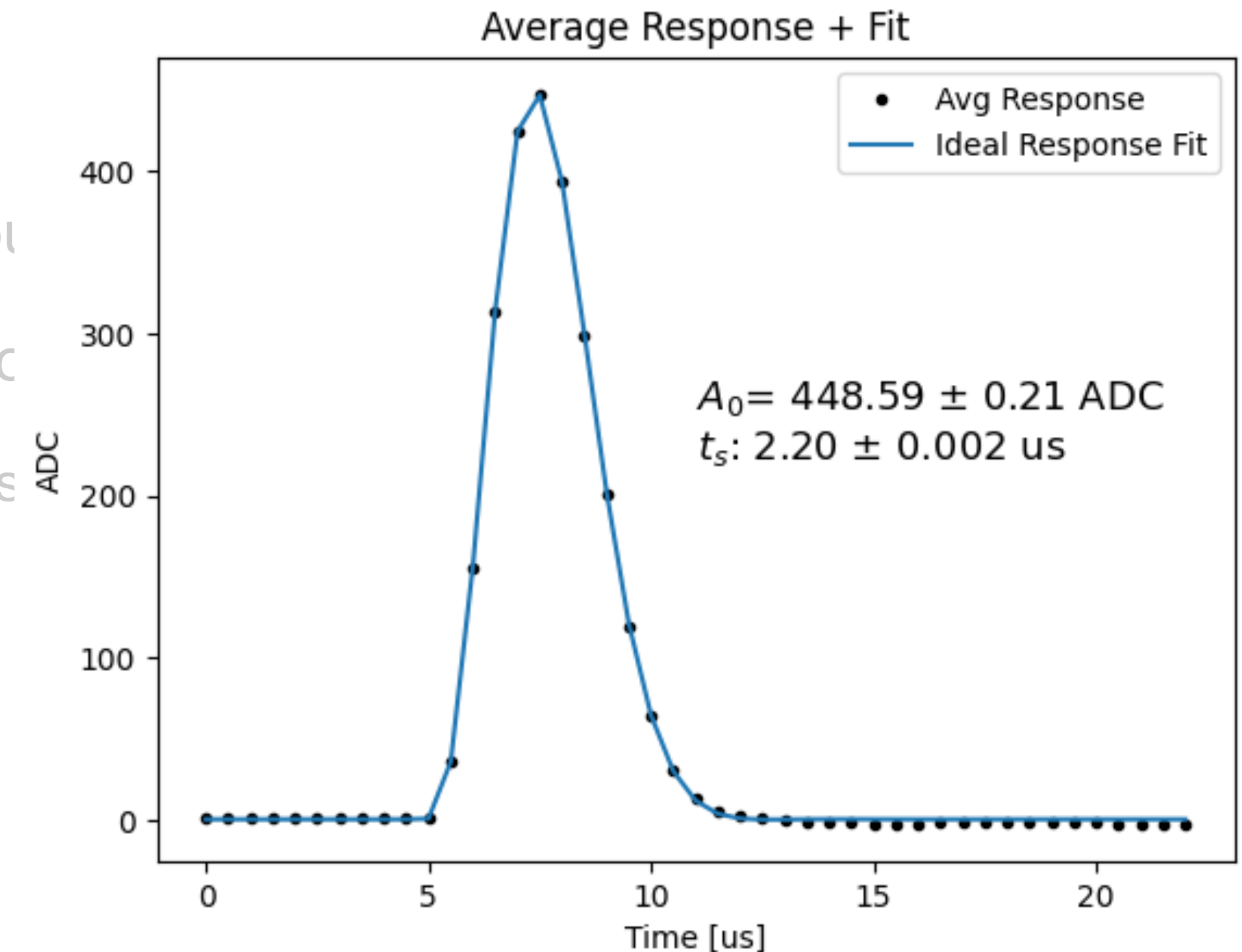
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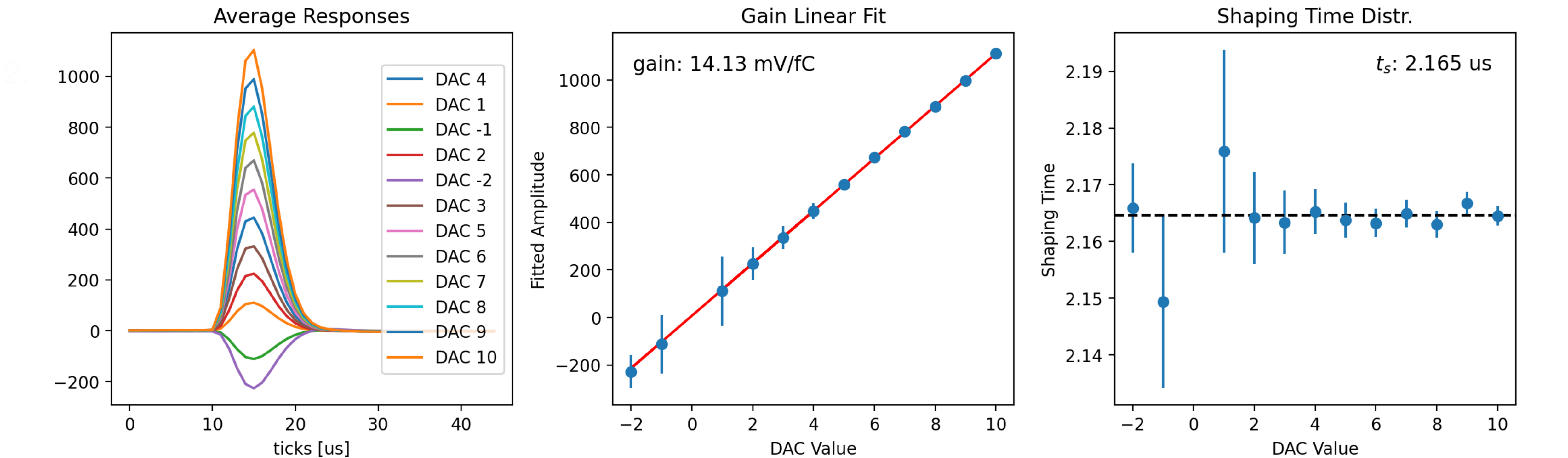
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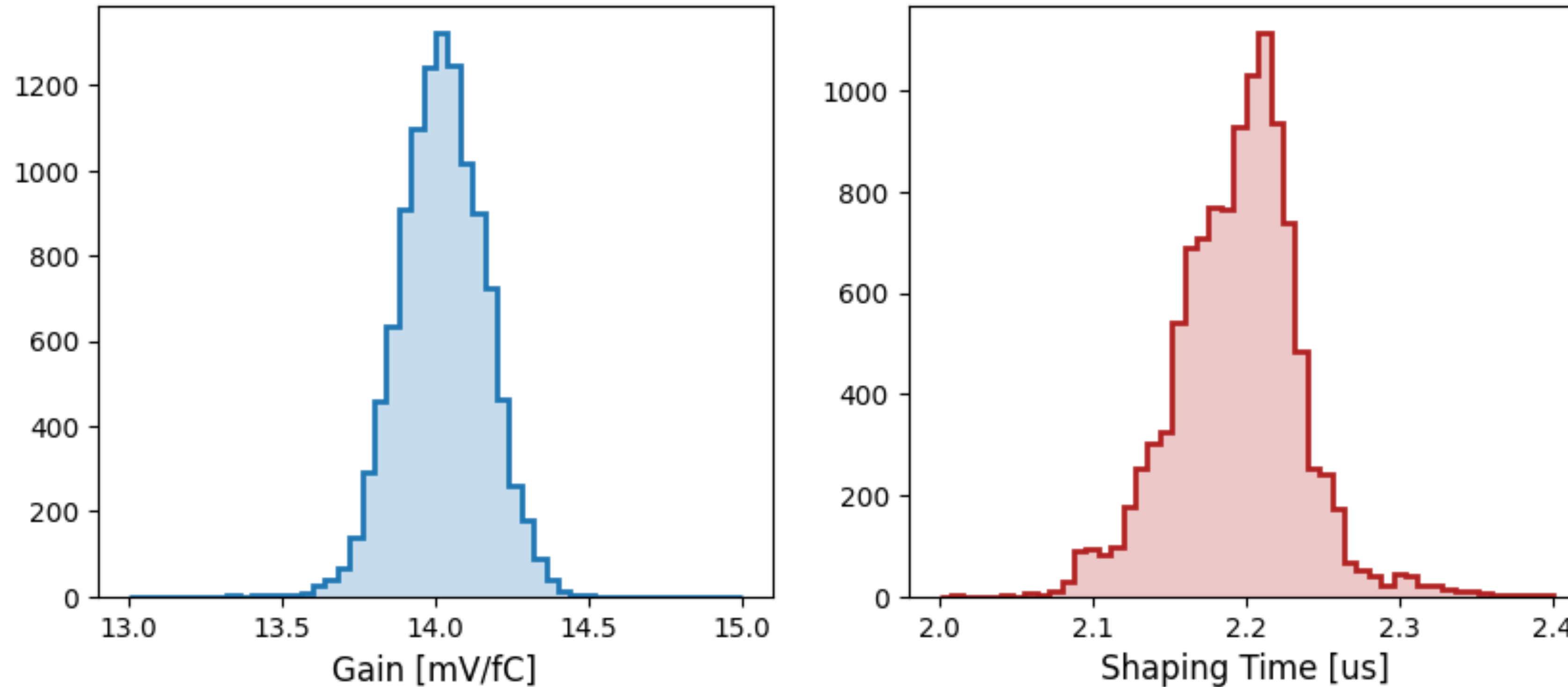
Sanity Check Plots: CH 7484



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Calibration Values

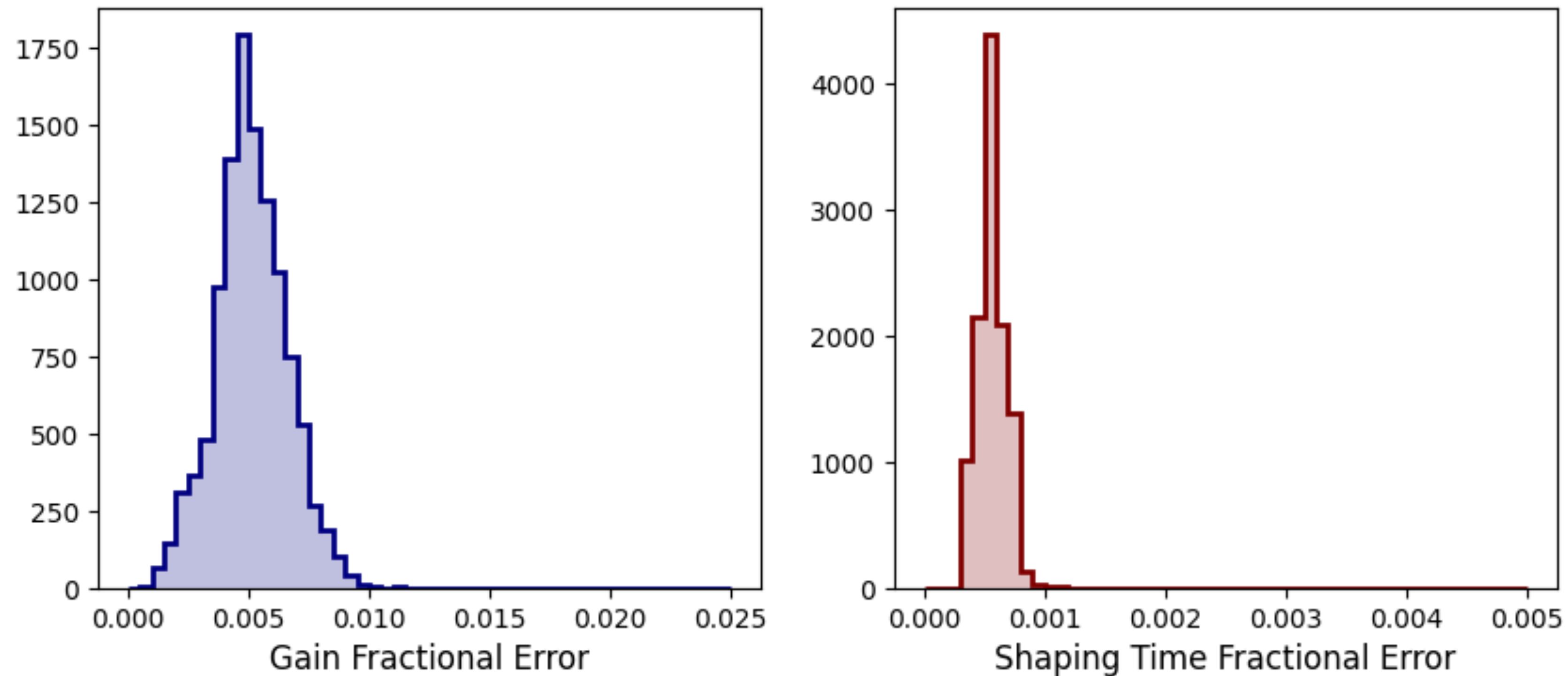
Fitted Gain and Shaping Time Distributions



- obtain gain and shaping time for all channels!

Calibration Value Errors

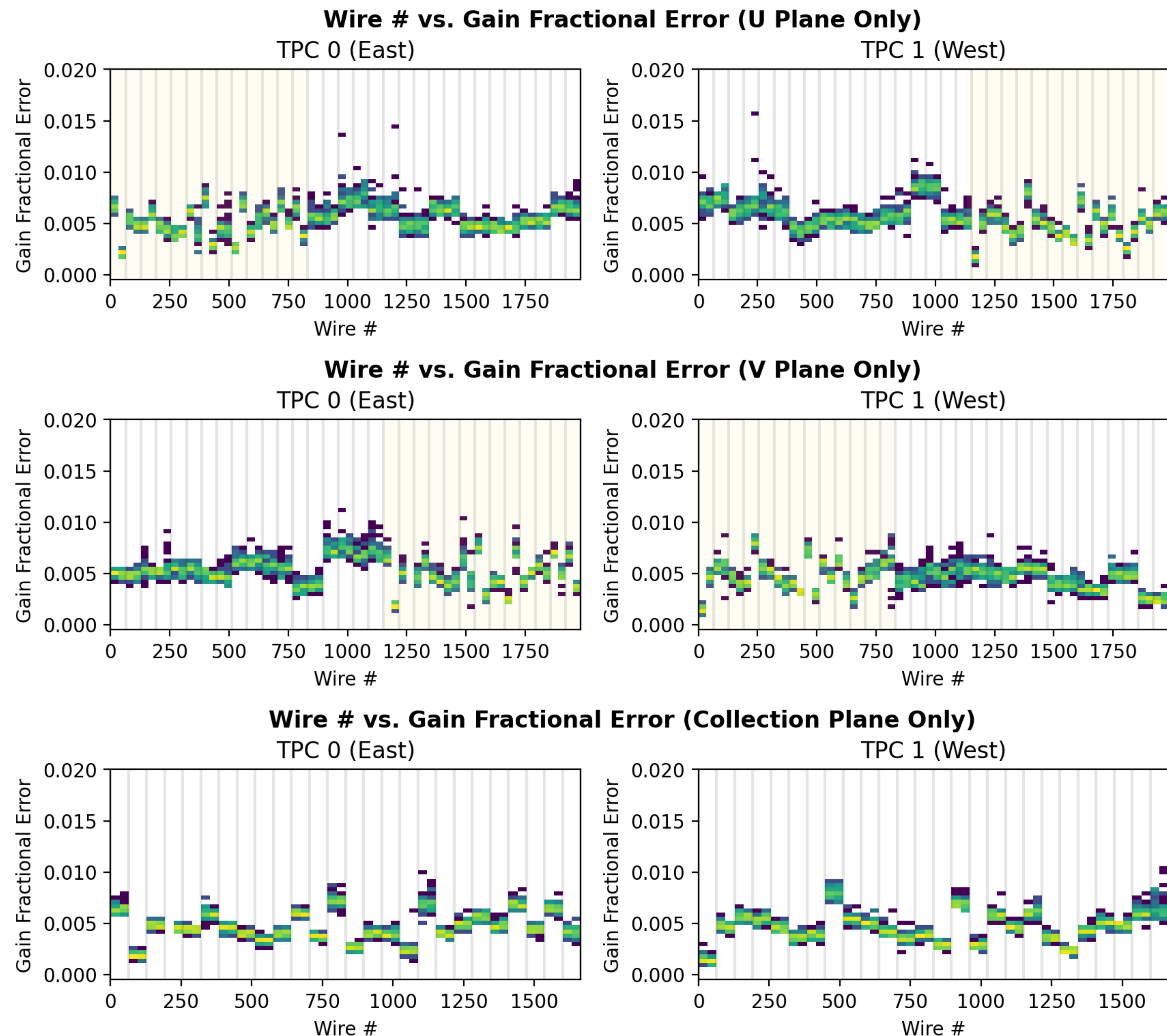
Fitted Gain and Shaping Time Errors



- distributions of the fractional error for both calibration parameters
 - error on the gain obtained directly from the linear fit, error on the shaping time is the error on the weighted average

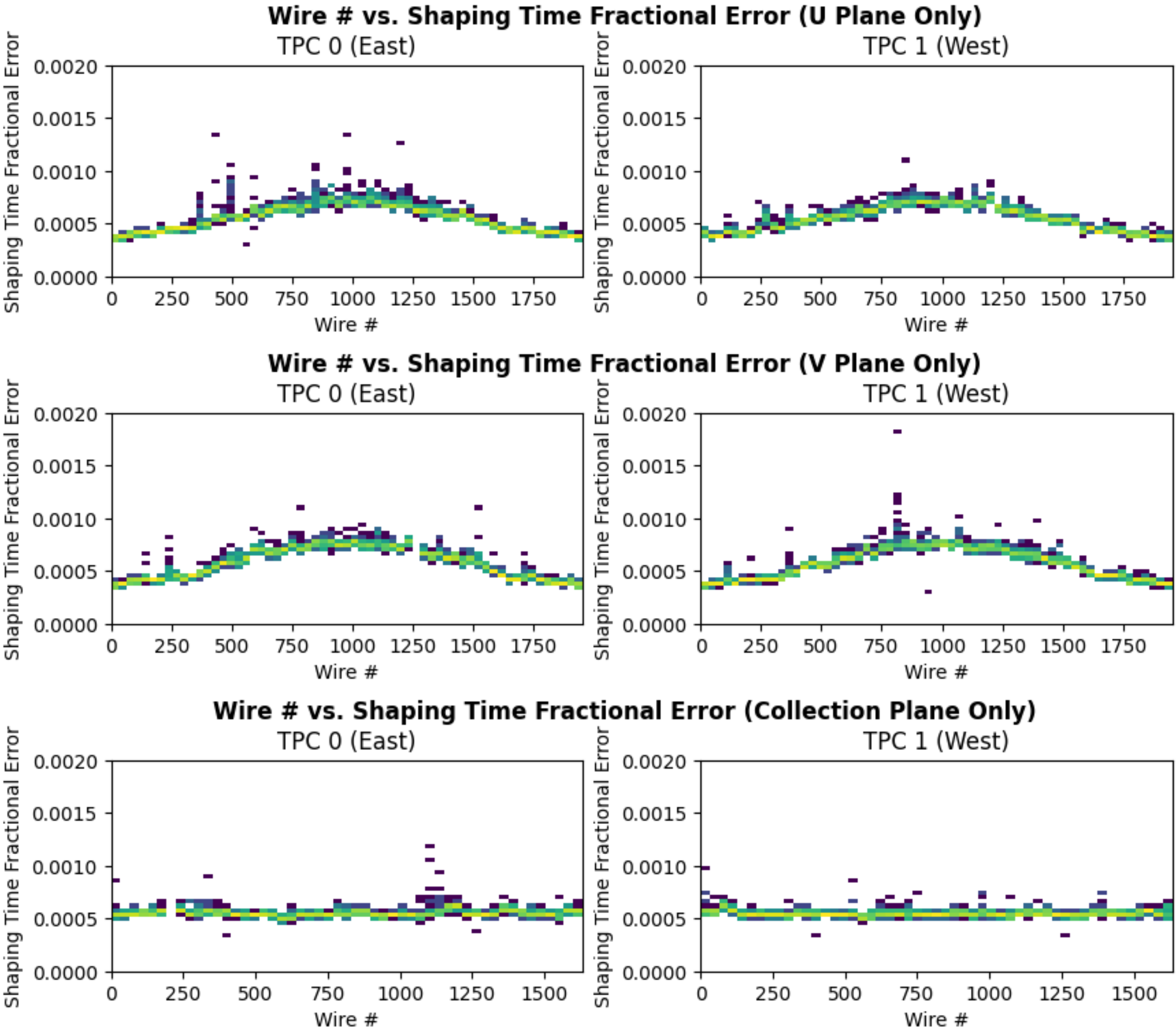
Fit Performance vs. Wire

- gain fractional error
- vertical lines separate groups of 64 channels
- induction planes with CE installed at the TPC sides seem to have 32 wire grouping vs those installed on the TPC top, which seem to have 128 wire grouping
- collection planes have grouping by 64 channels

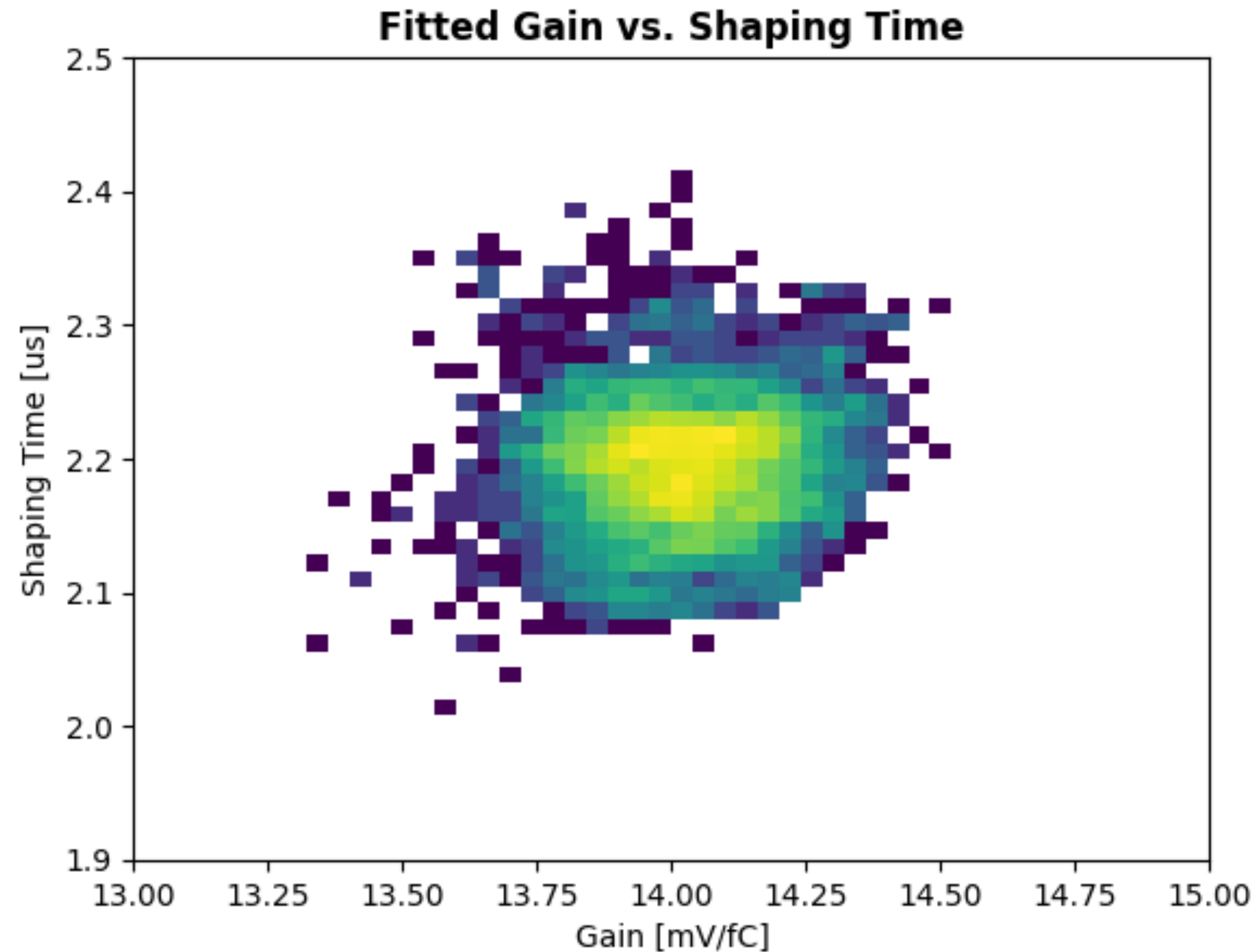


Fit Performance vs. Wire

- shaping time fractional error
- no clear wire grouping, but clear wire length dependency!



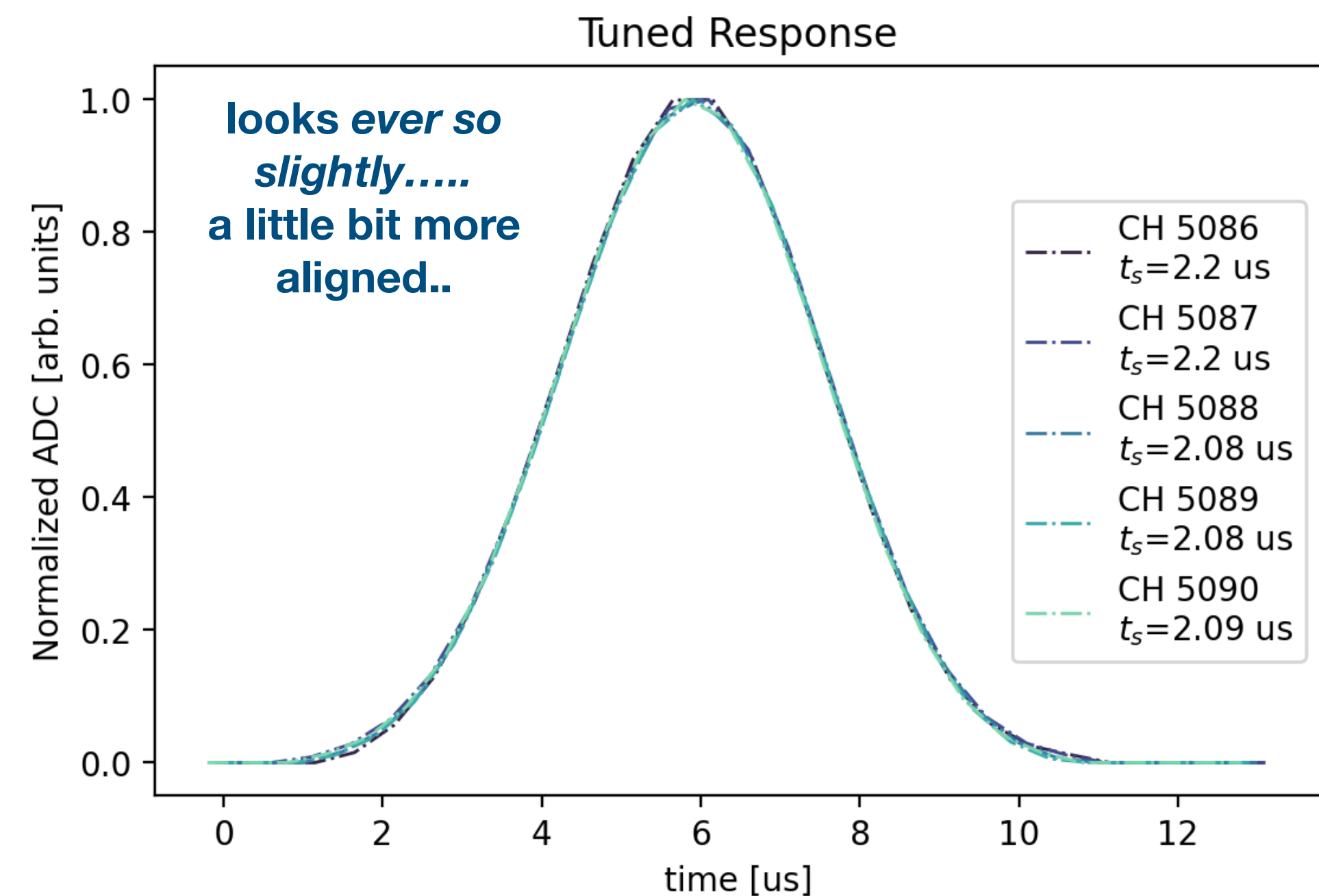
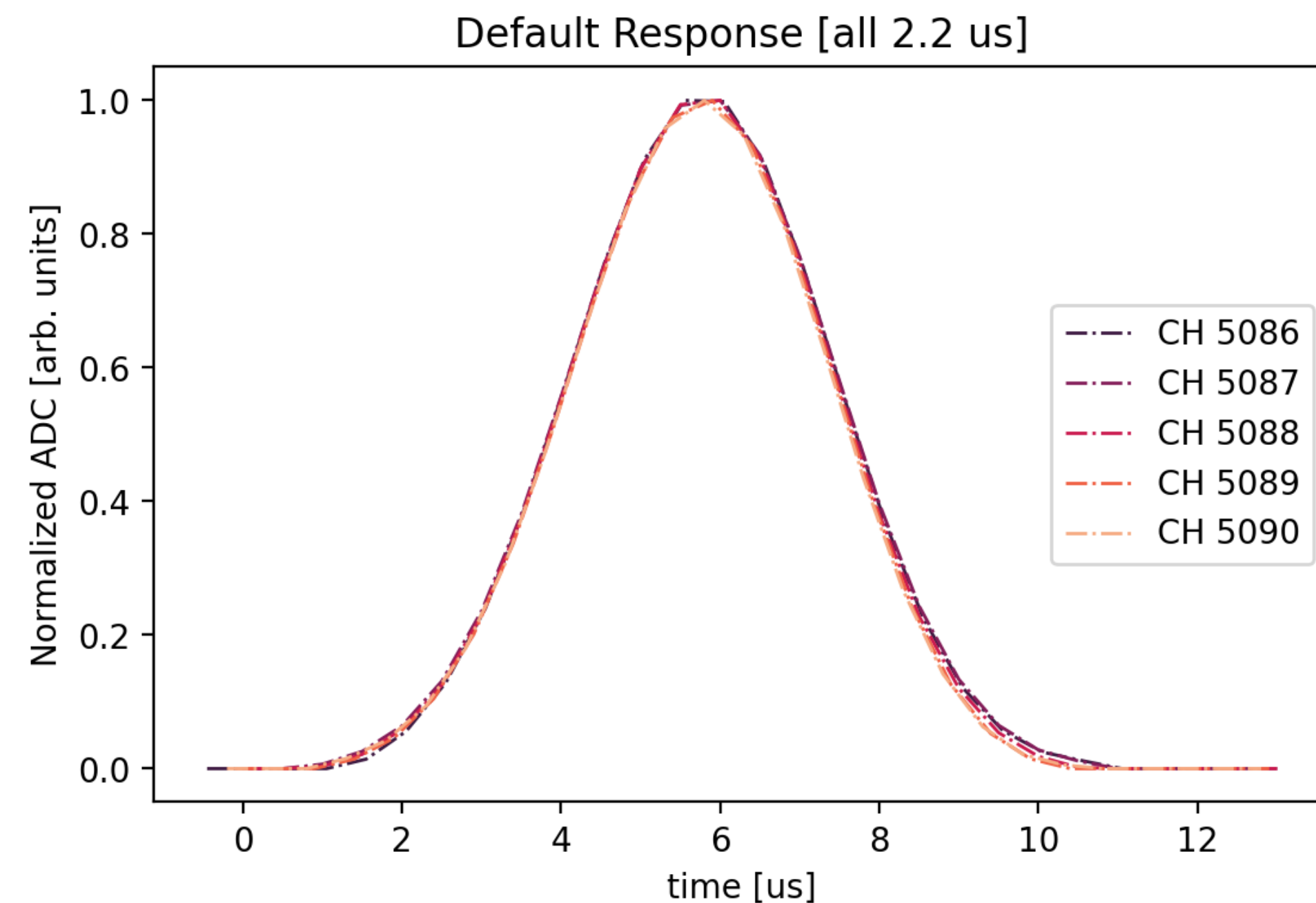
Sanity Check!



- we don't expect the gain and shaping time to be clearly correlated, so this looks good

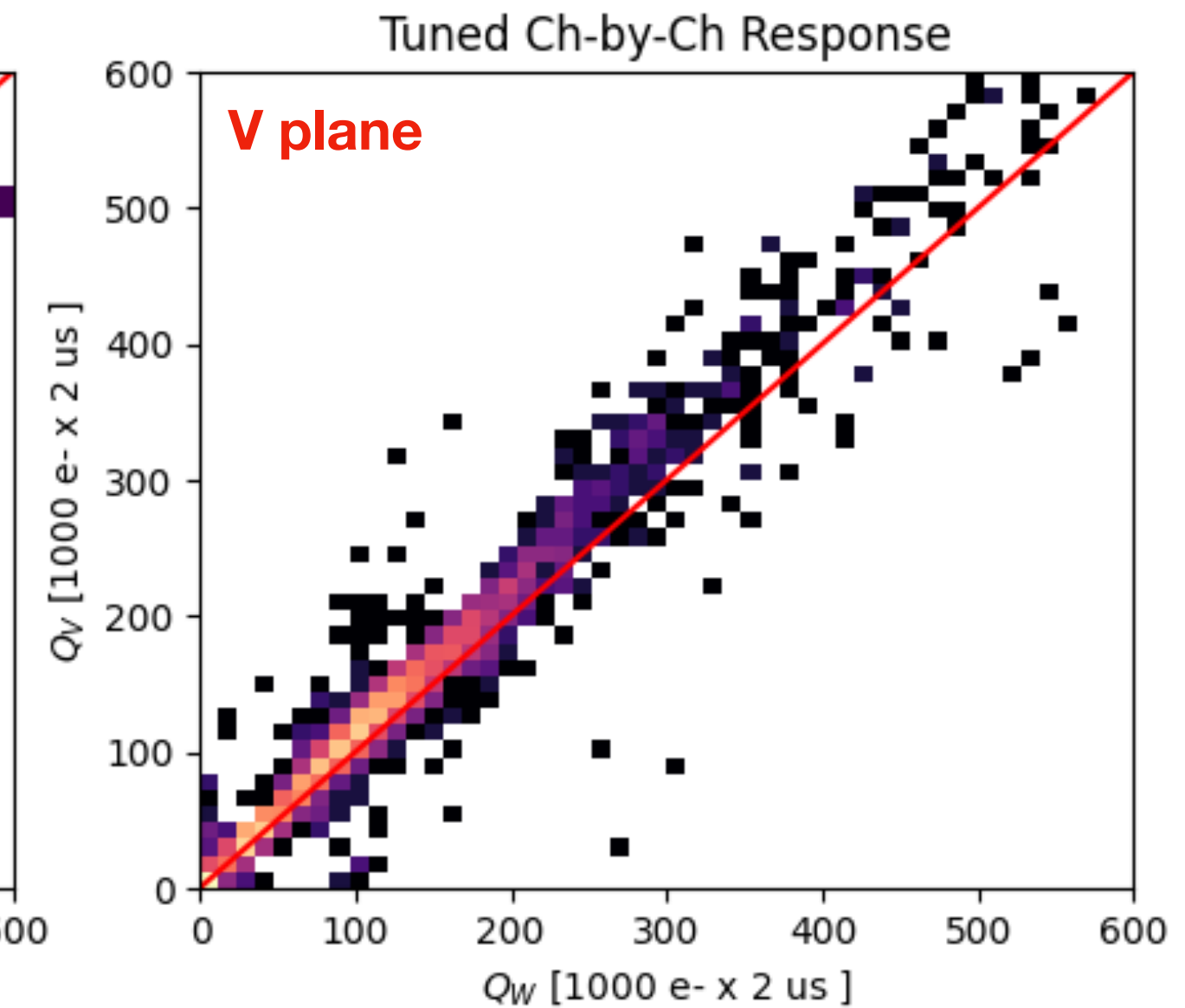
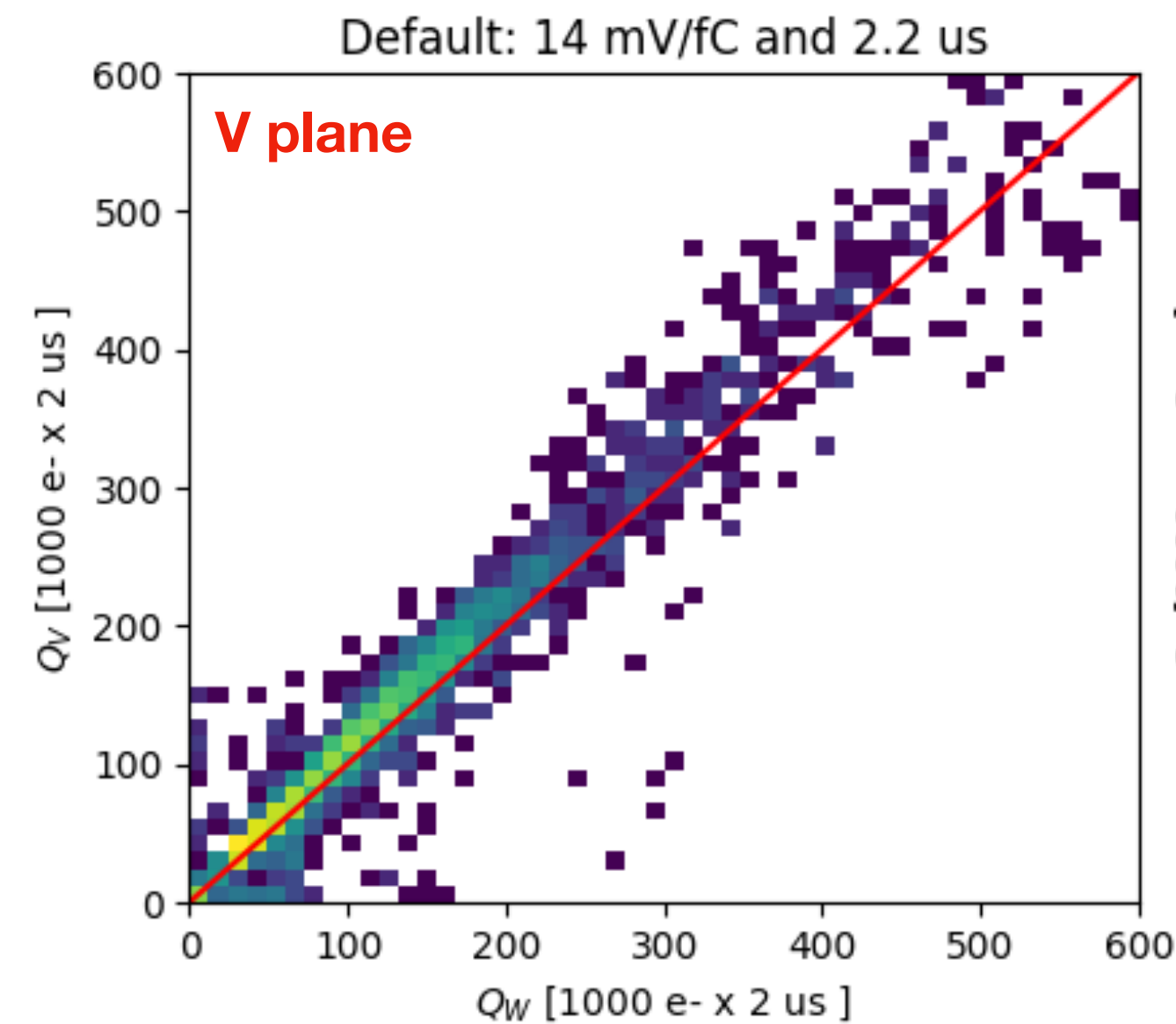
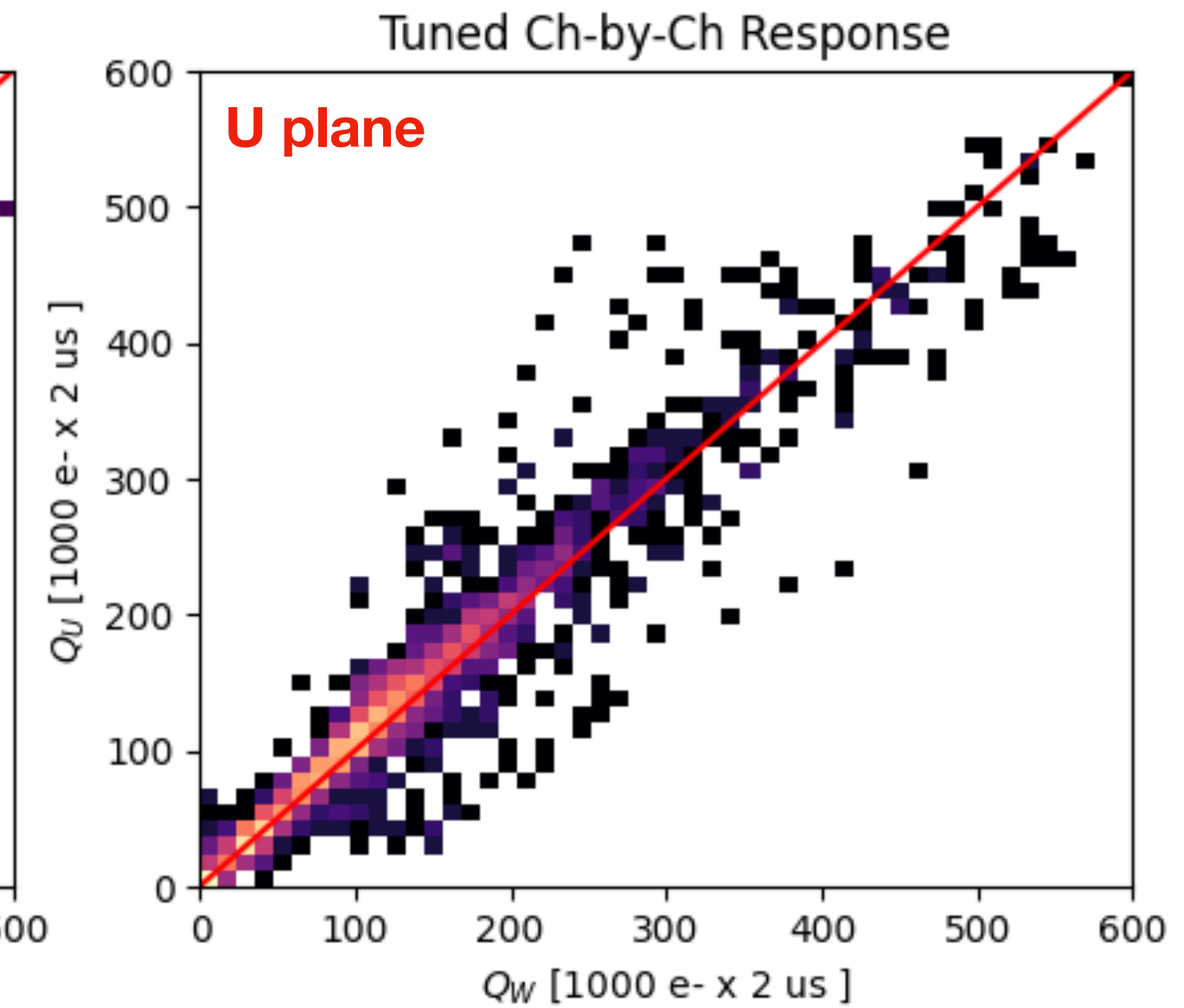
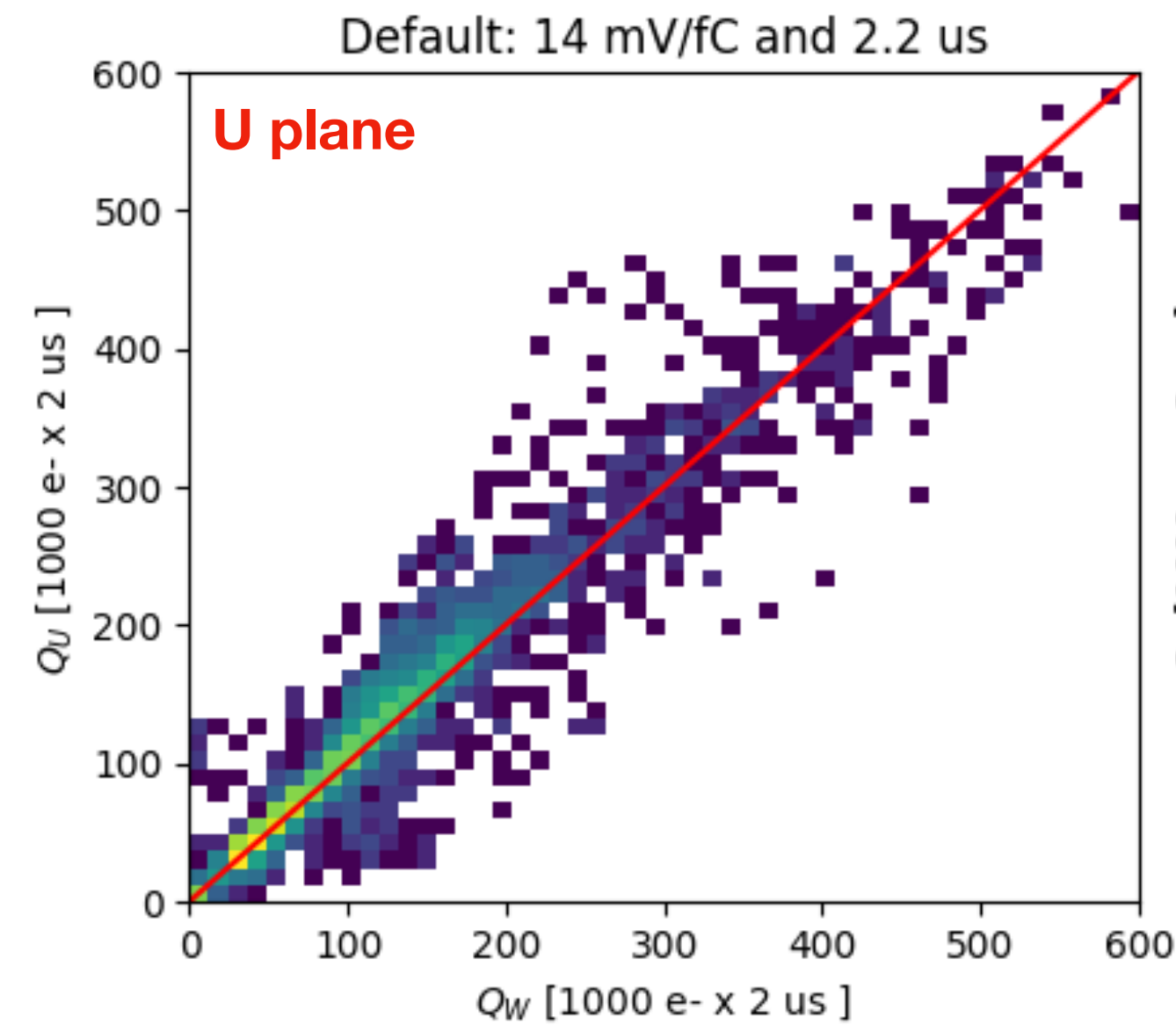
Validation with Calibrated Values

- validation with data is somewhat challenging; the improvement that we expect to see is *at most* on the few percent level, more likely even less after the inherent smearing of signal processing
- validation with full reconstruction, accurate dx correction, and larger statistics may help!

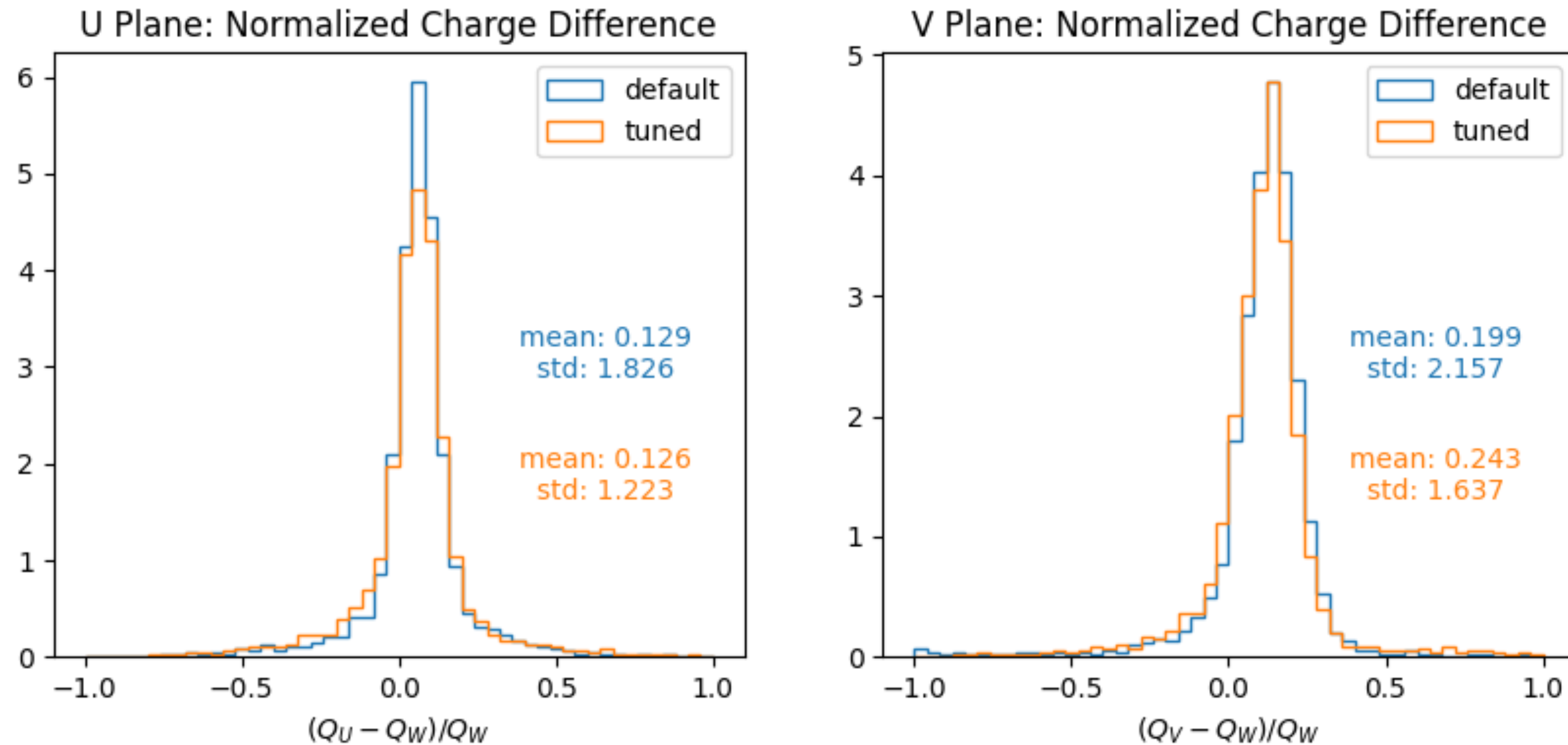


Calibration Validation

- some very basic validation using waveforms only:
 - matching the integrated deconvolved charge over time slices (4 ticks = 2 us), we can compare the extracted charge from the induction planes to the collection plane
- **outcome:** both the default and the tuned comparisons show good matching (with some bias)
- using the tuned response leads to better charge resolution!



Calibration Validation

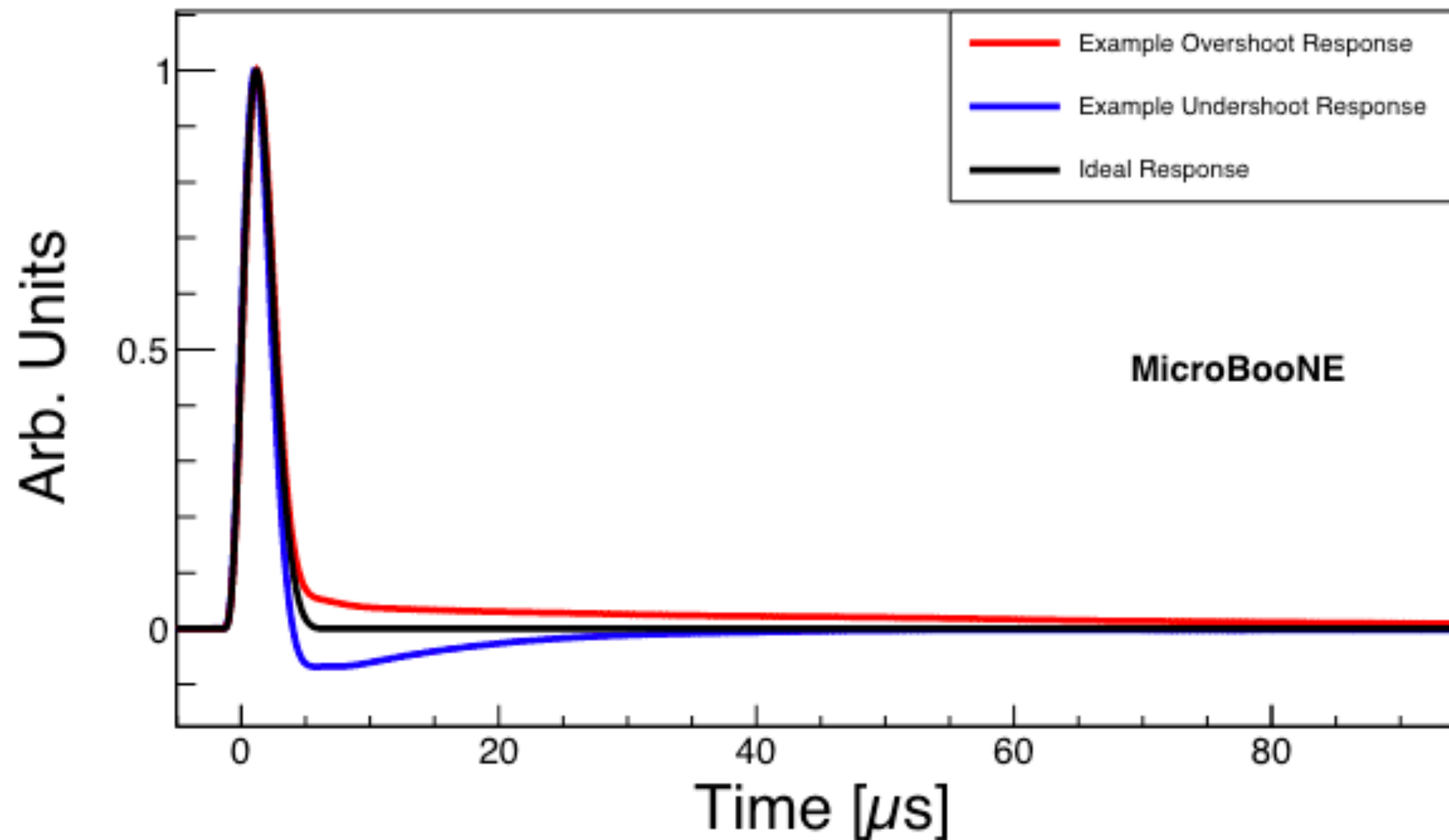


- the charge agreement between the induction planes and collection planes has overall improved using the tuned electronics response
- caveat: the mean and standard deviation are not great metrics due to the outliers in the distribution, but just using them as a first look!

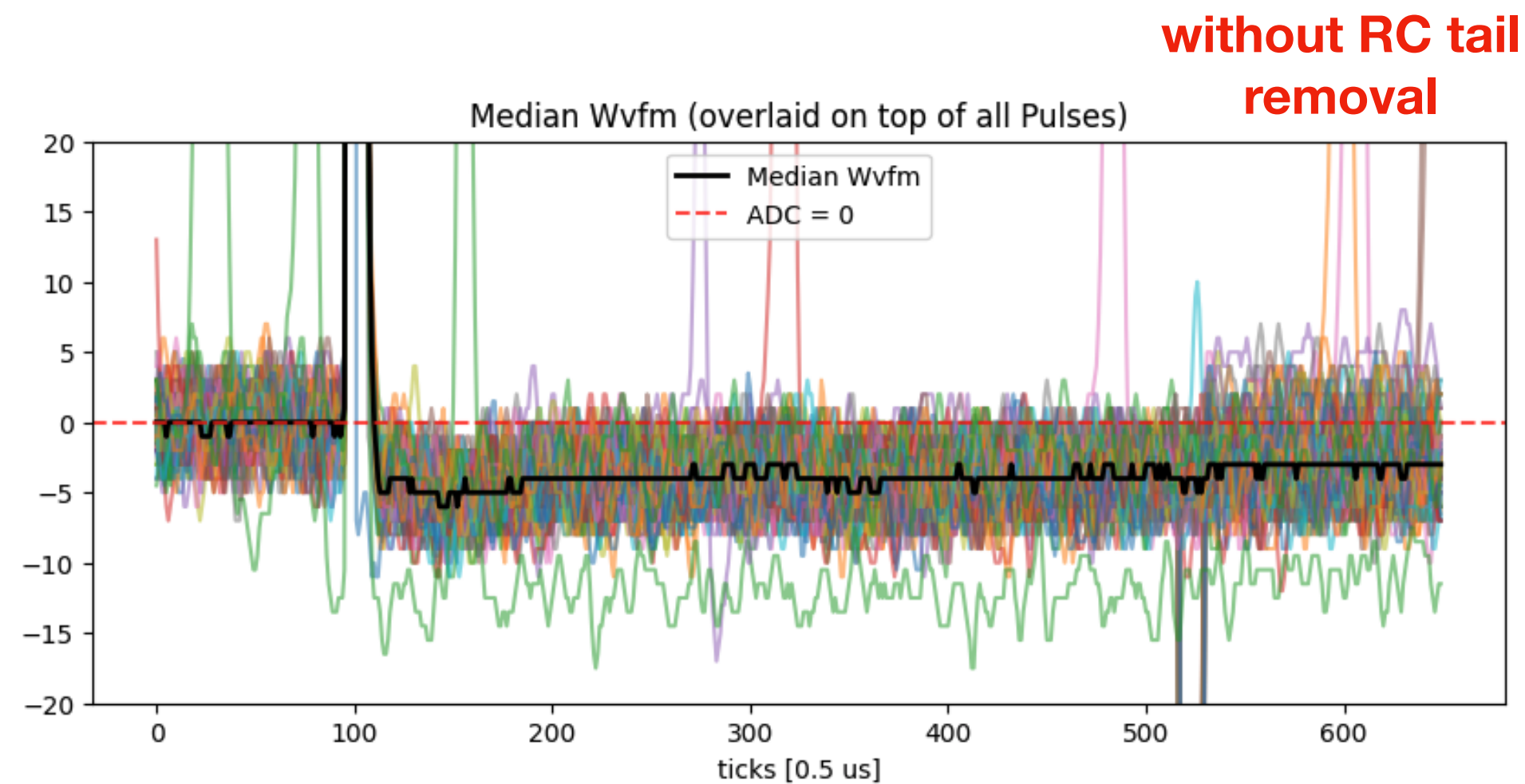
Updated Model (Imperfect Pole-Zero Cancellation)

Imperfect Pole-Zero Cancellation

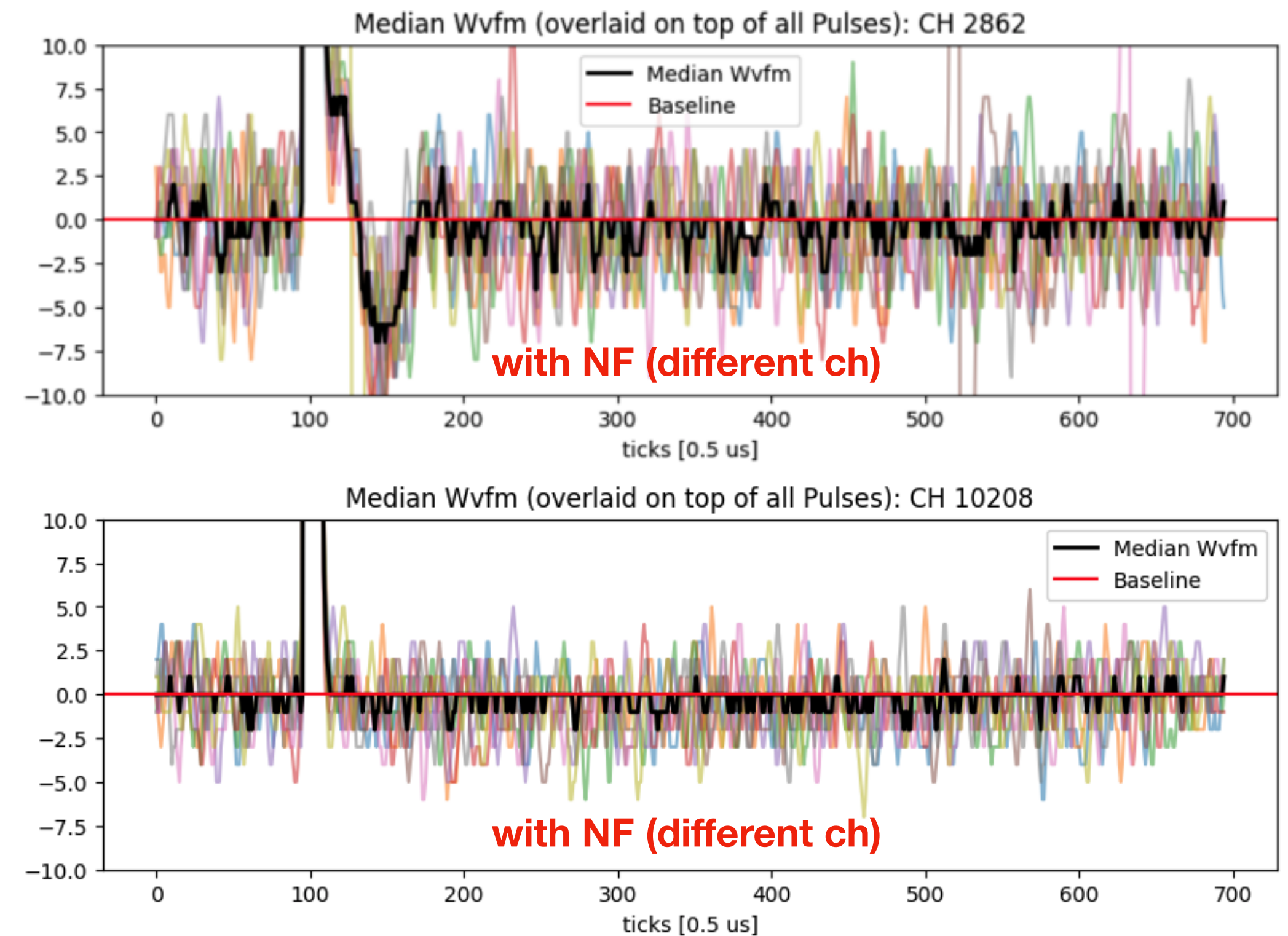
- although this model works well in many cases, the ideal electronics response does not account for some effects, such as *undershoot* and *overshoot* tails due to imperfect pole-zero cancellation



but first... RC effect

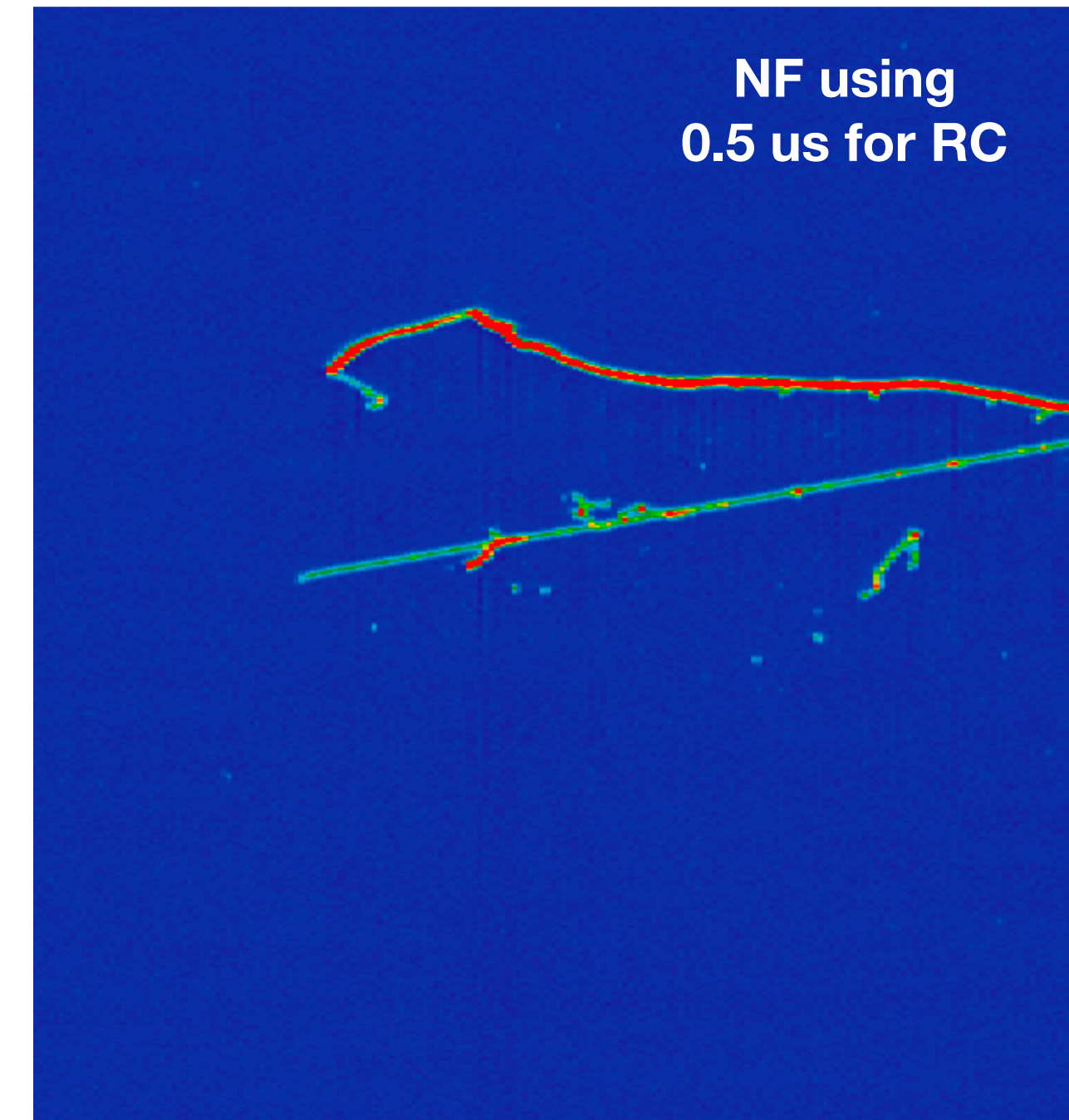
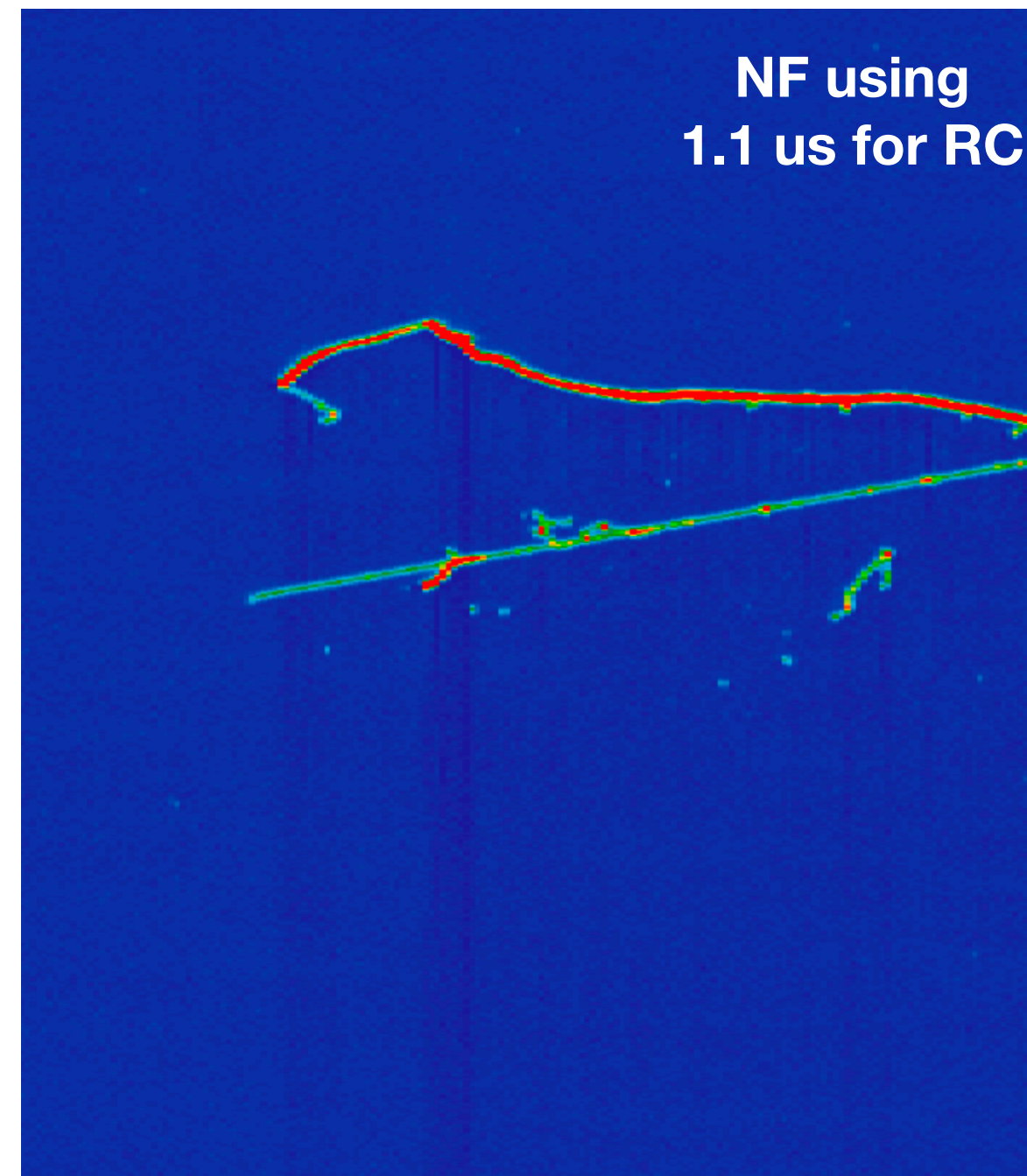
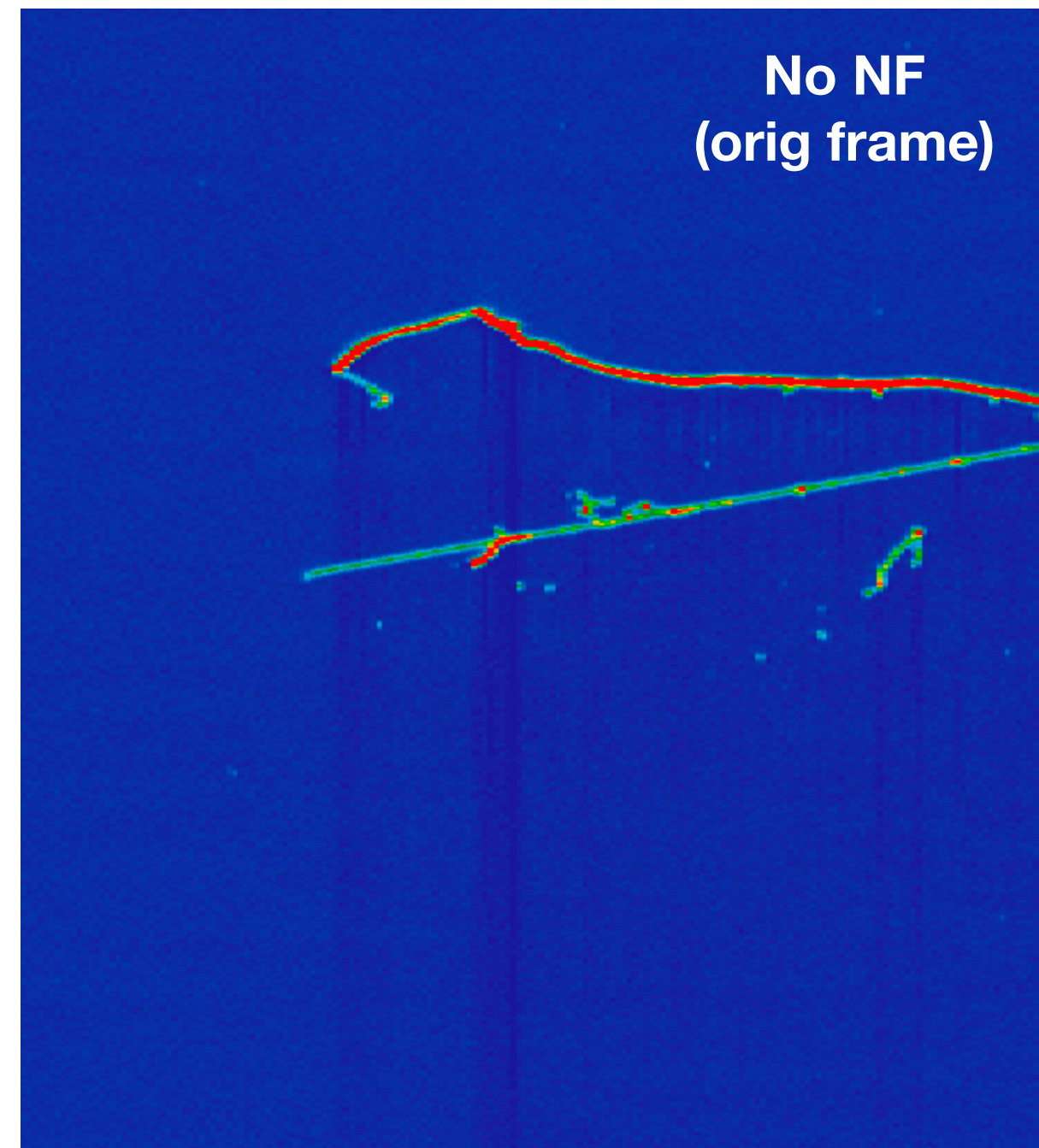


- when inspecting waveforms for small undershoots in the tail, noticed that nearly all had a small undershoot with very long time constant \rightarrow RC tail!



- need to remove the RC tail to properly characterize possible undershoot/overshoot effects due to pole-zero cancellation
- using NF waveforms (with coherent noise removal turned off)

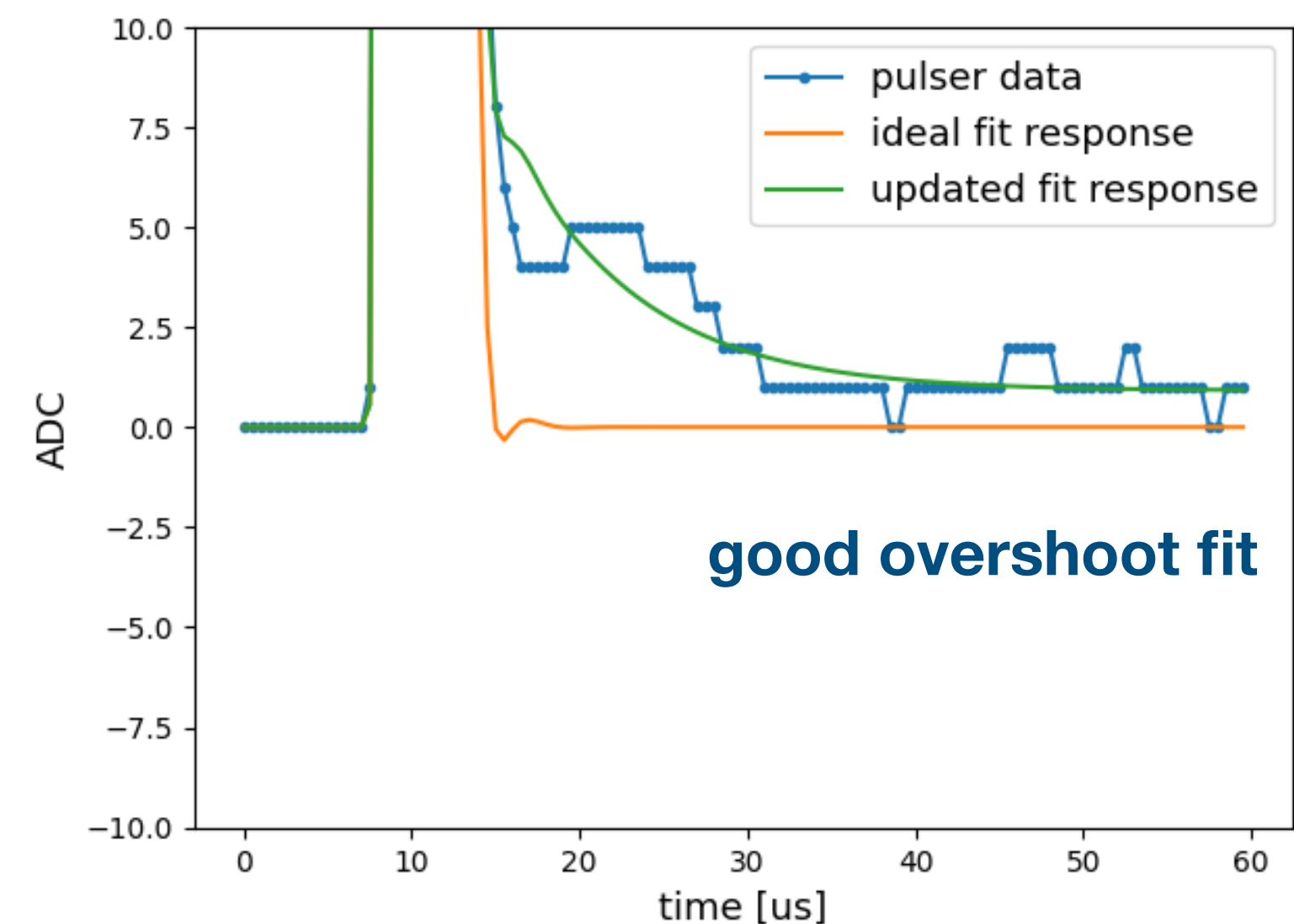
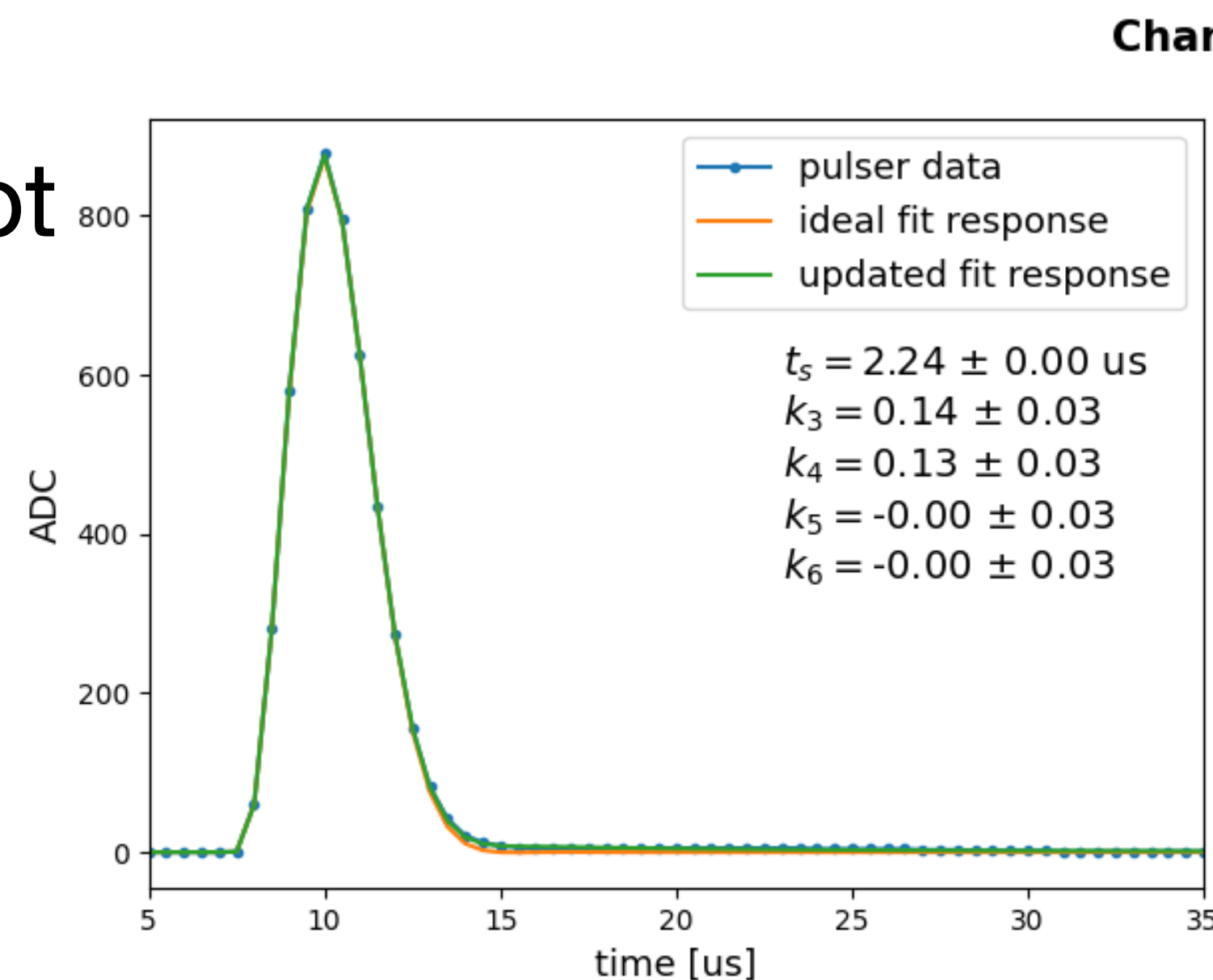
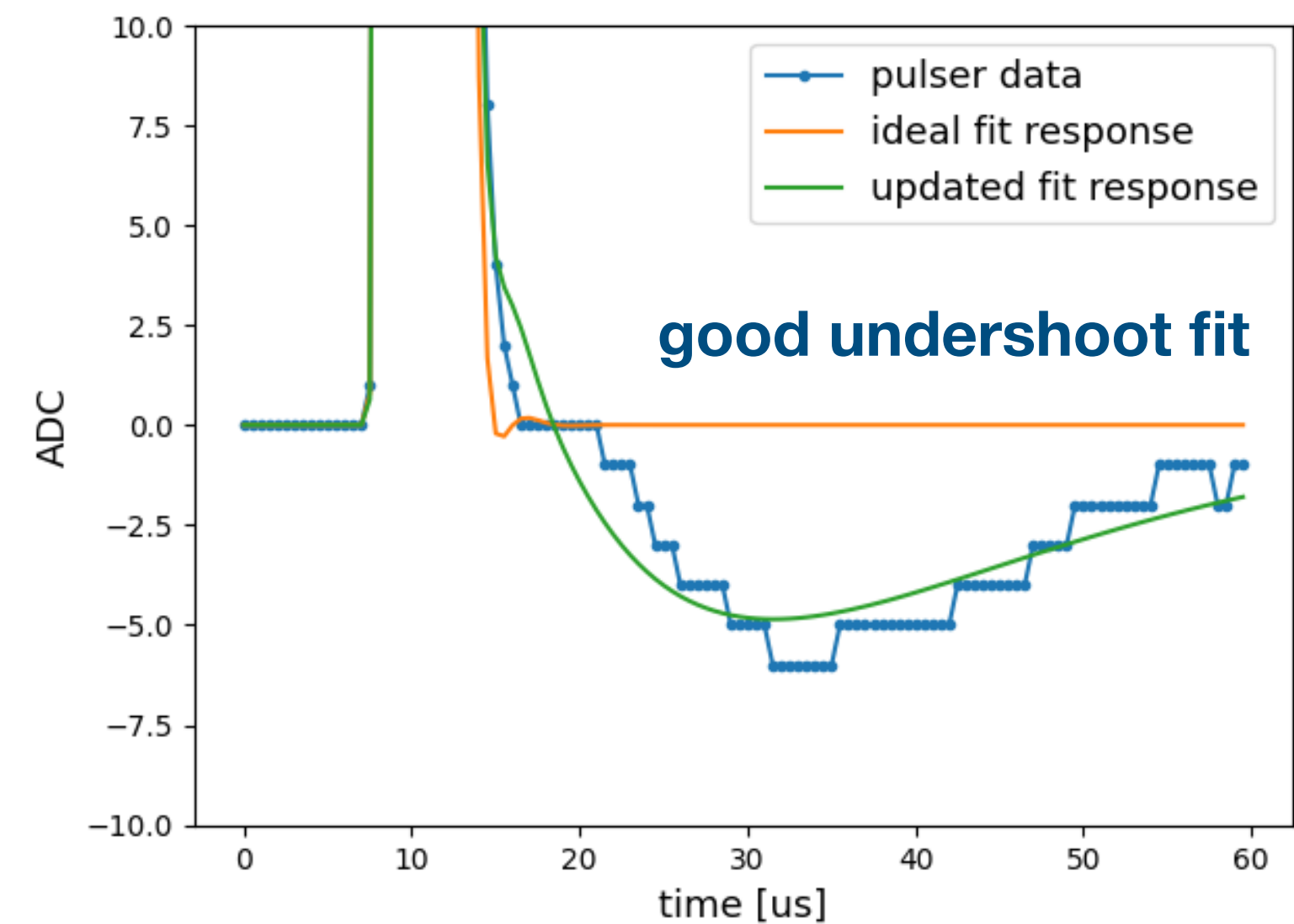
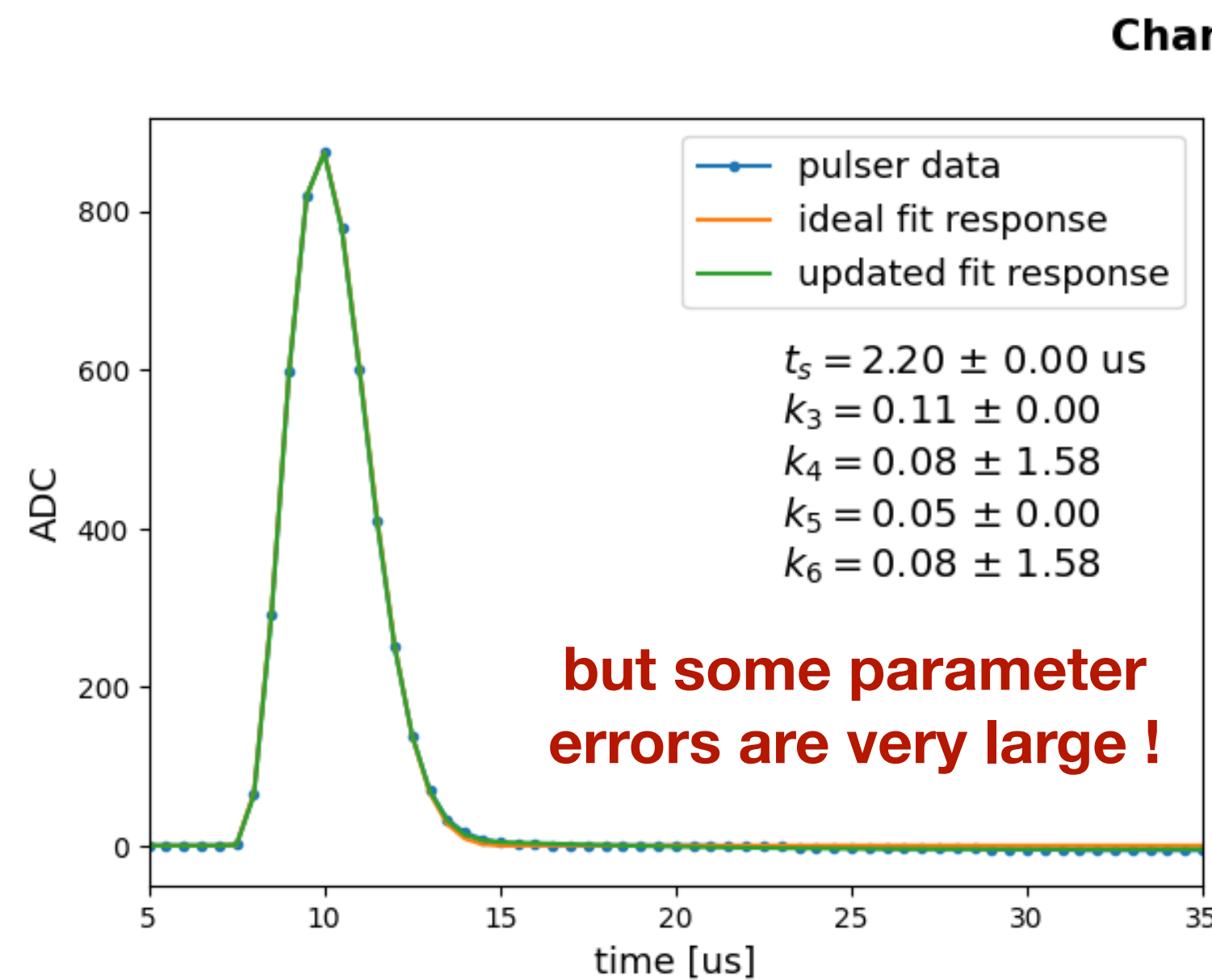
RC effect (cont.)



- the value of the RC time constant needed to remove the observed tail was very different from the expected
 - Shanshan reported **1.1 μ s** from his tests
 - after testing many values and comparing waveforms (backup) and event displays, **0.5 μ s** seemed to be most effective in removing the observed tail

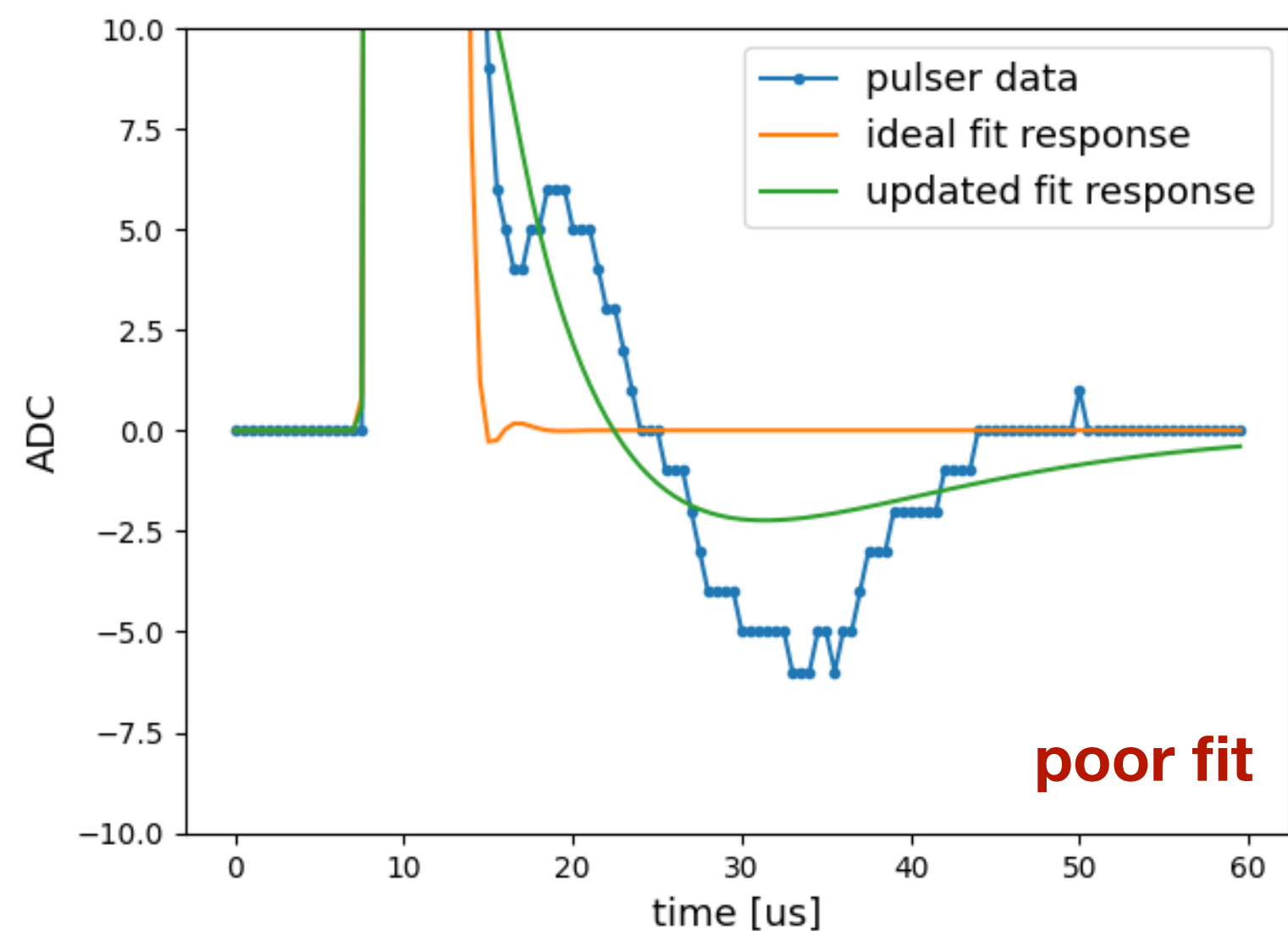
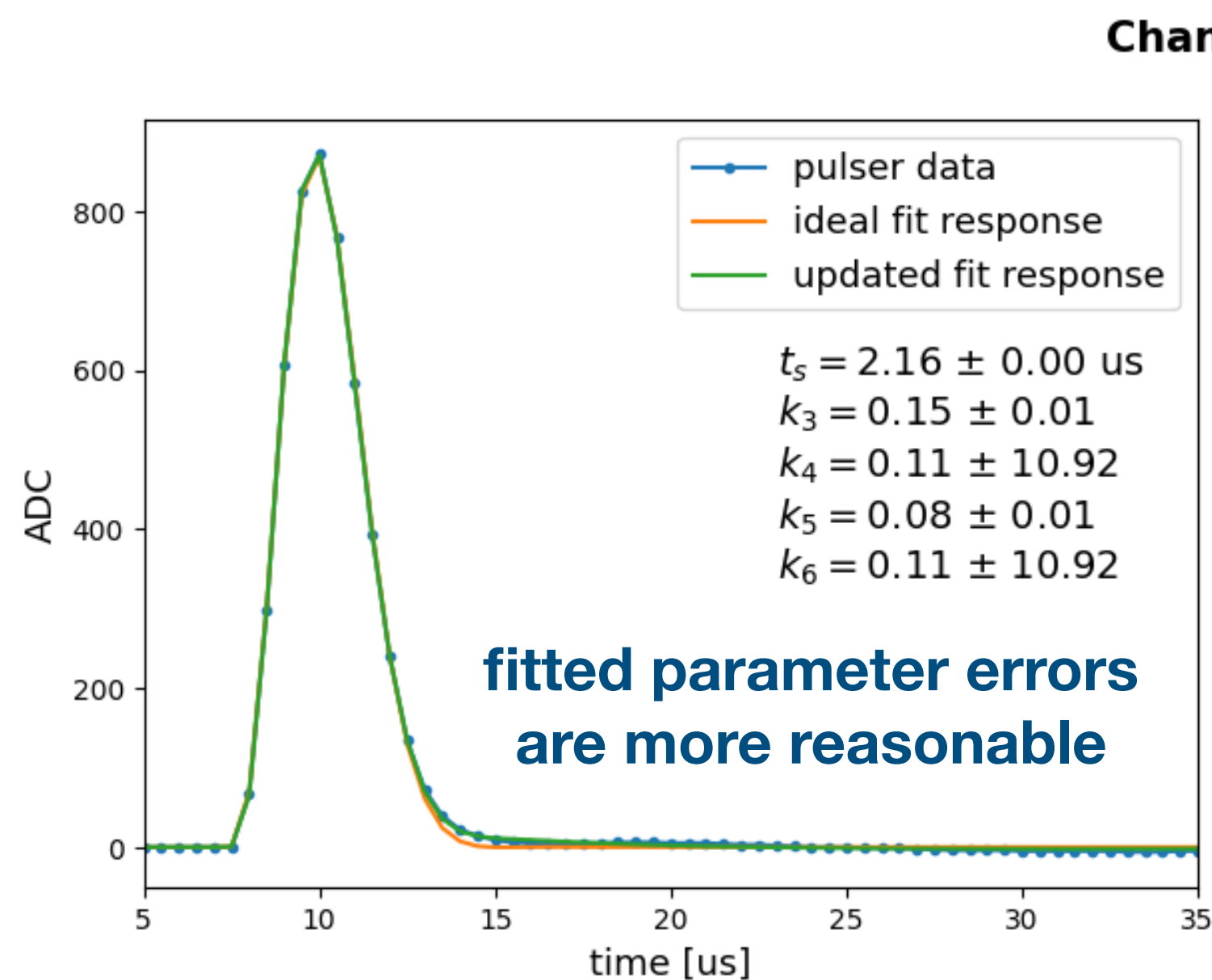
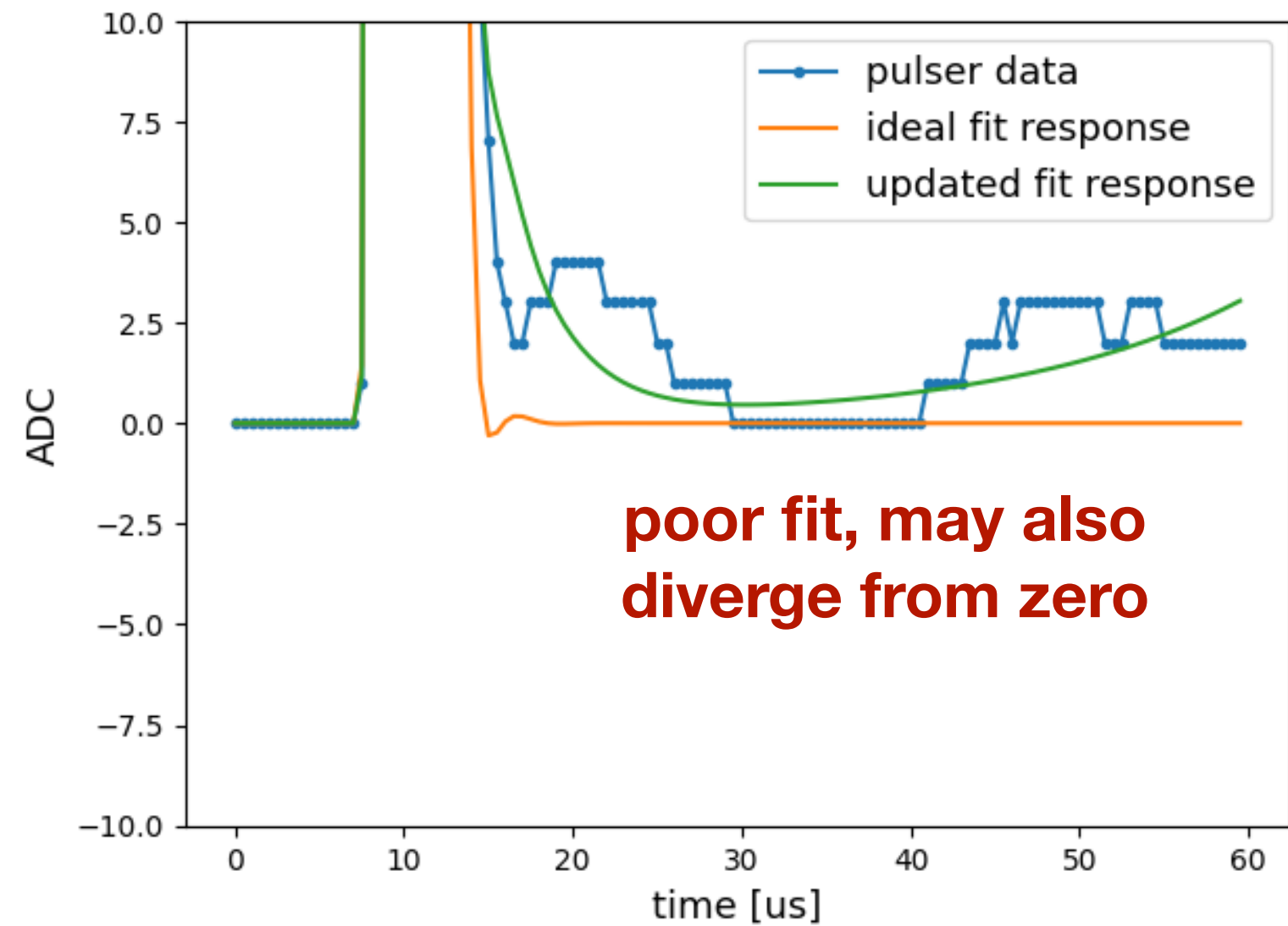
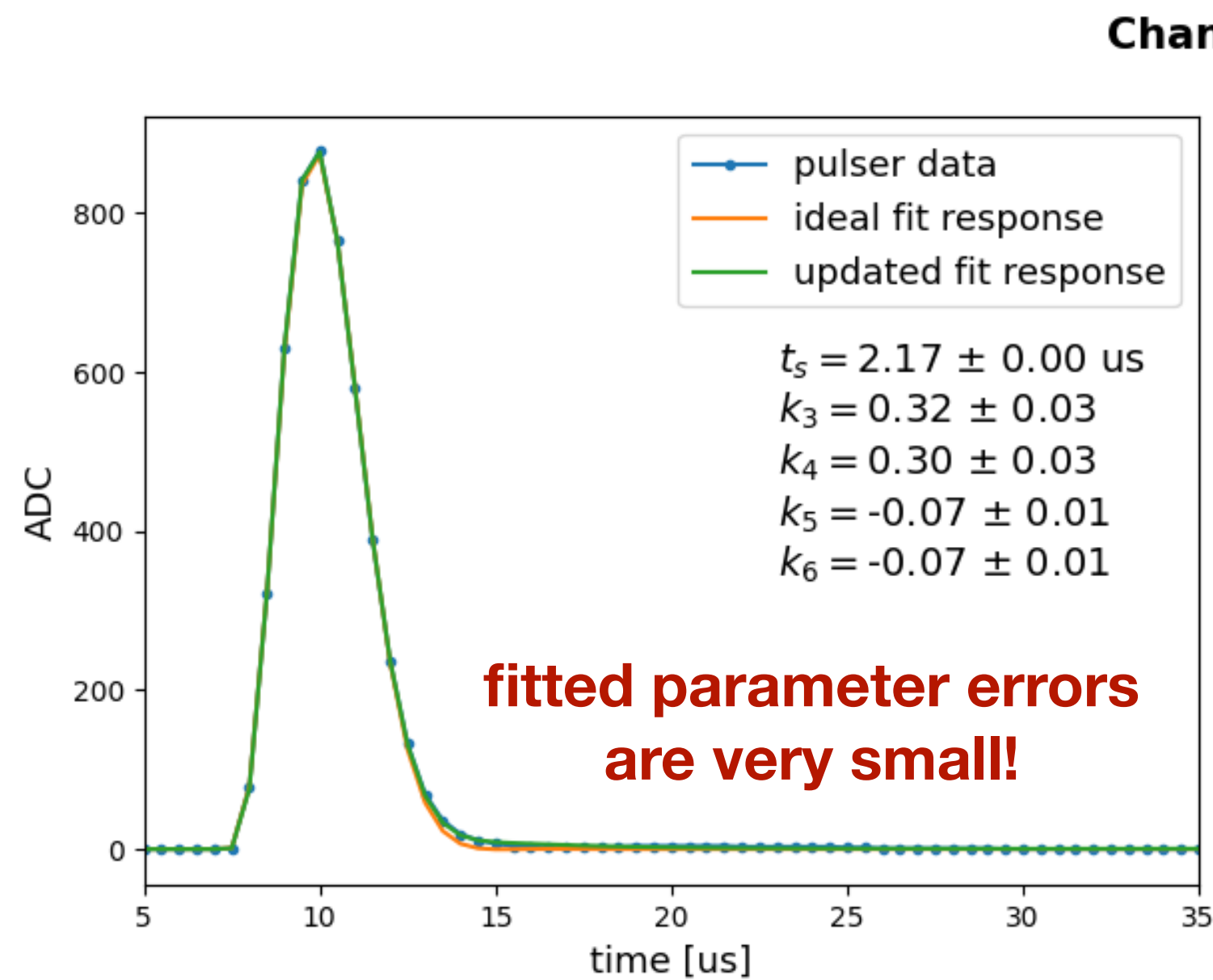
Updated Response Model

- for shaping studies with updated model, using 100+ pulses with DAC 8
- the updated response model can account for some features we also see in our pulser data
- the undershoot and overshoot effects in SBND pulser data are *very small* compared to the main response



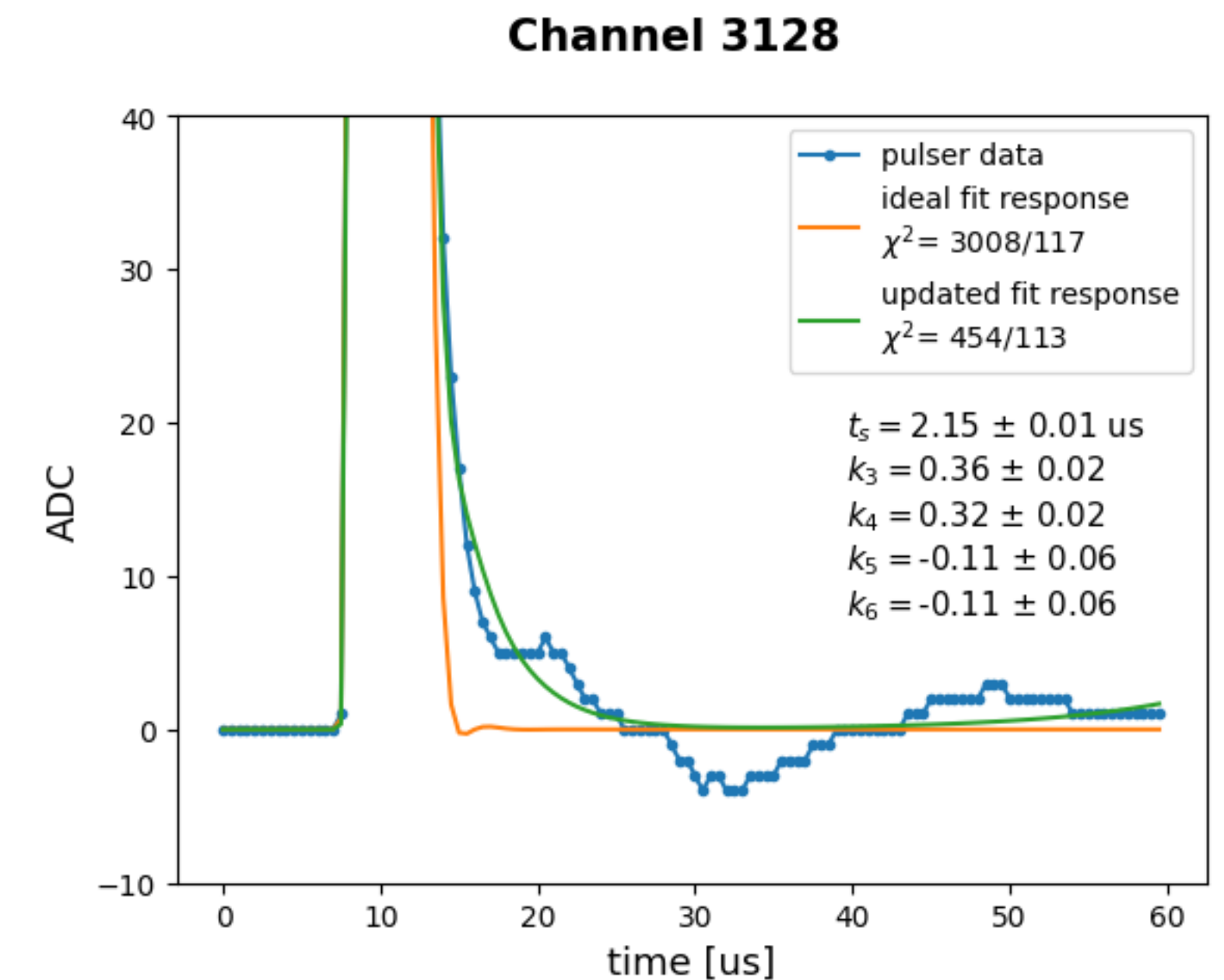
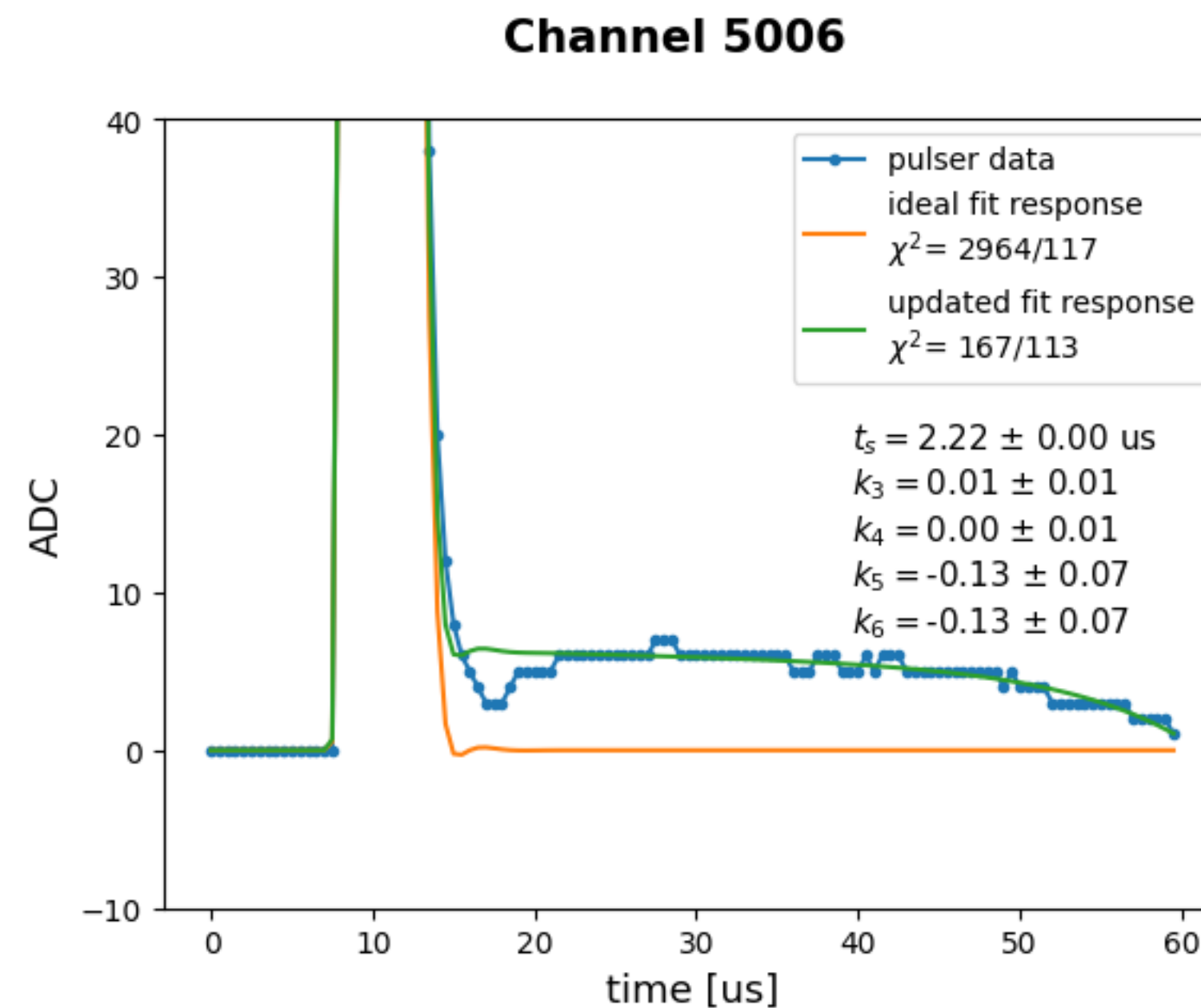
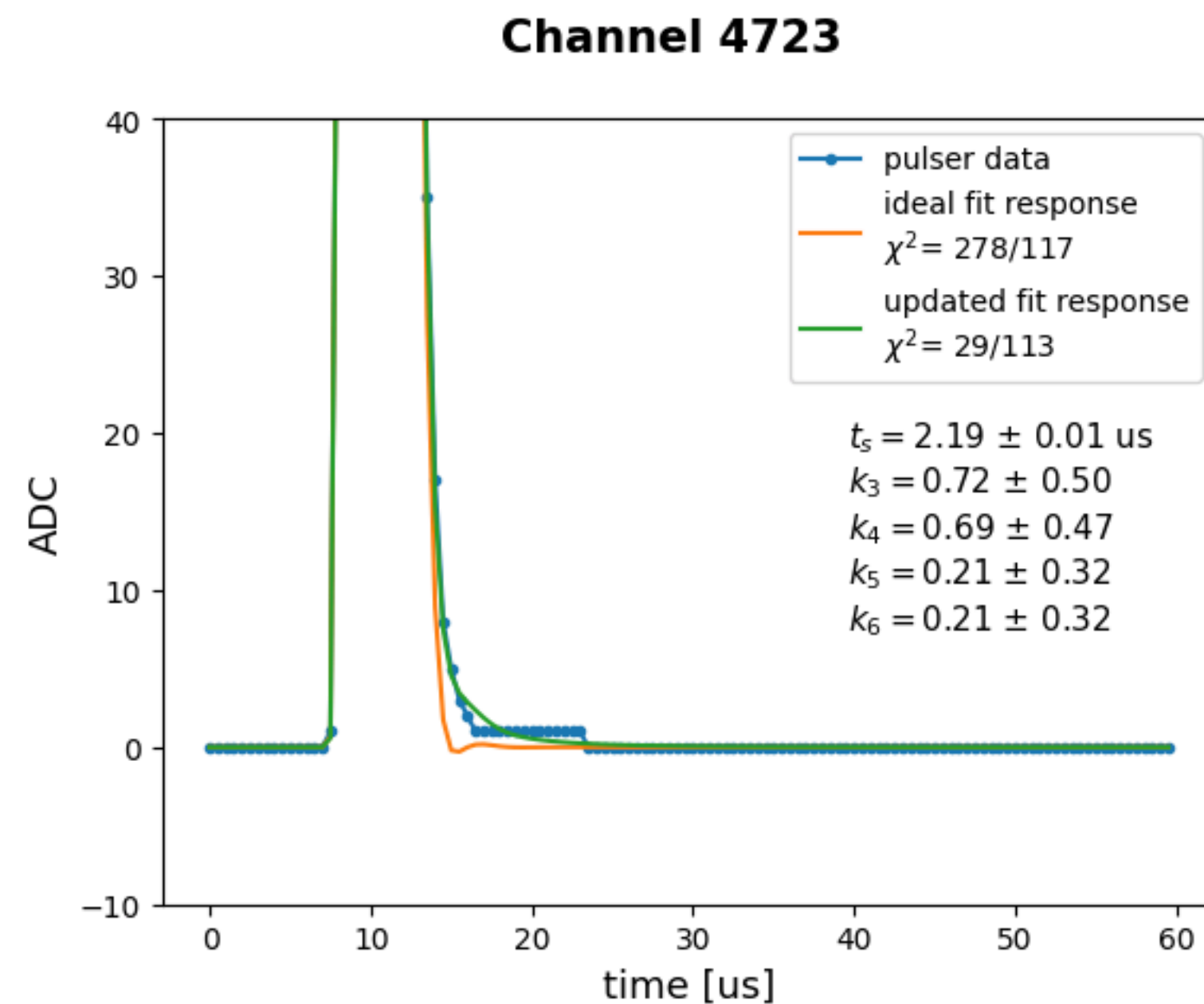
Updated Response Model

- will see features such as multiple over/undershoots, or features with very long time-scales
- imperfect pole-zero cancellation model doesn't model these well
- the errors in the fitted parameters do not necessarily reflect the goodness-of-fit



Updated Response Model

- still in the process of determining a metric and procedure for deciding when to use ideal response and when to use the updated model for each channel
- uncertainties in updated model fit do not always reflect goodness-of-fit



Updated Response Model: debugging

- when first attempting to use ParamsPerChannelResp correction with fitted pole values, the SP stage starts to output *empty frames*

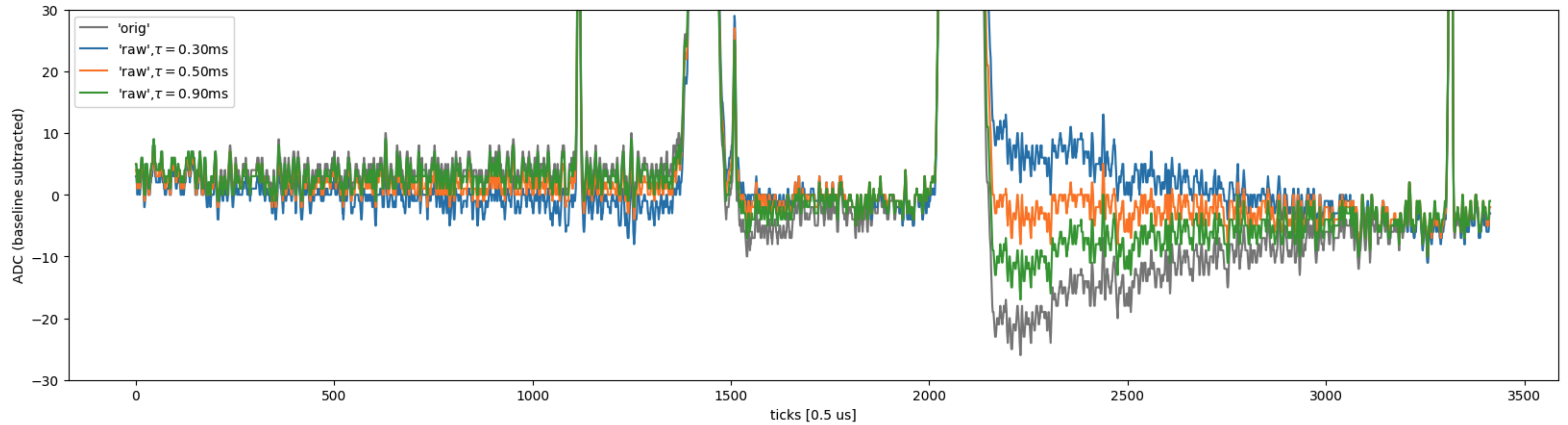
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[20:47:21.266] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 load plane index: 0, ntraces=5632, input bad regions: 1
[20:47:21.450] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 applying ch-by-ch electronics response correction
[20:47:24.892] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 load plane index: 1, ntraces=5632, input bad regions: 1
[20:47:25.047] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 applying ch-by-ch electronics response correction
[20:47:28.688] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 load plane index: 2, ntraces=5632, input bad regions: 0
[20:47:28.899] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 applying ch-by-ch electronics response correction
[20:47:30.343] D [sigproc ] <OmnibusSigProc:apa1sigproc1> 1664 empty rows out of size=(1664,3415)
[20:47:30.930] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 save plane index: 0, Qtot=56797706 Qloss=-6266144, 4613
indices spanning [0,4612] "wiener"
[20:47:31.315] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 save plane index: 0, Qtot=50996746 Qloss=-1695435, 2494
indices spanning [4613,7106] "gauss"
[20:47:31.775] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 save plane index: 1, Qtot=63567394 Qloss=-7627208, 3926
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indices spanning [11033,13142] "gauss"
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[20:47:32.728] D [sigproc ] <OmnibusSigProc:apa1sigproc1> call=0 gauss save plane index: 2 empty
```

- SP runs normally if all pole values are their default (using ideal response), where $k_3=k_4=0.1$, and $k_5=k_6=0.0$

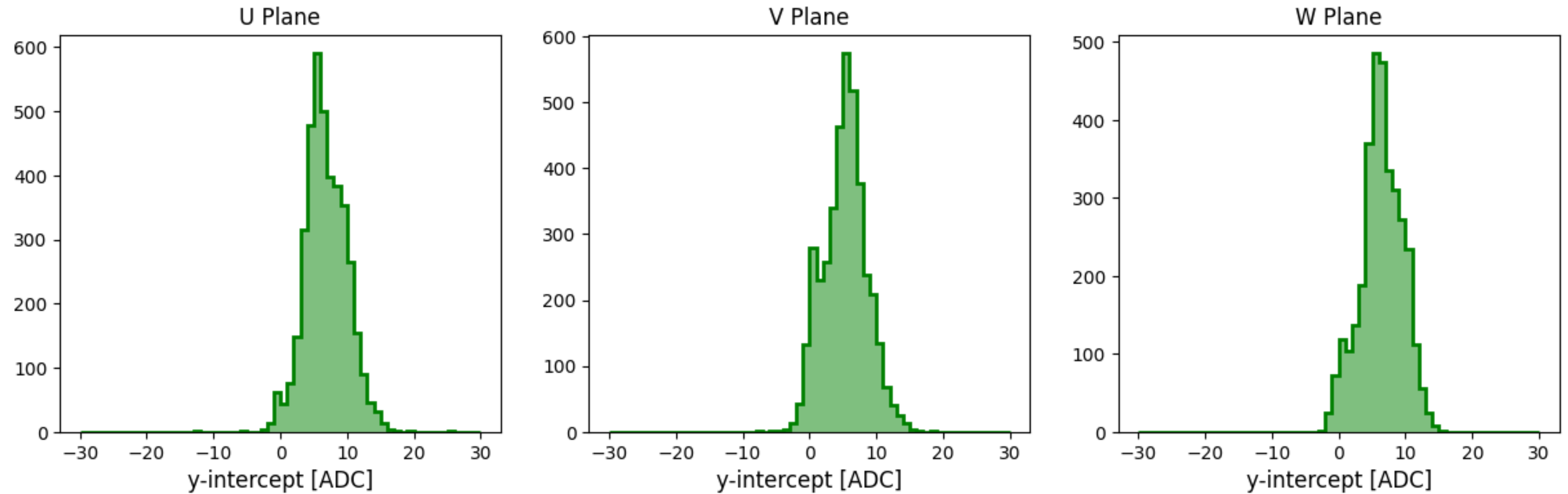
Summary

- First pass of the electronics response calibration has been performed using 100 kV pulser data!
 - work-in-progress: using an updated model to better characterize some very minor shape differences
- Very early validation shows improvement in the extracted charge agreement between the induction and collection panes

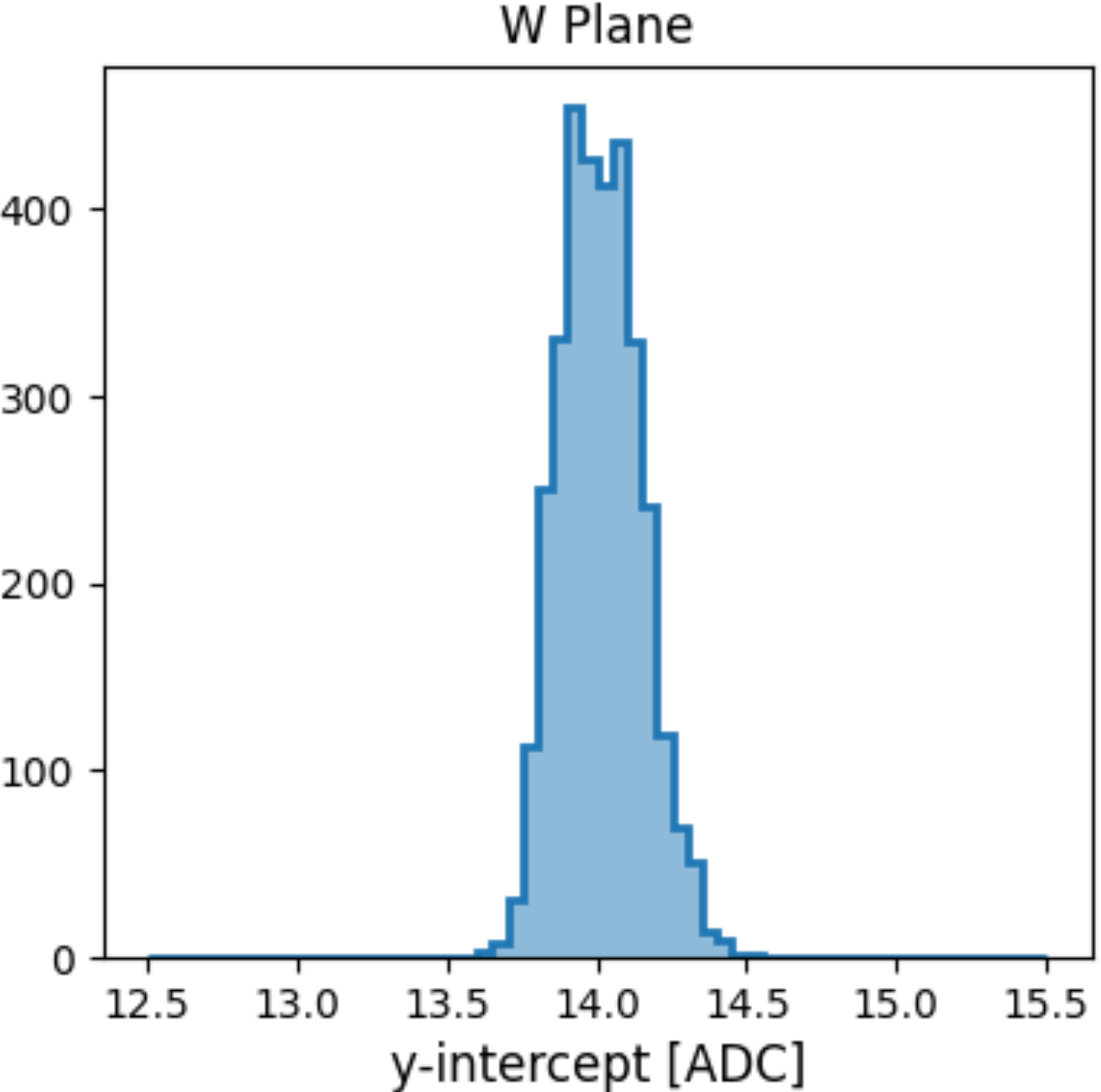
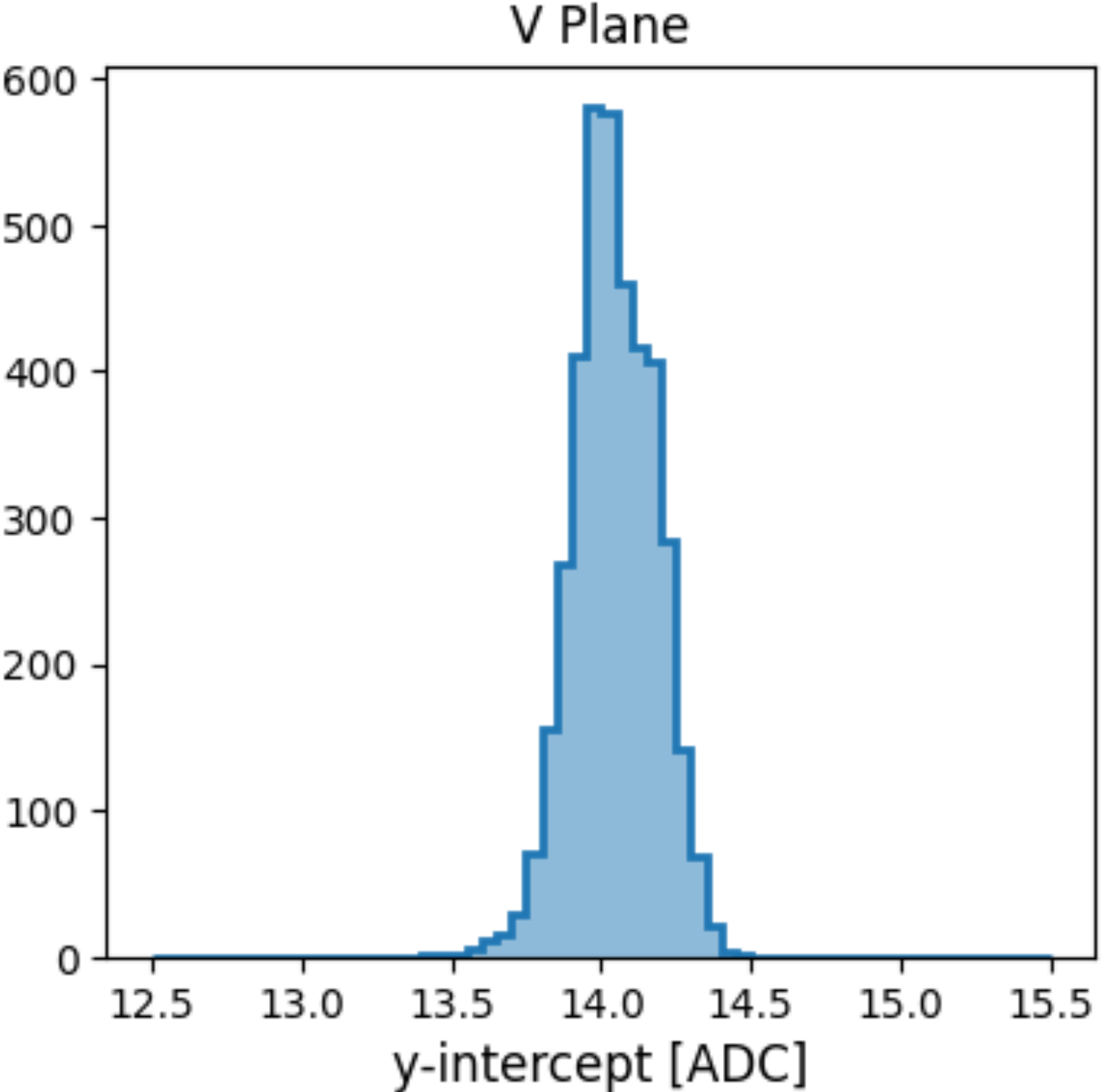
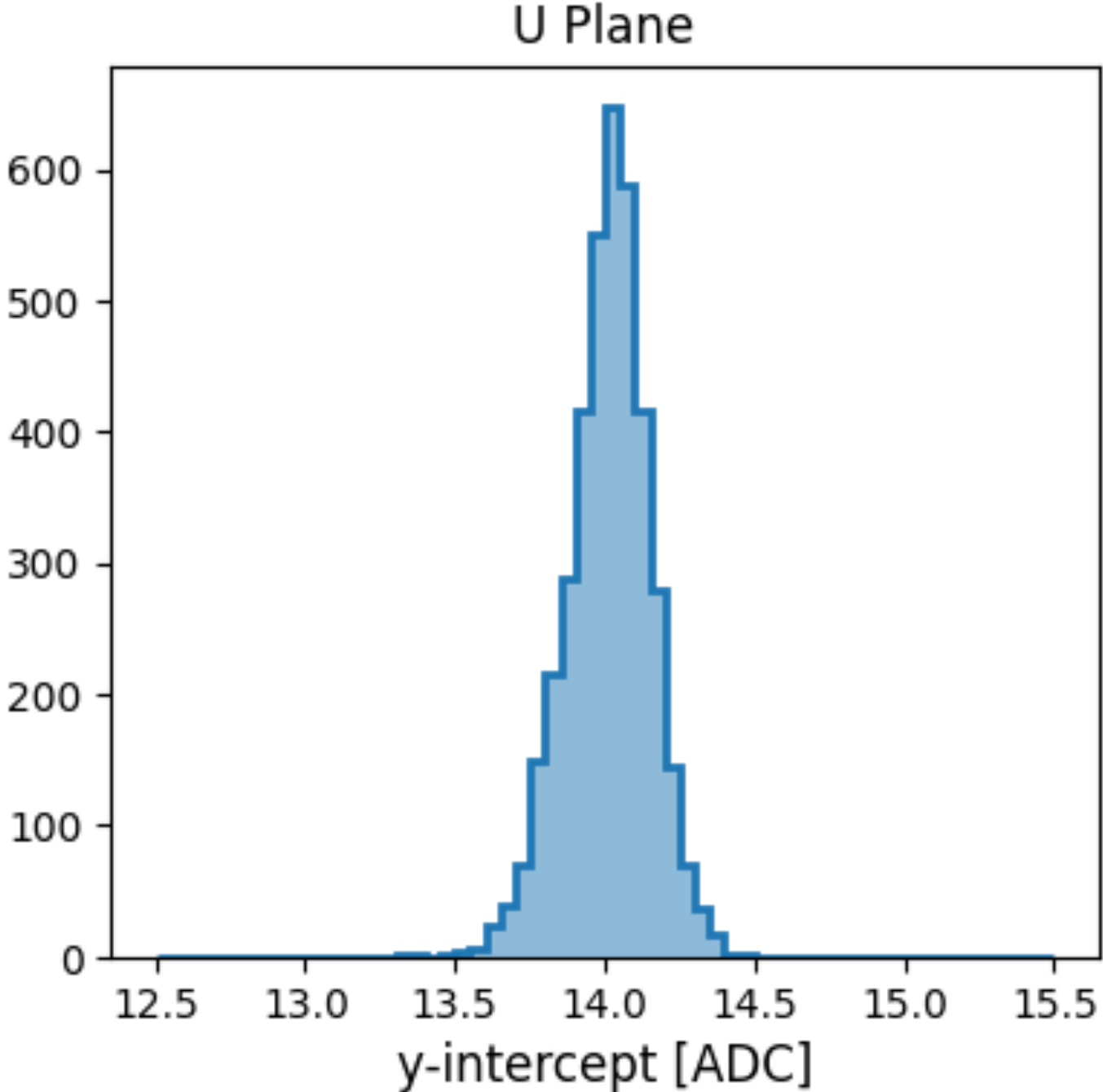
backup



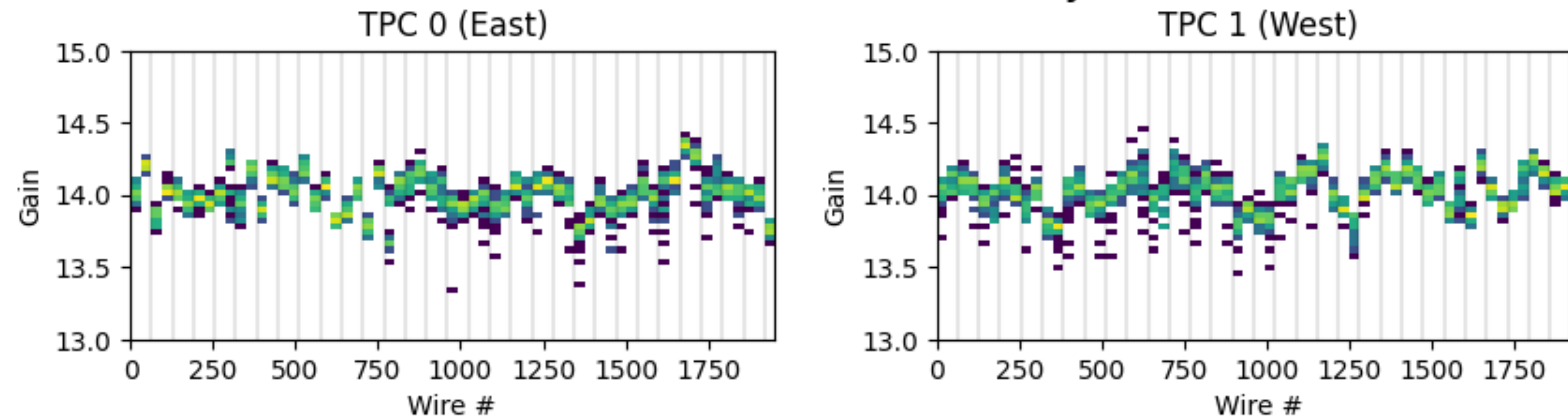
Distribution of Y-Intercept From Linear Fit (for Gain)



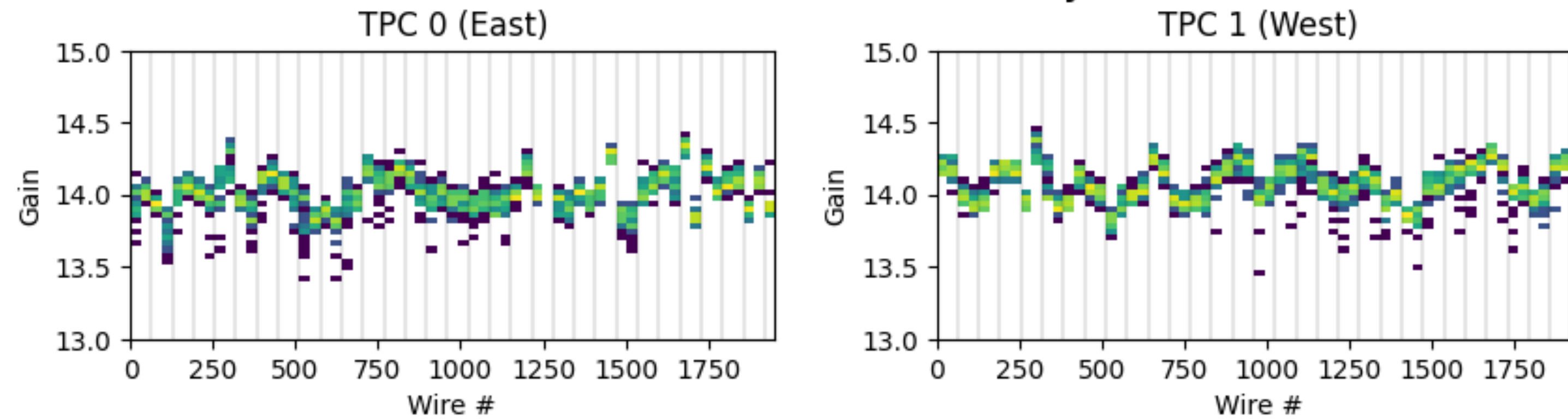
Distribution of Gains Per Plane



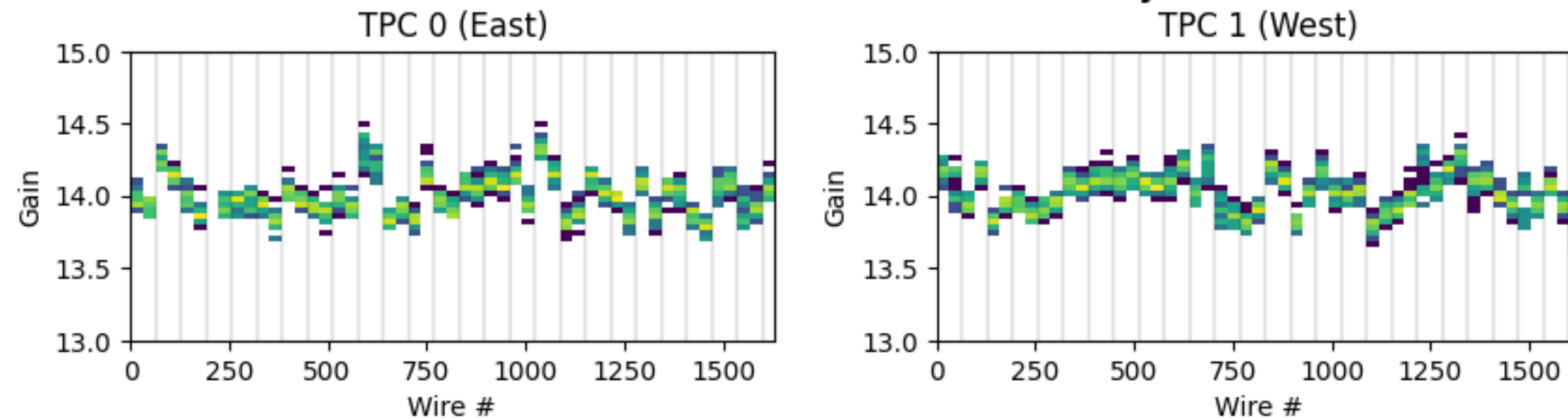
Wire # vs. Gain (U Plane Only)



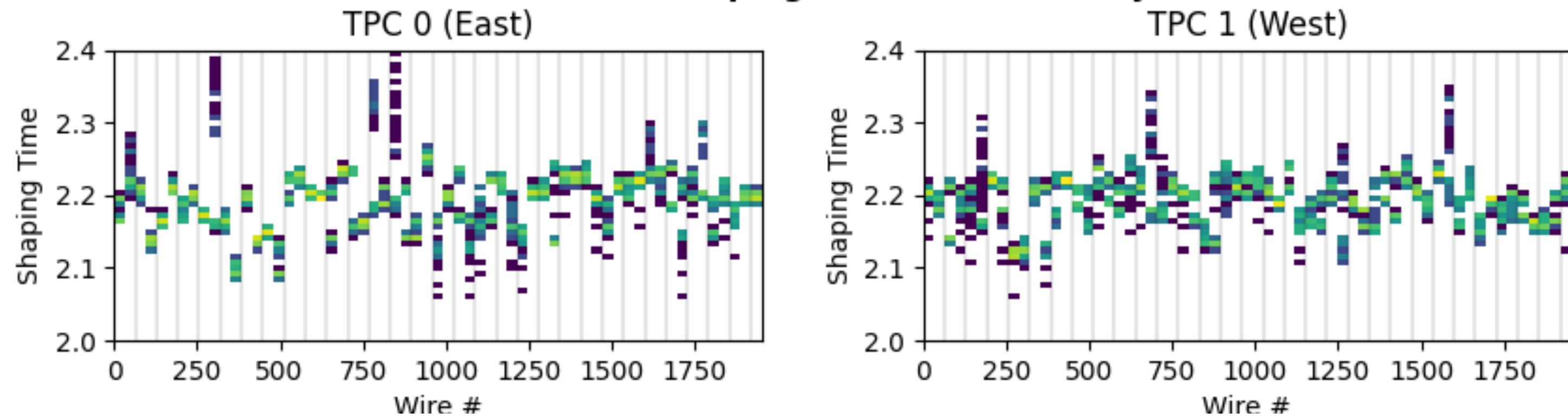
Wire # vs. Gain (V Plane Only)



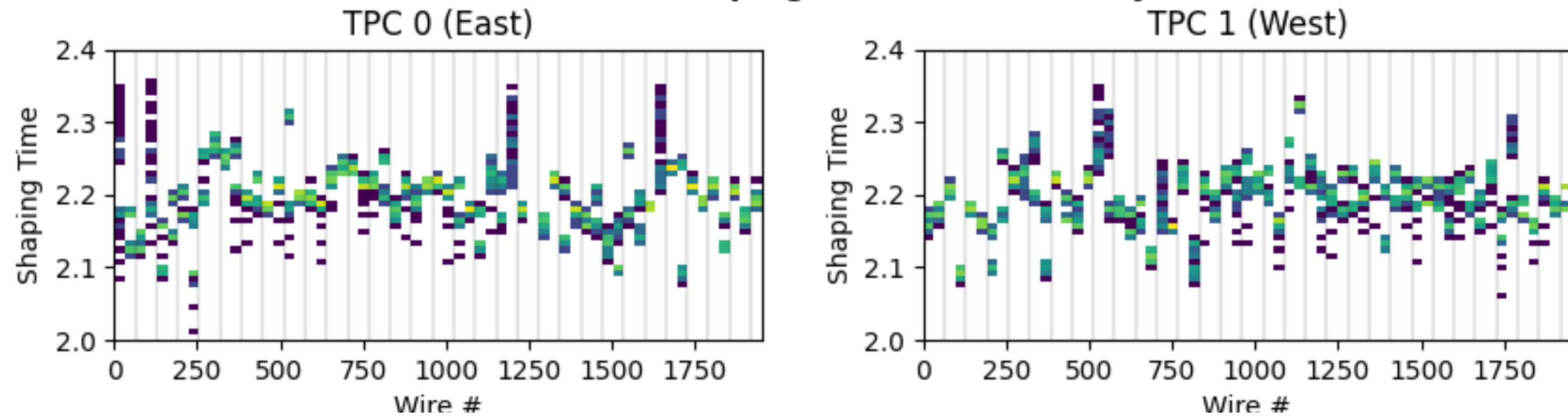
Wire # vs. Gain (Collection Plane Only)



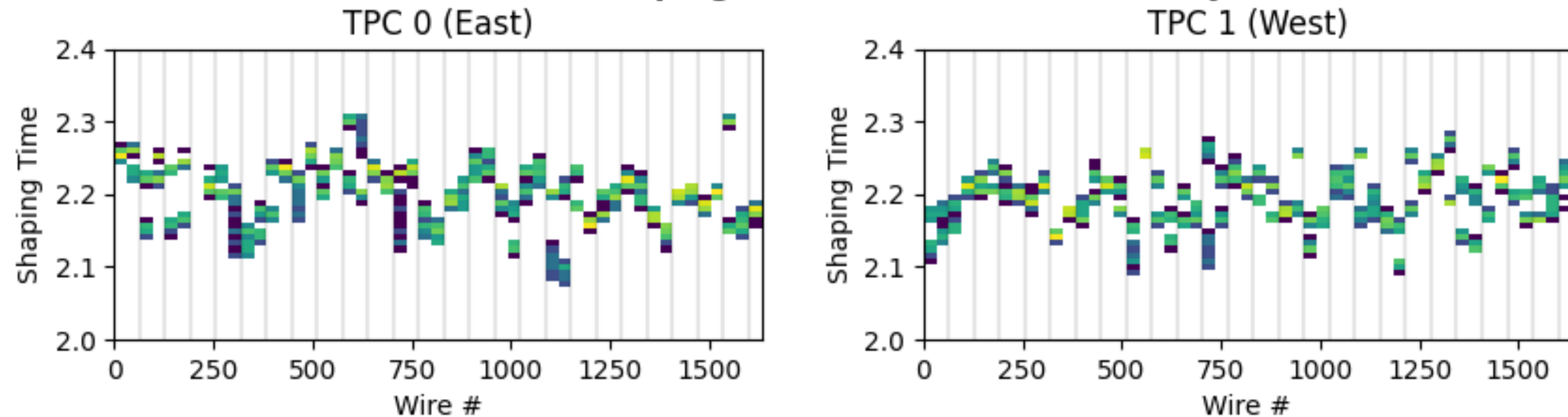
Wire # vs. Shaping Time (U Plane Only)



Wire # vs. Shaping Time (V Plane Only)



Wire # vs. Shaping Time (Collection Plane Only)



Inverse Laplace Transformation of $T(s)$

```
In[3]:= InverseLaplaceTransform[A / (p0 + s) / (pi1^2 + (pr1 + s)^2) / (pi2^2 + (pr2 + s)^2) * (k3 + s) / (k4 + s) * (k5 + s) / (k6 + s), s, t]
```

$$\text{Out[11]} = A \left(\frac{e^{-k_4 t} (-k_3 k_4 + k_4^2 + k_3 k_5 - k_4 k_5)}{(k_4 - k_6) (k_4 - p_0) (k_4^2 + p_{11}^2 - 2 k_4 p_1 + p_1^2) (k_4^2 + p_{12}^2 - 2 k_4 p_2 + p_2^2)} + \frac{e^{-k_6 t} (-k_3 k_5 + k_3 k_6 + k_5 k_6 - k_6^2)}{(k_4 - k_6) (k_6 - p_0) (k_6^2 + p_{11}^2 - 2 k_6 p_1 + p_1^2) (k_6^2 + p_{12}^2 - 2 k_6 p_2 + p_2^2)} + \right. \\ \left. \frac{e^{-p_0 t} (-k_3 k_5 + k_3 p_0 + k_5 p_0 - p_0^2)}{(k_4 - p_0) (-k_6 + p_0) (p_0^2 + p_{11}^2 - 2 p_0 p_1 + p_1^2) (p_0^2 + p_{12}^2 - 2 p_0 p_2 + p_2^2)} + (e^{-p_1 t} (p_{11} ((p_{11}^2 + p_1^2) (2 k_6 (p_{11}^2 + p_1^2) (p_1 - p_2) + k_6 p_0 (-p_{11}^2 + p_{12}^2 - p_1^2 + p_2^2) + (p_{11}^2 + p_1^2) (p_{11}^2 - p_{12}^2 + (p_1 - p_2) (2 p_0 - 3 p_1 + p_2)) + \right. \\ k_5 (2 p_{11}^2 (-2 p_1 + p_2) + p_0 (p_{11}^2 - p_{12}^2 - 3 p_1^2 + 4 p_1 p_2 - p_2^2) + 2 p_1 (p_{12}^2 + 2 p_1^2 - 3 p_1 p_2 + p_2^2) + k_6 (p_{11}^2 - p_{12}^2 + (p_1 - p_2) (2 p_0 - 3 p_1 + p_2))) + k_4 ((p_{11}^2 + p_1^2) (2 (p_{11}^2 + p_1^2) (p_1 - p_2) + p_0 (-p_{11}^2 + p_{12}^2 - p_1^2 + p_2^2)) + \\ k_5 (2 k_6 (p_{11}^2 + p_1^2) (p_1 - p_2) - k_6 p_0 (p_{11}^2 - p_{12}^2 + p_1^2 - p_2^2) + (p_{11}^2 + p_1^2) (p_{11}^2 - p_{12}^2 + (p_1 - p_2) (2 p_0 - 3 p_1 + p_2)) + k_6 (-p_{11}^4 + p_{11}^2 (p_{12}^2 - 2 p_1^2 + 2 p_0 p_2 + p_2^2) + p_1 (p_1 (p_{12}^2 - p_1^2 + p_2^2) - 2 p_0 (p_{12}^2 - p_1 p_2 + p_2^2)))) + \\ k_3 (- (p_{11}^2 + p_1^2) (4 p_{11}^2 p_1 - 2 p_{12}^2 p_1 - 4 p_1^3 - 2 p_{11}^2 p_2 + 6 p_1^2 p_2 - 2 p_1 p_1 p_2^2 + p_0 (-p_{11}^2 + p_{12}^2 + 3 p_1^2 - 4 p_1 p_2 + p_2^2) + k_6 (-p_{11}^2 + p_{12}^2 - (p_1 - p_2) (2 p_0 - 3 p_1 + p_2))) + k_5 (-p_{11}^4 + p_{11}^2 (p_{12}^2 - 4 p_0 p_1 + 10 p_1^2 + 2 p_0 p_2 - 8 p_1 p_2 + p_2^2) + \\ k_6 (2 p_{11}^2 (-2 p_1 + p_2) + p_0 (p_{11}^2 - p_{12}^2 - 3 p_1^2 + 4 p_1 p_2 - p_2^2) + 2 p_1 (p_{12}^2 + 2 p_1^2 - 3 p_1 p_2 + p_2^2)) + p_1 (2 p_0 (p_{12}^2 + 2 p_1^2 - 3 p_1 p_2 + p_2^2) - p_1 (3 p_{12}^2 + 5 p_1^2 - 8 p_1 p_2 + 3 p_2^2))) + k_4 (2 k_6 (p_{11}^2 + p_1^2) (p_1 - p_2) + \\ k_6 p_0 (-p_{11}^2 + p_{12}^2 - p_1^2 + p_2^2) + (p_{11}^2 + p_1^2) (p_{11}^2 - p_{12}^2 + (p_1 - p_2) (2 p_0 - 3 p_1 + p_2)) + k_5 (2 p_{11}^2 (-2 p_1 + p_2) + p_0 (p_{11}^2 - p_{12}^2 - 3 p_1^2 + 4 p_1 p_2 - p_2^2) + 2 p_1 (p_{12}^2 + 2 p_1^2 - 3 p_1 p_2 + p_2^2) + k_6 (p_{11}^2 - p_{12}^2 + (p_1 - p_2) (2 p_0 - 3 p_1 + p_2)))))) \\ \text{Cos}[p_{11} t] - ((p_{11}^2 + p_1^2) ((p_{11}^2 + p_1^2) (p_0 (p_{11}^2 - p_{12}^2 - (p_1 - p_2)^2) + p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (-3 p_1 + 2 p_2)) + k_6 (p_{11}^4 + (p_0 - p_1) p_1 (p_{12}^2 + (p_1 - p_2)^2) - p_{11}^2 (p_{12}^2 - p_0 p_1 + 2 p_0 p_2 - 2 p_1 p_2 + p_2^2)) + \\ k_5 (-p_{11}^4 + (p_0 - p_1) p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (p_{12}^2 - 3 p_0 p_1 + 6 p_1^2 + 2 p_0 p_2 - 6 p_1 p_2 + p_2^2) + k_6 (p_0 (p_{11}^2 - p_{12}^2 - (p_1 - p_2)^2) + p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (-3 p_1 + 2 p_2)))) + \\ k_4 ((p_{11}^2 + p_1^2) (p_{11}^4 + (p_0 - p_1) p_1 (p_{12}^2 + (p_1 - p_2)^2) - p_{11}^2 (p_{12}^2 - p_0 p_1 + 2 p_0 p_2 - 2 p_1 p_2 + p_2^2)) + k_5 ((p_{11}^2 + p_1^2) (p_0 (p_{11}^2 - p_{12}^2 - (p_1 - p_2)^2) + p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (-3 p_1 + 2 p_2)) + \\ k_6 (p_{11}^4 + (p_0 - p_1) p_1 (p_{12}^2 + (p_1 - p_2)^2) - p_{11}^2 (p_{12}^2 - p_0 p_1 + 2 p_0 p_2 - 2 p_1 p_2 + p_2^2))) + k_6 ((p_{11}^2 + p_1^2) (p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (p_1 - 2 p_2)) - p_0 (p_{11}^4 + p_{11}^2 (p_{12}^2 + (p_1 - p_2)^2) - p_{11}^2 (p_{12}^2 - 2 p_1^2 + 2 p_1 p_2 + p_2^2)))) + \\ k_3 ((p_{11}^2 + p_1^2) (-p_{11}^4 + (p_0 - p_1) p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (p_{12}^2 - 3 p_0 p_1 + 6 p_1^2 + 2 p_0 p_2 - 6 p_1 p_2 + p_2^2) + k_6 (p_0 (p_{11}^2 - p_{12}^2 - (p_1 - p_2)^2) + p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (-3 p_1 + 2 p_2))) + k_5 (5 p_{11}^4 p_1 - 3 p_{11}^2 p_{12}^2 p_1 - 10 p_{11}^2 p_1^3 + p_{12}^2 p_1^3 + \\ p_1^5 - 2 p_{11}^4 p_2 + 12 p_{11}^2 p_1^2 p_2 - 2 p_1^4 p_2 - 3 p_{11}^2 p_1 p_2^2 + p_1^3 p_2^2 - p_0 (p_{11}^4 + p_1^2 (p_{12}^2 + (p_1 - p_2)^2) - p_{11}^2 (p_{12}^2 + 6 p_1^2 - 6 p_1 p_2 + p_2^2)) + k_6 (-p_{11}^4 + (p_0 - p_1) p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (p_{12}^2 - 3 p_0 p_1 + 6 p_1^2 + 2 p_0 p_2 - 6 p_1 p_2 + p_2^2))) + \\ k_4 ((p_{11}^2 + p_1^2) (p_0 (p_{11}^2 - p_{12}^2 - (p_1 - p_2)^2) + p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (-3 p_1 + 2 p_2)) + k_6 (p_{11}^4 + (p_0 - p_1) p_1 (p_{12}^2 + (p_1 - p_2)^2) - p_{11}^2 (p_{12}^2 - p_0 p_1 + 2 p_0 p_2 - 2 p_1 p_2 + p_2^2)) + \\ k_5 (-p_{11}^4 + (p_0 - p_1) p_1 (p_{12}^2 + (p_1 - p_2)^2) - p_{11}^2 (p_{12}^2 - 3 p_0 p_1 + 6 p_1^2 + 2 p_0 p_2 - 6 p_1 p_2 + p_2^2) + k_6 (p_0 (p_{11}^2 - p_{12}^2 - (p_1 - p_2)^2) + p_1 (p_{12}^2 + (p_1 - p_2)^2) + p_{11}^2 (-3 p_1 + 2 p_2)))))) \text{Sin}[p_{11} t]) / \\ (p_{11} (k_4^2 + p_{11}^2 - 2 k_4 p_1 + p_1^2) (k_6^2 + p_{11}^2 - 2 k_6 p_1 + p_1^2) (p_0^2 + p_{11}^2 - 2 p_0 p_1 + p_1^2) (p_{11}^4 - 2 p_{11}^2 (p_{12}^2 - (p_1 - p_2)^2) + (p_{12}^2 + (p_1 - p_2)^2)^2)) + \\ (e^{-p_2 t} (-p_{12} (k_4 (- (p_{12}^2 + p_2^2) (p_0 (p_{11}^2 - p_{12}^2 + p_1^2 - p_2^2) - 2 (p_1 - p_2) (p_{12}^2 + p_2^2)) + k_5 ((p_{11}^2 - p_{12}^2 + (2 p_0 + p_1 - 3 p_2) (p_1 - p_2)) (p_{12}^2 + p_2^2) + 2 k_6 (p_1 - p_2) (p_{12}^2 + p_2^2) + k_6 p_0 (-p_{11}^2 + p_{12}^2 - p_1^2 + p_2^2)) + \\ k_6 (p_{12}^4 - p_{12}^2 (2 p_0 p_1 + p_1^2 - 2 p_2^2) - p_{11}^2 (p_{12}^2 + p_2 (-2 p_0 + p_2)) - (p_1 - p_2) p_2 (-2 p_0 p_1 + p_2 (p_1 + p_2))) + (p_{12}^2 + p_2^2) ((p_{11}^2 - p_{12}^2 + (2 p_0 + p_1 - 3 p_2) (p_1 - p_2)) (p_{12}^2 + p_2^2) + \\ 2 k_6 (p_1 - p_2) (p_{12}^2 + p_2^2) + k_6 p_0 (-p_{11}^2 + p_{12}^2 - p_1^2 + p_2^2) + k$$