

electronic response for PDVD

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electronic calibration data:

Run-VD	DAC	charge (fC)
41573	1	2.65
41574	2	5.30
41577	5	13.26
41582	10	26.51
41587	15	39.77
41593	21	55.67
41597	25	66.28
41602	30	79.53
41603	31	82.18

RUN-HD	DAC	charge_fC
30367	5	13.26
30376	10	26.51
30385	15	39.77
30394	20	53.02
30404	25	66.28
30413	30	79.53
30421	35	92.79
30430	40	106.04

$$1 \text{ mV} = \frac{2^{\text{resolution}}}{(\text{fullscale}_{hi} - \text{fullscale}_{lo})} = \frac{2^{14}}{(1.6 - 0.2) \text{ V} \times 1000 \frac{\text{mV}}{\text{V}}} = \frac{16384}{1400} = 11.703 \text{ ADC}$$

$$Q_{\text{fC}} (\text{fC}) = \text{pulse_dac} (\text{bit}) \times \frac{CC (\text{F}) \times \text{dac_du} (\text{mV/bit})}{1000 (\text{mV/V})} \times 10^{15} (\text{fC/C})$$

$$= \text{pulse_dac} (\text{bit}) \times \frac{1.85 \times 10^{-13} (\text{F}) \times 14.33 (\text{mV/bit})}{1000 (\text{mV/V})} \times 10^{15} (\text{fC/C}) = \text{pulse_dac} \times 2.65105 (\text{fC})$$

Electronic response

- Calibrate the ch-by-ch electronics response function with dedicated pulser data
- The **non-uniform electronics response** is then replaced by an **ideal response function** during signal processing

Imperfect Pole-Zero cancellation

- $T(s) = \frac{(s+k3)(s+k5)}{(s+k4)(s+k6)} \times \frac{A}{(s+p_0)(p_{1i}^2 + (p_{1r} + s)^2)(p_{2i}^2 + (p_{2r} + s)^2)}$
- In the case of $k3 = k4$ and $k5=k6$, transfer function recovers to the ideal function form
- $K3 \sim k4 \sim 10$ kHz
- $K5 \sim k6 \sim 30$ kHz
- Mismatch between $k3$ ($k5$) and $k4$ ($k6$) is essentially the **imperfect pole-zero cancellation**

Ideal Electronics Response

$$T(s) = \frac{A_0 \cdot C_A}{(p_0 + s) \cdot (p_{i1}^2 + (p_{r1} + s)^2) \cdot (p_{i2}^2 + (p_{r2} + s)^2)}, \quad (3.1)$$

with s being a complex frequency variable. The parameters in equation 3.1 are obtained from a detailed simulation of the network design and are determined to be:

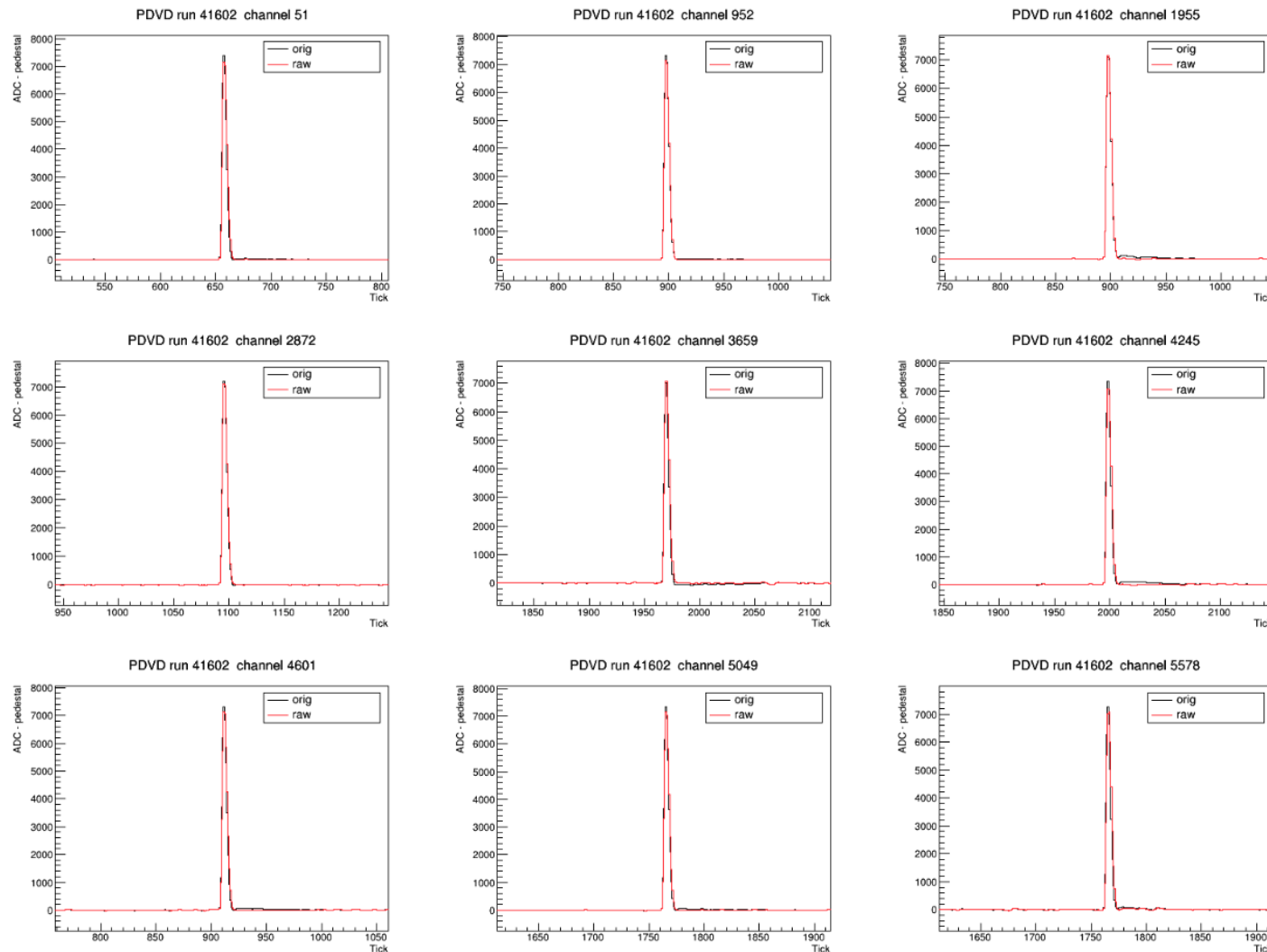
$$\begin{aligned} p_{r1} &= \frac{1.417}{t_p \cdot C_T}, & p_{r2} &= \frac{1.204}{t_p \cdot C_T}, \\ p_{i1} &= \frac{0.598}{t_p \cdot C_T}, & p_{i2} &= \frac{1.299}{t_p \cdot C_T}, \\ p_0 &= \frac{1.477}{t_p \cdot C_T}, & C_A &= \frac{2.7433}{(t_p \cdot C_T)^4}, \\ C_T &= \frac{1}{1.996}; \end{aligned} \quad (3.2)$$

where A_0 is the gain parameter and t_p is the peaking time constant. $T(s)$ has units of $\frac{V}{C} (\text{Hz})^{-1}$.

- placed at then end of one channel noise filter
- source code: perChannelShaper
 - <https://github.com/WireCell/wire-cell-toolkit/blob/master/sigproc/src/ResponseShaper.cxx>

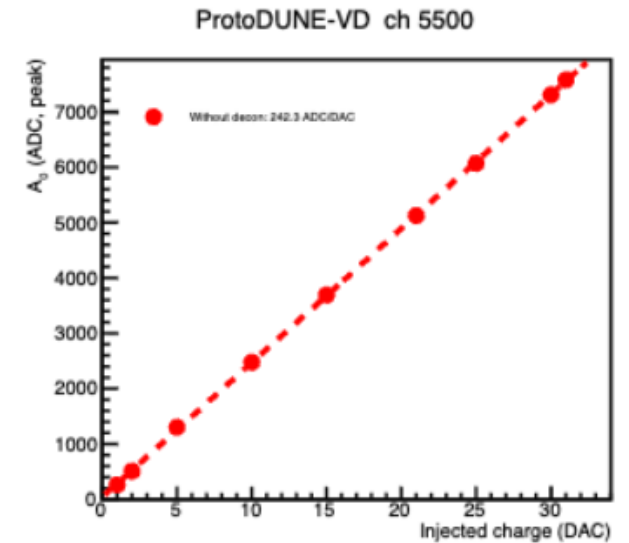
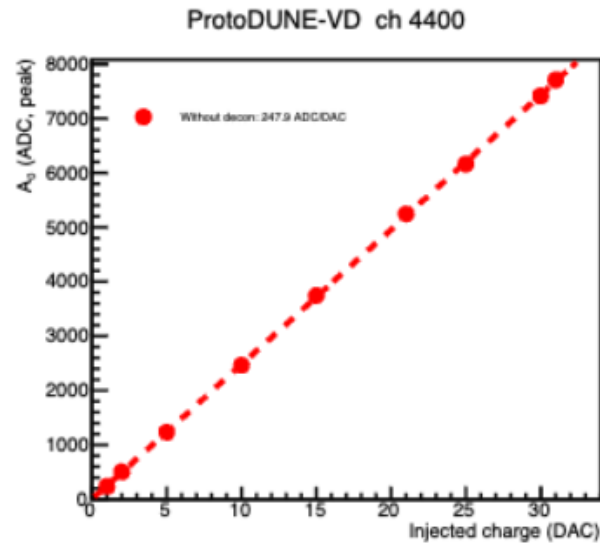
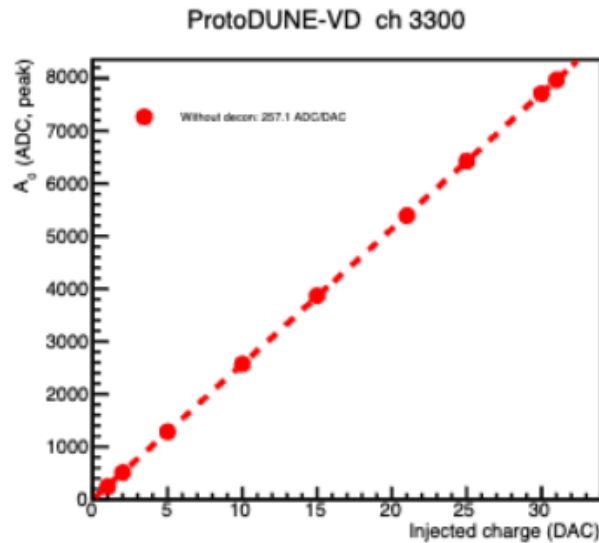
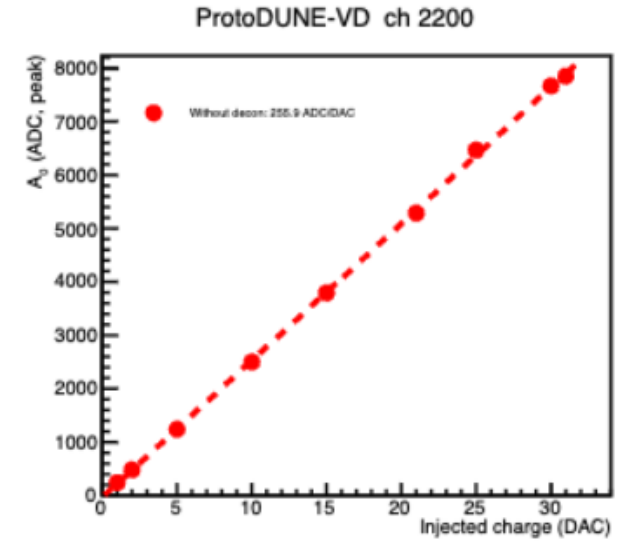
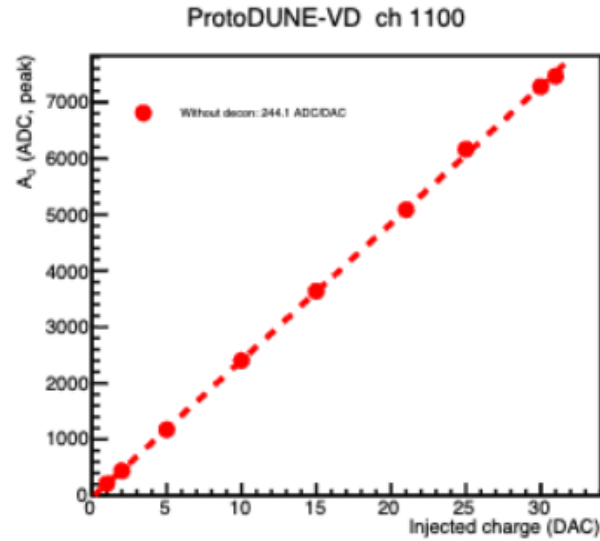
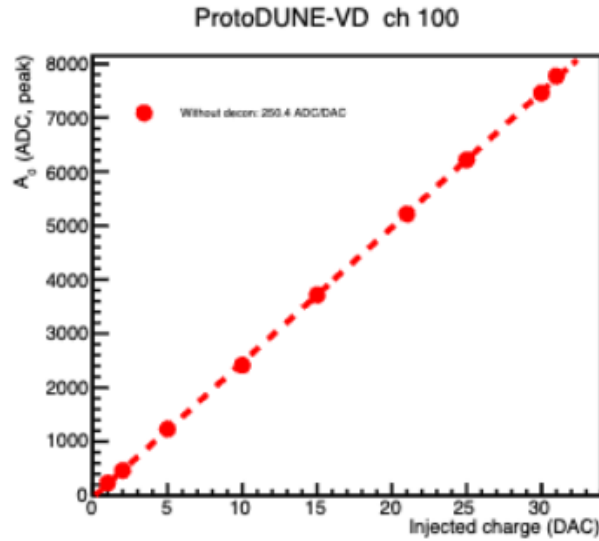
Response result check for PDVD

- Karla already has all the fitting result for all the calibration pulse
- With this fitted result, **for pulse calibration data**, I disable all the noise filter, only apply *perChannelShaper*

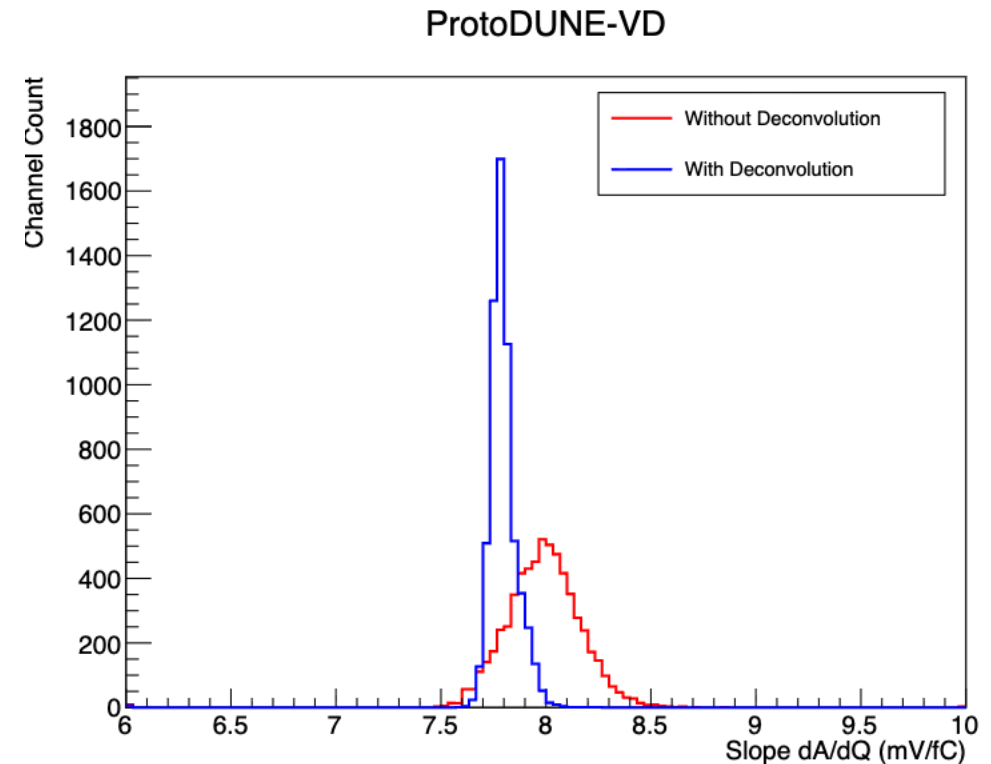
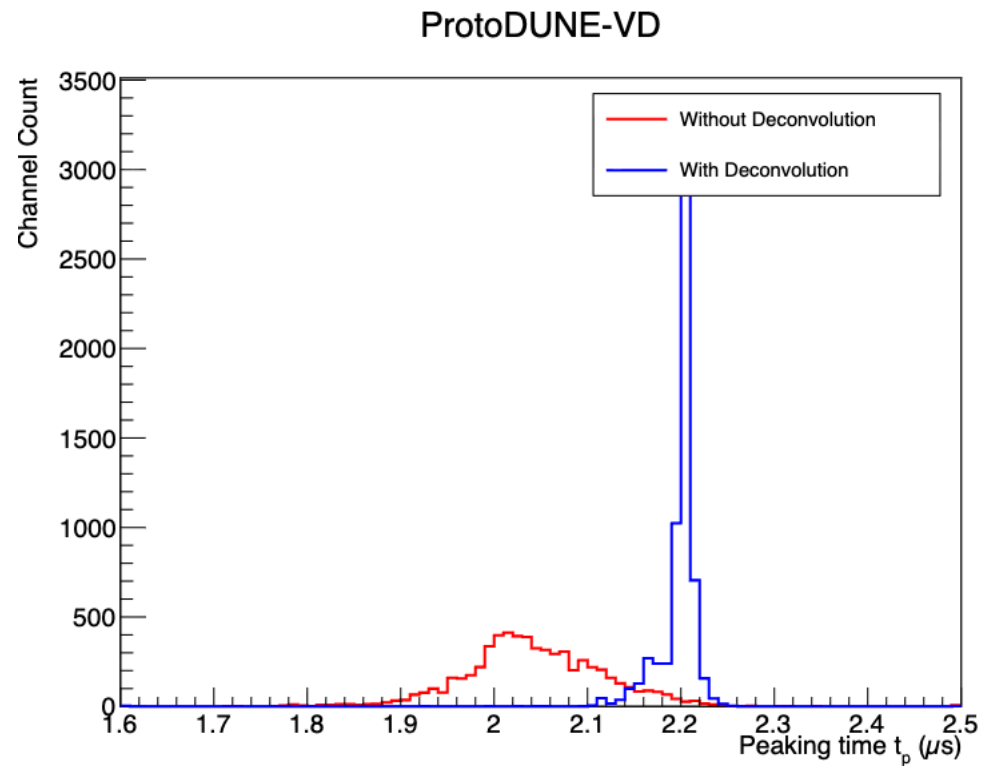


- orig is original data
- **raw** is after ideal response replaced.

Injected DAC vs A(ADC)



Fitted result for VD before and after response



- jsonnet files:
 - <https://github.com/DUNE/dunereco/commit/0b6d6ae6253c3606b4d65ba6766818423bd42b97>
- fcl:
 - /exp/dune/data/users/xning/proto-dune-vd/elec_res/run_nf_elec_calib_vd.fcl