INTT Ladder NIM Figures





Silicon pad region	
	Ę

	Regist	20	μm
	Copper plated	15	μm
L1	Electrolytic copper foil	9	μm
	Base Polyimide	50	μ m
L2	Electrolytic copper foil	9	μm
	Glue	25	μ m
	Base Polyimide	12.5	μm
	Glue	15	μm
L3	Electrolytic copper foil	9	μm
	Base Polyimide	50	μm
L4	Electrolytic copper foil	9	μm
	Glue	25	μm
	Base Polyimide	12.5	μm
	Glue	15	μm
L5	Electrolytic copper foil	9	μm
	Base Polyimide	50	μ m
L6	Electrolytic copper foil	9	μm
	Glue	25	μ m
	Base Polyimide	25	μ m
L7	Electrolytic copper foil	9	μm
	Copper plated	15	μm
	Regist	20	μ m
		438	μm

Total thickness 418 $\,\mu$ m

ο μπ









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INTT_Meeting_Minutes_200722.pdf
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Hi,

There was some typo and missing to do item in my last minutes. Thank you for Genki for point it out. Here is the updated one.

o Estimated effective thickness of the silver epoxy based on the volume of the glue mask provided from Rachid in the last meeting. The resulting effective thickness is 14um which is 28% of full thickness 50um. As a consequence, the contribution of the silver epoxy is now 0.04% instead of 0.14%. The total material budget was 1.12% before his update, and now 1.14%, very tiny increase. Although the carbon fiber stave thickness and silver epoxy glue are increased, these additional thickness were pretty much compensated by effective Cu thickness of HDI.

o Although the effective thickness based on the BNL mask is implemented to GEANT INTT model, NCU crews should also measure the amount of glue actually used in Taiwan assembly. The contribution of the silver epoxy in the material budget is not negligible if the effective thickness is near 50um, we should know realistic amount for the Taiwan ladders as well.

o GEANT model update is now complete and it is ready to report to the tracking group. Once it is approved by them, then Genki will commit the change as an official version. **Itaru will arrange the occasion with the tracking group.**

- Assembly in Taiwan < Cheng-Wei>

o Mounting wirebonded and encapsuled silicon module on to the stave is attempted. The pick up tool is tested this time. Will optimize the operation as the next step.

INTT_Cables_Performance.pptx



Eye Bran Specifications

• The receiver is designed for regular LVDS f.i. $4mA@100\Omega$. This translates to be $\Delta V =$

The receiver is not employing any commercial device, so no clear specification is defined.
However Tom considers △V= 100mV should work, but △V= 50mV is a bit uncomfortable level.



This figure is presented by Doug in FVTX review. The center diamond is not provided by Tom.

FPHX_dicussion_190930.pptx

410m/

V [U13.14 (at) V [U13.13 (at]

HDI Resistance

D14 $f_x = D13*26/1000$

Calculation from the cross section of the power layer

	A	В	С	D	E	F	G	I	Н	I	J	К	L	М		Ν
1	HDI Power Layer Dimension					雷气抵抗率(の比較(でんき	きていこ	5 h	つのひかく)では 雷気は	行家を比較	できろよう	昇順に表に	する	
2	Width [mm]	38	38	38		H XUOUT .							10007	Thereare	2 00	
3	Thickness [um]	9	9	9		長さ L [m]、断面積 A [m ²]の物体の電気抵抗 R [Ω]は、次式で求めることができる。										
4	Length [m]	0.2	0.2	0.2												
5	Area [m ²]	3.E-07	3.E-07	3.E-07		R = ho .	$\cdot L/A$									
6	Mesh facto r[%]	100	90	10		スのよう両方	= # # * * * * *									
7	Electric Resistivity (Cu) rho	1.68E-08	2.E-08	2.E-07		この方が电う	式担別辛での	ノ、甲位	LIG L	2111 (00 000						
8	Resistance R=rho*L/A [ohm]	0.010	0.011	0.098												
9											1	1				
10	FPHX Chip							因数 単	恤	值 (Ωm)	物質	温度特性	(毎ケルビン)			
11	Power consumption/Chip [mW]	65	65	65				0		0	超伝導					
12	Operation Voltage [V]	3	3	3												
13	Current Draw/Chip [mA]	21.67	21.67	21.67						1.59 × 10 ⁻⁸	銀	.0061				
14	Current Draw for 26 chips [A]	0.56	0.56	0.56						1.68×10^{-8}	銅	.0068				
15										2.21×10^{-8}	金					
16	Voltage Drop in Length B4 [V]	0.006	0.006	0.055						2.65×10^{-8}	アルミニウム	00429				
17										4.42 × 10-8	マガネシウム	100 120				
18	Voltage Drop in 40cm [V]	0.011	0.012	0.111						4.42 × 10 ⁻⁸		0045				
19								0 ⁻⁸ 10 n	Ωm	5.29 × 10 °	979277	.0045				
20										5.81 × 10 ⁻⁸	3/()/ト					
21															_	

Drawing Current for FPHX Chips

FPHX chip consumes about 1/3 power in analogue and 2/3 in digital sections, respectively.

	Total	Digital	Analogue
LVDS min.	0.54 A	0.36 A	0.18 A
LVDS max.	0.64 A	0.42 A	0.21 A

	Total	Partial	Conversion Cable		Bus Extender	HDI	
	Current [A]	Current [A]	20cm [Ω]	$40 \text{cm}[\Omega]$	Resistance $[\Omega]$	$40 \text{cm}[\Omega]$	
LVDS min.	0.54		0.2	0.4	0.3	0.1	
Digital		0.36	0.07	0.14	0.11	0.04	
Analogue		0.18	0.04	0.07	0.05	0.02	Anticipated Valtage
LVDS max.	0.64						Drop in each cables
Digital		0.42	0.08	0.17	0.13	0.04	·
Analogue		0.21	0.04	0.08	0.06	0.02	12

Radiation Hardness of the BEX



H. Imai Diploma Thesis

Origin of 5 kGy in sPHENIX

Kondo et al.: Development of Long and High-Density Flexible Printed Circuits (1/10)

[Technical Paper]

Development of Long and High-Density Flexible Printed Circuits

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(Received August 3, 2021; accepted July 7, 2022, published August 4, 2022)

Abstract

The super Pioneering High-Energy Nuclear Interaction eXperiment (sPHENIX), which aims to unravel the mysteries of the creation of the universe, is scheduled to be launched in 2023 at Brookhaven National Laboratory, U.S.A, using the relativistic heavy ion collider. As a typical high-energy particle accelerator-based experiment, the collision area of sPHENIX is to be tightly occupied with various radiation detectors, requiring a minimal special budget to run cables and transmit massive signals generated by these detectors to downstream electronics for data processing located in a remote distance. Accordingly, a long, high signal line-density cable has been developed based on the flexible printed circuit

more than the minimum required bit error rate of 50 ppm. 4.2 Mechanical characteristics

In sPHENIX, high reliability is required for the FPC because it is difficult to access the inside the radiation area during the experiment. This reliability was evaluated by the peeling and thermal-shock tests.

The objective of the peel test is to verify that the laminate substrate has sufficient peel strength between layers. We prepared a test sample of the same stackup as the prototype, but with no pattern in every layers, and then tested it by peeling it up and down at an angle of 180° in the second or third layer using a tensile tester. The test results are presented in Fig. 14. The peel strength is defined at the point of the observed tensile force where the stress samples demonstrated higher peel strength than the required 10 N/cm (a typical peel strength of conventional polyimide). This result is an improvement over the initial prototype test sample. This improvement was a biproduct of the new bonding sheet introduced in Section 3.3. The observed peel strength can be degraded after daily

The observed peer strength can be degraded after daily use in the radiation environment. Therefore, the peel strength was measured for the samples under radiation exposure by 5 kGy. In addition, 5 kGy is the expected radiation dose for five years of operation in sPHENIX. We did not observe obvious degradation in the peel strength within the accuracy of the measurement.

Because the cable comprises 4 layers of $12-\mu m$ thick



Fig. 13 Measurement result of eye-diagram



The origin of 5 kGy in sPHENIX needs to be double checked (Itaru)

Felix Clock Block Diagram



This is underdevelopment.

