### Naval Nuclear Laboratory Thermal Scattering Library Analyses

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#### Neptune Experiment Used for Validation of ENDF/B-VIII.0( $\beta$ 5) H-H<sub>2</sub>O TSL as a Function of Temperature

- Rolls-Royce conducted a series of critical experiments at the Neptune facility to validate the ability to predict criticality for water-isolated arrays as function of temperature [see Ref.].
- Configurations were neutronically similar to spent fuel storage racks without poison inserts in flux trap.
- Test was specifically designed to assess criticality safety issues for spent fuel rack configurations with water gaps.
- In this configuration, undermoderated fuel assemblies can have a positive temperature coefficient of reactivity.
- Water temperature varied from 20-60 °C

#### **Schematic of Core and Detector Arrangement**



FC = Fission Chamber SDA = ShutDown Amplifier Log = Log Channel PC = Pulse Channel WRL = Wide Range Linear RM = Reactivity Meter

Schematic of Fuel Arrangement Showing Increase in Effective Water Gap



Ref.: S. Walley et al., "Measurement of Positive Temperature Coefficients of Reactivity for Rack-like Arrangements of Reactor Fuel in the Neptune Zero Energy Facility," Proc. RRFM-2016, Berlin, March 13-17, 2016.



#### Neptune Configuration C Positive Bank Height vs. Temperature Displaying a Positive Temperature Coefficient of Reactivity



This Neptune experiment is specifically designed to be sensitive to thermal scattering in water as a function of temperature.

Various combinations of ENDF non-moderator libraries and H-H2O TSL libraries were used to determine if the positive temperature coefficient of reactivity was being accurately predicted.



# $\label{eq:MC21} MC21 \ Calculated \ k_{eff} \ for \ Neptune \ Configuration \ C \\ as a \ Function \ of \ Temperature \ Using \ ENDF/B-VII.1 \\ Non-Moderator \ Libraries \ and \ Various \ H-H_2O \ TSL \ Libraries \ Non-Moderator \ Non-Moderator \ Libraries \ Non-Moderator \ No-Moderator \ Non-Mode$





#### MC21 Calculated $k_{eff}$ for Neptune Configuration C as a Function of Temperature Using ENDF/B-VII.1 Non-Moderator Libraries and Various H-H<sub>2</sub>O TSL Libraries





#### MC21 Calculated $k_{eff}$ for Neptune Configuration C as a Function of Temperature Using ENDF/B-VII.1 Non-Moderator Libraries and Various H-H<sub>2</sub>O TSL Libraries



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#### MC21 Calculated $k_{eff}$ for Neptune Configuration C as a Function of Temperature Using ENDF/B-VIII.0( $\beta$ 4) Non-Moderator Libraries and Various H-H<sub>2</sub>O TSL Libraries



---- ENDF-VIII.0(ß4) w/ -VII.1 H-H2O



#### MC21 Calculated $k_{eff}$ for Neptune Configuration C as a Function of Temperature Using ENDF/B-VIII.0( $\beta$ 4) Non-Moderator Libraries and Various H-H<sub>2</sub>O TSL Libraries





#### MC21 Calculated $k_{eff}$ for Neptune Configuration C as a Function of Temperature Using ENDF/B-VIII.0( $\beta$ 4) Non-Moderator Libraries and Various H-H<sub>2</sub>O TSL Libraries



----- ENDF-VIII.0(64) w/ -VII.1 H-H2O ----- ENDF-VIII.0(64) ----- ENDF-VIII.0(64) w/ -VIII.0(65) H-H2O



#### KRITZ Reactor Experiment Benchmark Description

- The KRITZ reactor was operated in Studsvik, Sweden, in the 1970s.
- IRPhEP experiment benchmarks KRITZ-LWR-RESR-002 (2:1) and -003 (2:13) are designed to attain criticality in a rectangular 40x40 array of 3.65m LEU UO<sub>2</sub> fuel rods in pressurized light water by regulating water level and boration.
- KRITZ-002 has 14.85mm lattice pitch. KRITZ-003 has 16.35mm lattice pitch.
- KRITZ-002 was performed at 292.9K (67.5°F) and 521.7K (479.3°F).
  KRITZ-003 was performed at 295.3K (71.8°F) and 516.2K (469.4°F).
- KRITZ is one of very few public (unclassified and non-proprietary) benchmarks available for nuclear data library validation at elevated temperatures.



#### KRITZ-002 Reactor Experiment Configuration (KRITZ-003 Differs by Pitch, Water Level, and Boration)















































![](_page_23_Picture_2.jpeg)

#### ENDF-VII.1 Graphite Total Thermal Cross Sections Calculated from File 7 with NDEX 8 at 296K, 500K, 700K, and 1000K

![](_page_24_Figure_1.jpeg)

![](_page_24_Picture_2.jpeg)

#### ENDF-VIII.0(β5) Crystalline Graphite (w/ Cubic Approximation Elastic) Total Thermal Cross Sections Calculated from File 7 with NDEX 8 at 296K, 500K, 700K, and 1000K

![](_page_25_Figure_1.jpeg)

![](_page_25_Picture_2.jpeg)

#### ENDF-VIII.0(β5) 10% Porous Graphite (w/ DW-Matrix Elastic) Total Thermal Cross Sections Calculated from File 7 with NDEX 8 at 296K, 500K, 700K, and 1000K

![](_page_26_Figure_1.jpeg)

![](_page_26_Picture_2.jpeg)

#### ENDF-VIII.0(β5) 30% Porous Graphite (w/ Cubic Approximation Elastic) Total Thermal Cross Sections Calculated from File 7 with NDEX 8 at 296K, 500K, 700K, and 1000K

![](_page_27_Figure_1.jpeg)

![](_page_27_Picture_2.jpeg)

## ENDF-VIII.0( $\beta$ 5) vs. -( $\beta$ 4) H-H<sub>2</sub>O Phonon Spectrum Adjustments in LEAPR Input Deck

![](_page_28_Figure_1.jpeg)

#### ENDF-VIII.0( $\beta$ 5) vs. -( $\beta$ 4) H-H<sub>2</sub>O Phonon Spectrum Adjustments in LEAPR Input Deck

ENDF-VIII.0(\$5) Phonon DOS / \$4 Phonon DOS

![](_page_29_Figure_2.jpeg)

![](_page_29_Picture_3.jpeg)

#### H-H<sub>2</sub>O ENDF-VIII.0(β5) vs. -(β4) Temperature-Dependence of Intermediate-Energy Thermal Scattering Cross Section Ratios to 293.6 K Cross Sections

![](_page_30_Figure_1.jpeg)

![](_page_30_Picture_2.jpeg)