

# Production Status

RIKEN/RBRC

Itaru Nakagawa

# COVID-19 Status

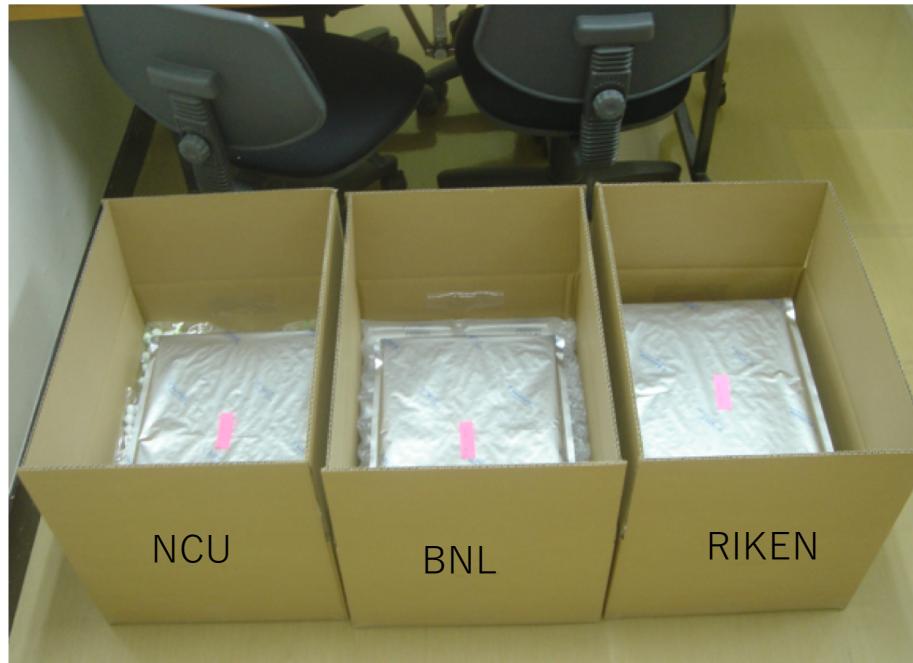
- NY State announced to be on pause until May 15<sup>th</sup>. BNL is closed until end of April, but may be extended accordingly.
  - Only work **approved as essential** can be done.
- RIKEN has been closed since April 8<sup>th</sup> until May 6<sup>th</sup> (likely to be extended)
  - Still can receive delivered items (HDI, Staves, …)
  - New contract will be pended until reopens
  - **Work which can cause trouble to other institute** may be approved as an essential business. (This logic is applied NCU shippings)
- NWU is closed as well. Takashi lost his access to the lab.
- NCU is still running.

# Executive Summary

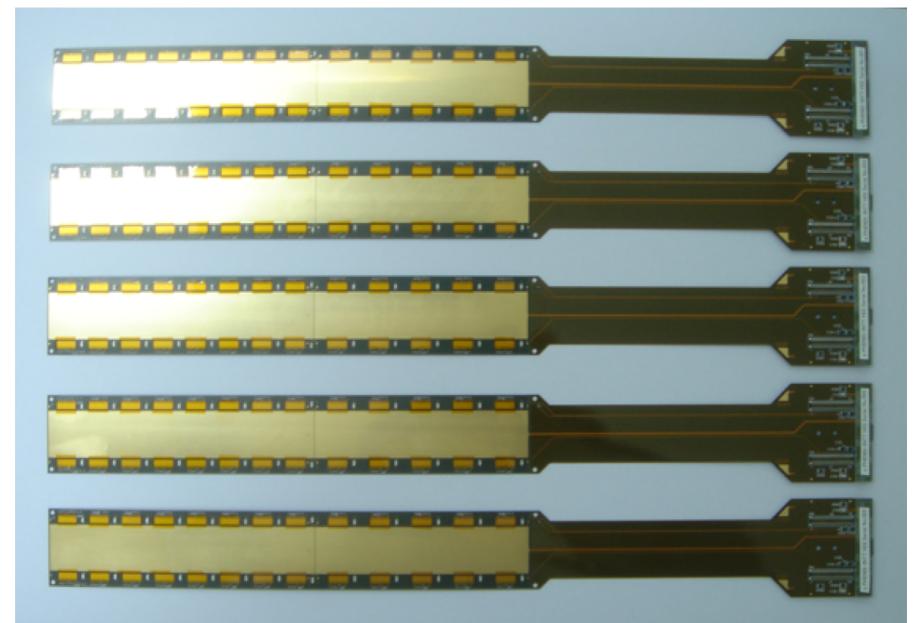
- **Silicon Sensors**
  - 29 Sensors are delivered to NCU in April 17<sup>th</sup>.
- **HDI**
  - Delivered to RIKEN on April 17<sup>th</sup>.
    - 19 HDI's arranged to be shipped to NCU on April 24<sup>th</sup>.
    - 39 HDI's for BNL are on hold at RIKEN.
  - 2<sup>nd</sup> Batch (90 more HDI's) is on hold for PO until RIKEN reopens and we confirm the modification around the bias connector. However the company pre-orders rolled copper foils (see my presentation 2020/03/16) in advance to save a few months for the fabrication.
- **Stave**
  - Issues of the delivered 8 staves are mostly overcame.
  - Updated report from ASUKA co. about the leak test.
- **FPHX**
  - Arranging 1,5k good FPHX chips are on their way to Taiwan.
- **Thin Trigger Scintillators**
  - Got quote from G-Tech co. for 9mm and 230mm thin scintillators. We have to wait for PO until RIKEN reopens.

We have been managed to supply components to NCU to keep them running. At least , we would like to keep this at least as a bottom line.

# HDI Delivery on April 17<sup>th</sup>



NCU box is to be picked up on April 24<sup>th</sup>.



# FPHX Chips

# 2016+2018 FPHX Production Statistics

| Batch                    | # | Wafer ID     | Good        | Bad          | Total       |                          |  |
|--------------------------|---|--------------|-------------|--------------|-------------|--------------------------|--|
| 2016                     | 1 | 19G4         | 729         | 108          | 837         | 2020/4/17 shipped to NCU |  |
|                          | 2 | 18H1         | 805         | 27           | 832         | 2020/4/17 shipped to NCU |  |
|                          | 3 | 24E5         | 738         | 95           | 833         |                          |  |
|                          | 4 | 23F2         | 798         | 30           | 828         |                          |  |
|                          | 5 | 21G4         | 792         | 47           | 839         |                          |  |
|                          | 6 | 20H1         | 814         | 22           | 836         |                          |  |
|                          | 7 | 22F7         | 705         | 119          | 824         |                          |  |
|                          |   | <b>Total</b> | <b>5381</b> | <b>448</b>   | <b>5829</b> |                          |  |
| 2018                     | 1 | W6B752-01D0  | 831         | 9            | 840         |                          |  |
|                          | 2 | W68752-02C3  | 837         | 3            | 840         |                          |  |
|                          | 3 | W6B752-03B6  | 836         | 4            | 840         |                          |  |
|                          | 4 | W6B752-04B1  | 833         | 7            | 840         |                          |  |
|                          | 5 | W6B72-05A4   | 834         | 6            | 840         |                          |  |
|                          | 6 | W6B752-06H2  | 830         | 10           | 840         |                          |  |
|                          | 7 | W6B752-07G5  | 831         | 9            | 840         |                          |  |
|                          | 8 | W6B752-08G0  | 834         | 6            | 840         |                          |  |
|                          | 9 | W6B7562-09F3 | 838         | 2            | 840         |                          |  |
|                          |   | <b>Total</b> | <b>7504</b> | <b>56</b>    | <b>7560</b> |                          |  |
| <b>2018+2019 TOTAL</b>   |   | <b>12885</b> | <b>504</b>  | <b>13389</b> |             |                          |  |
| Quantity for 120 Ladders |   | 6240         |             |              |             |                          |  |
| Number of spares         |   | 6645         |             |              |             |                          |  |

Total : 1,669 FPHX  
 Good : 1,534 Chips  
 Bad : 135 Chips

We have 12k FPHX chips  
 About half (6k) are used for 120 Ladders  
 Remaining half (6k) are sufficient for spares

Itaru Nakagawa

# Package



Contains 2 bags of FPHX  
Dropped off on to the shipping  
yard yesterday on April 20<sup>th</sup>.

Special Thanks to Mike Lenz for packing FPHX bags and the shipping arrangement.

# Bags of FPHX Chips

Bag contains multiple FPHX cases

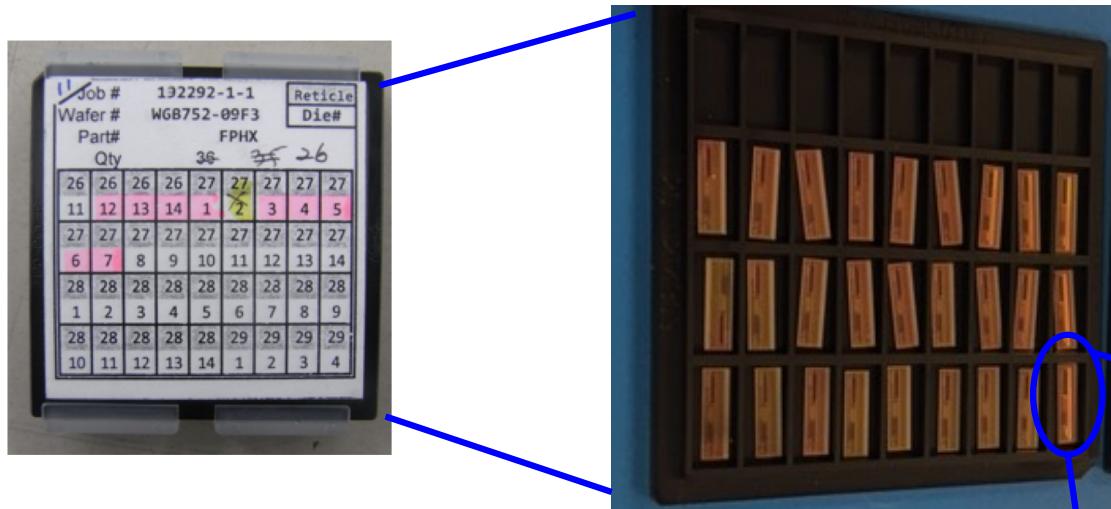


## FPHX case

|         |             |          |
|---------|-------------|----------|
| Job #   | 132292-1-1  | Reticule |
| Wafer # | WGB752-09F3 | Die#     |
| Part#   | FPHX        |          |
| Qty     | 36          | 35 26    |
| 26      | 26          | 26       |
| 11      | 12          | 13       |
| 27      | 27          | 27       |
| 6       | 7           | 8        |
| 28      | 28          | 28       |
| 1       | 2           | 3        |
| 28      | 28          | 28       |
| 10      | 11          | 12       |

Wafer ID  
**19G4**  
**18H1**  
24E5  
23F2  
21G4  
20H1  
22F7

Please find the bags for wafer #**19G4** and **18H1** from the stack of bags in the desiccator and pack them in a box with cushioning materials

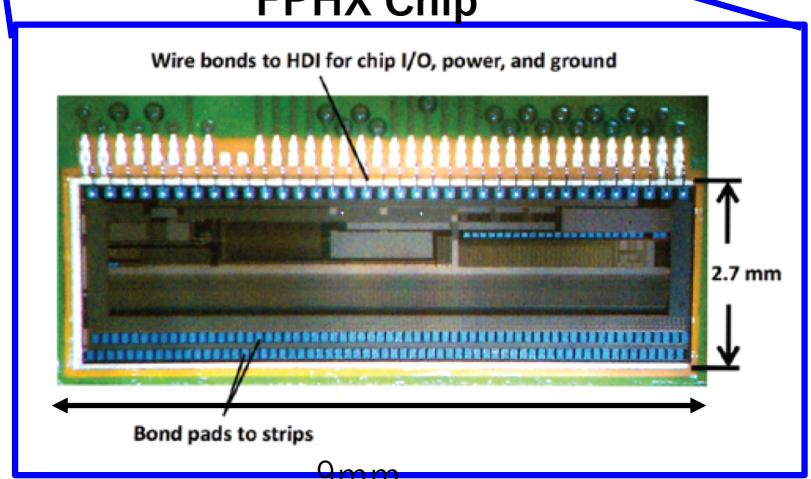


- ECCN : EAR99
- Make : MOSIS Service  
<https://www.mosis.com>
- Year : 2010 (Wafer)
- Specification is summarized in other document : FPHXspecSept08review08-14-08.pdf

**FPHX Chip**

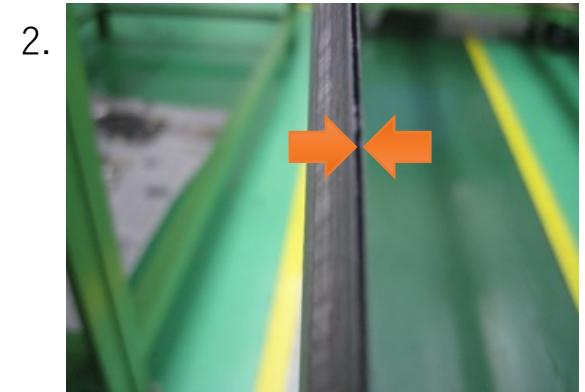
Instruction to use:

- Attention on the note pasted on the top of the case. This note represents result of the FPHX chip test after dicing for corresponding chips in the case.
- Highlighted or crossed IDs are identified as bad. Avoid them from the assembly.



# Stave

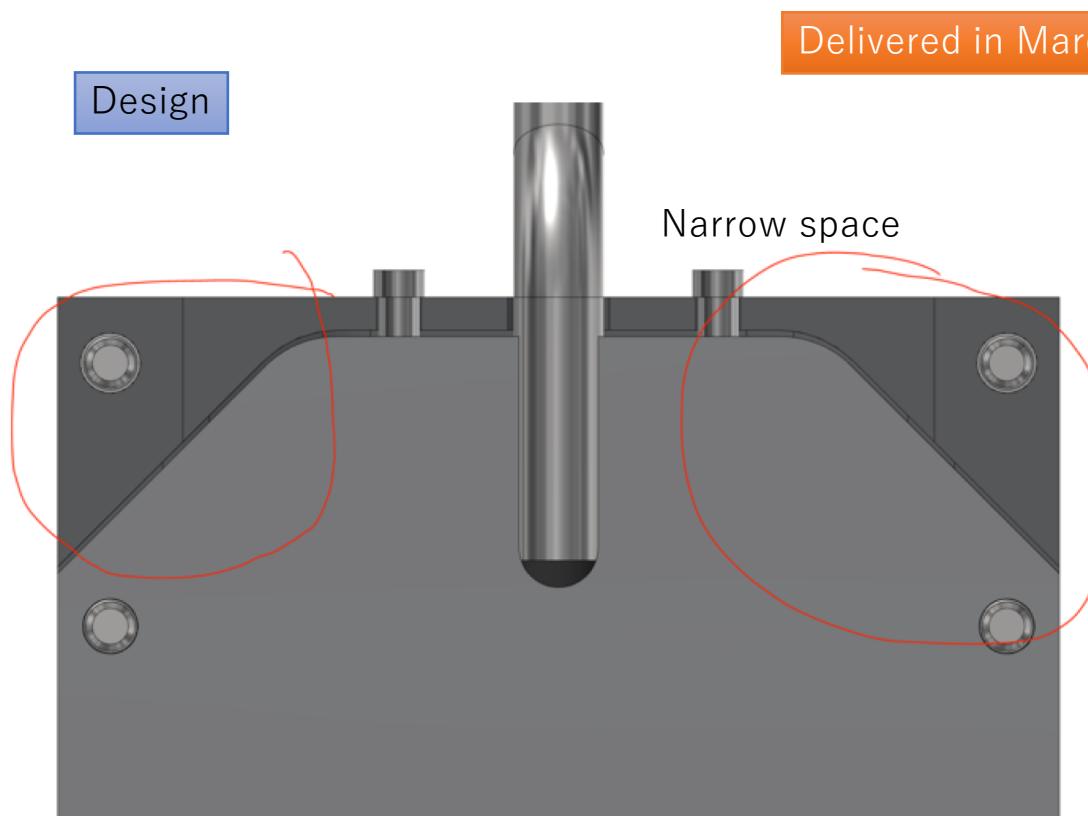
1. Extra space between CFRP plates and end cap
2. Space between the top and bottom CFRP plates.
3. Leak performance



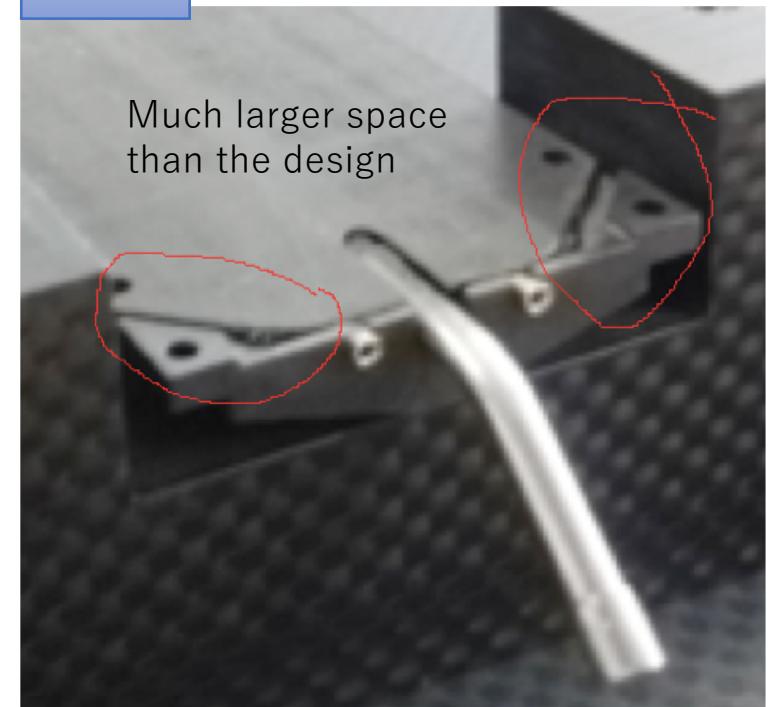
# Stave Schedule

- 12 Staves to be delivered by the end of April is on schedule.
  - 4 staves are to be shipped to NCU
  - 8 staves for BNL are to be on hold in RIKEN(?)
- Note these staves are **pre-production**, not production yet. Thus the ladders assembled on these staves considered as pre-production ladders (can be used for the assembly practice), but good to evaluate the performances.
- The design can be modified later depending on the performance of this version.
- Do we need an additional leak test in NCU before the assembly? Depends on the purpose of the ladder use. Do we need the leak test if the ladder is meant to be used for a future beam test?

# Space between End cap and CFRP

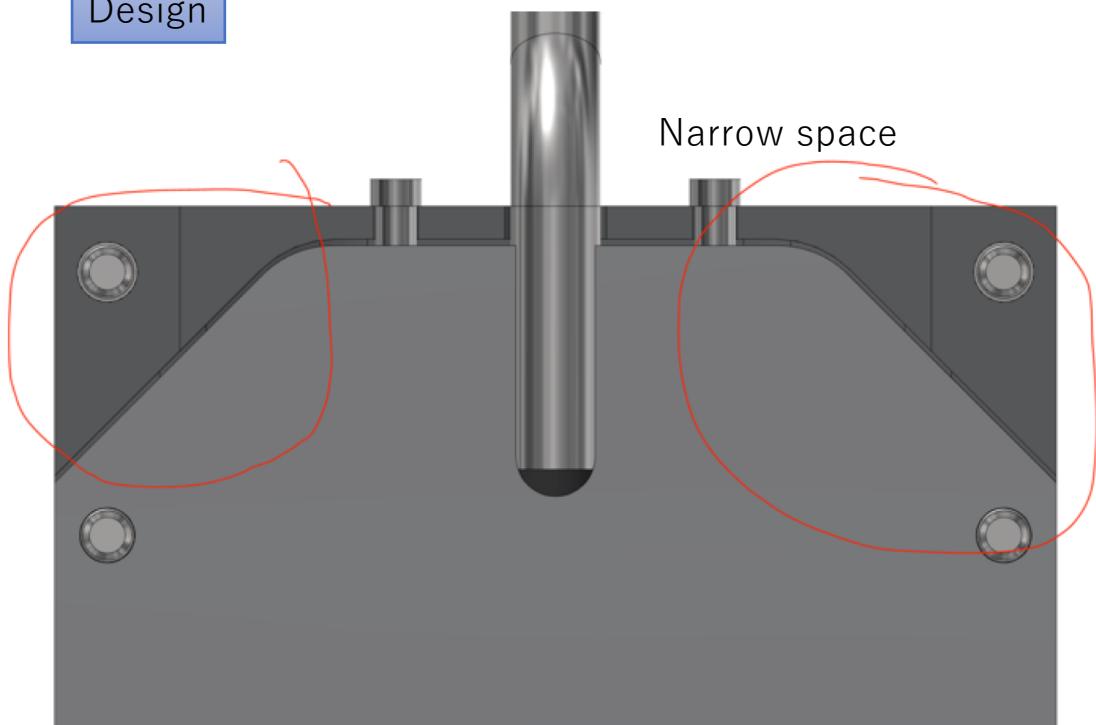


Product



# Space between End cap and CFRP

Design



Ongoing assembly today

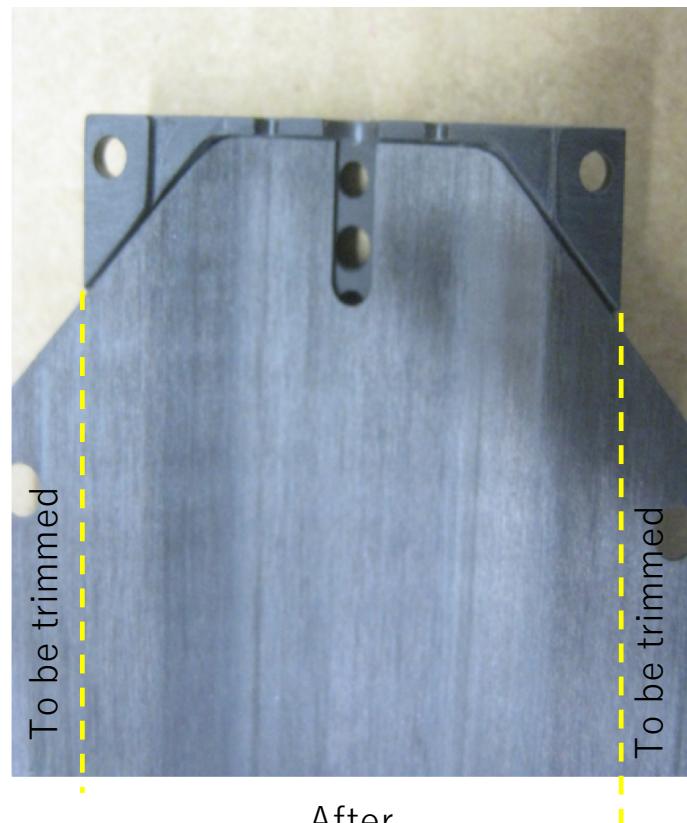
Product



# Before & After Comparison



before



After

# Cooling tube leak test update

Report from ASUKA Co. on April 16th

# Vacuum Leak Test Using a Pressure Gage

$$Q = \frac{V\Delta P}{\Delta t}$$

Report from March 18th

where

$Q$  : Leak quantity [ $Pa \cdot l/s$ ]

Requirement:  
 $Q < 0.01 \text{ mbar} \cdot \text{ml/s} = 1 \text{ Pa} \cdot \text{ml/s}$

$V$  : Test Volume [ $l$ ]

$\Delta P$  :  $P_0 - P_{\Delta t}$  = Pressure difference after  $\Delta t$  [ $Pa$ ]

$\Delta t$  : Measurement time [s]

Actual measurements

| $\Delta t$ [s]       | 0    | 10   | 20   | 30   | Error : $\pm 0.1$ [kPa] |
|----------------------|------|------|------|------|-------------------------|
| $P_{\Delta t}$ [kPa] | 48.8 | 48.9 | 48.9 | 48.9 |                         |

$$Q = \frac{1.57|48.8 - 48.9|}{30} = 5 \pm 5 \text{ [Pa} \cdot \text{ml/s]}$$

This measurement doesn't satisfy the requirement  $< 1 \text{ [Pa} \cdot \text{ml/s]}$

# Solution

- A) Upgraded the pressure gauge which can measure 10 times better precision.
- B) Leak Tight the fitting joint with the cooling tube.
- C) Longer measurement (15 minutes) for stability.

C) They've done extended ours measurement for 56 min. (3360 sec).

$$t=0[\text{s}] : P=-58.2 \text{ [kPa]}$$
$$t=3360[\text{s}] : P=-57.7 \text{ [kPa]}$$

$$Q = 0.23 \pm 0.046 \text{ [Pa ml/s]} < 1 \text{ [Pa} \cdot \text{ml/s]}$$

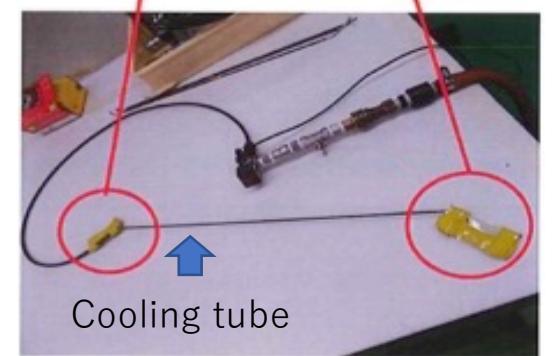
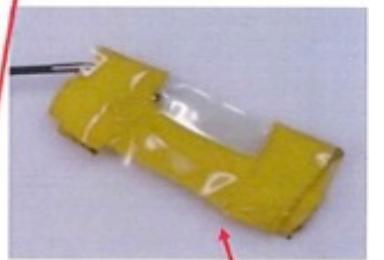
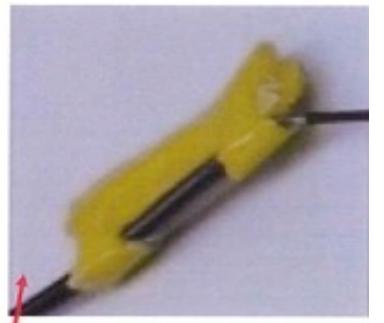
☞ This well meets the criteria, but tested only one tube.

A) \*\*.\* kPa → \*\*.\*.\* kPa



Pressure gauge  
Range : 0 ~ 20 kPa

B) Leak Tight Fitting Joint



# Cooling Pipe Leak Test (April 17<sup>th</sup> Update)

| Sample Number | Gauge Pressure (*.** kPa) |            |                 | Leak Rate<br>$Q$ [ml Pa/s] |
|---------------|---------------------------|------------|-----------------|----------------------------|
|               | $t=0$ [s]                 | $t=30$ [s] | $\Delta P$      |                            |
| 1             | -10.24                    | -10.24     | $0.00 \pm 0.01$ | $0.0 \pm 0.52$             |
| 2             | -9.50                     | -9.50      | $0.00 \pm 0.01$ | $0.0 \pm 0.52$             |
| 3             | -9.85                     | -9.85      | $0.00 \pm 0.01$ | $0.0 \pm 0.52$             |
| 4             | -9.36                     | -9.35      | $0.01 \pm 0.01$ | $0.5 \pm 0.52$             |
| 5             | -9.54                     | -9.53      | $0.01 \pm 0.01$ | $0.5 \pm 0.52$             |
| 6             | -9.73                     | -9.72      | $0.01 \pm 0.01$ | $0.5 \pm 0.52$             |
| 7             | -9.89                     | -9.89      | $0.00 \pm 0.01$ | $0.0 \pm 0.52$             |
| 8             | -9.37                     | -9.37      | $0.00 \pm 0.01$ | $0.0 \pm 0.52$             |
| 9             | -9.13                     | -9.11      | $0.02 \pm 0.01$ | $1.0 \pm 0.52$             |
| 10            | -8.97                     | -8.97      | $0.00 \pm 0.01$ | $0.0 \pm 0.52$             |
| 11            | -8.85                     | -8.84      | $0.01 \pm 0.01$ | $0.5 \pm 0.52$             |
| 12            | -8.07                     | -8.06      | $0.01 \pm 0.01$ | $0.5 \pm 0.52$             |
| 13            | -8.11                     | -8.10      | $0.01 \pm 0.01$ | $0.5 \pm 0.52$             |

Gauge measures 10 Pa level

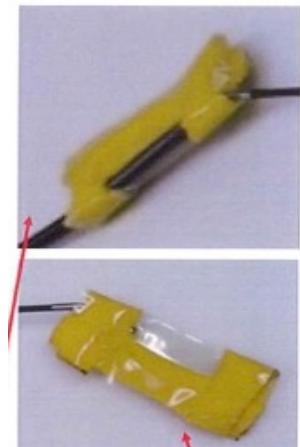
# Discussion

- 13 cooling tubes are tested
  - 6 tubes observed 0.00 kPa/30s pressure change :  $< 0.01 \text{ mbar ml/s}$
  - 6 tubes observed 0.01 kPa/30s pressure change :  $\leq 0.01 \text{ mbar ml/s}$
  - 1 tube observed 0.02 kPa/30s pressure change :  $\sim 0.01 \text{ mbar ml/s}$
- Evidently, their measurement needs to be improved to safely meet the requirement.
- The applied pressure was around  $-10 \sim -8$  instead of  $\sim -58$  last time. The pressure was factor of  $6 \sim 7$  weaker, which cannot be blamed because we didn't specify in the contract. However tubes suppose to be survivors of 60 psi ( $\sim 4\text{atm}$ ) for 1hour burst test.
- For this time, I will let them proceed to 12 stave assembly except for 0.02 kPa/30s tube.

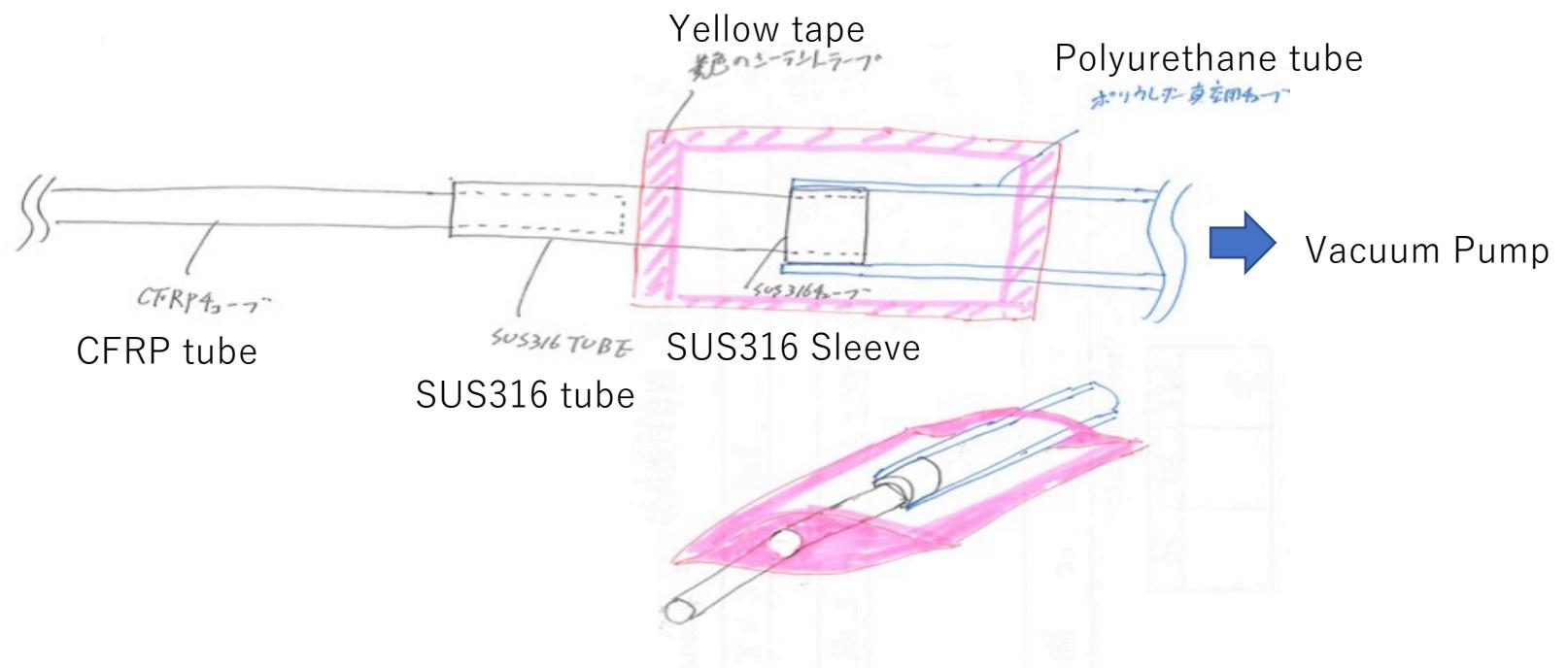
## For Next Round (Future)

- Dan and Rob proposed even higher leak tight criteria:
  - $0.01 \text{ ml-mbar/s}$  ( $0.6 \text{ ml-mbar/min}$ ) ->  $0.2 \text{ ml-mbar/min}$
- Perhaps we better provide leak tight fitting joint to them if possible. As you can imagine for their setup photo, they have a hard time to establish leak tight condition at the joint.
- Longer measurement in the order of 15 minutes to 12hours need to develop measurement infrastructure. Sequential measurement of 150 cooling tubes doesn't sound feasible. Need to achieve at least 10 tubes parallel measurement which requires investment on their infrastructure.

Leak tight established by tape (not ideal solution for production)



# ASUKA's setup around the joint



# Carbon Fiber Tubes



- I found Asuka co. procured carbon fiber tubes from one of local fishing rod makers and not from ROCKWEST.com
- There is no specification available in their web page. The order was custom made.
- As far as I heard, the carbon fiber tubes are made based on TORAYCA T700 which is allowed based on the statement in the design “TORAYCA T700 or equivalent”.
- I will ask them to check the leak tightness of the carbon fiber tube for extended period at least once.
- Do you have any suggestion in further testing?

<http://www.saoya-kimuraya.com>

# Asuka's Original Report

2020/4/16 御アスカ 吉川

Prototype Stave Design  
CFRPチューブリークテスト

**Q<0.01mbar・ml/s**  
**0.01mbar=0.001kpa=1pa**

圧力変化法(真空引きにて検査)

圧力ゲージ表示Kpa(\*,\*\*)  
真空引き実施圧力ゲージ確認し  
真空ポンプバルブ締め後の圧力ゲージを確認

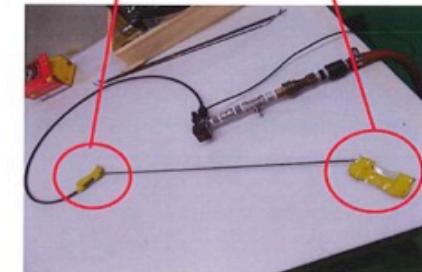
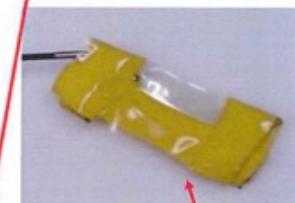
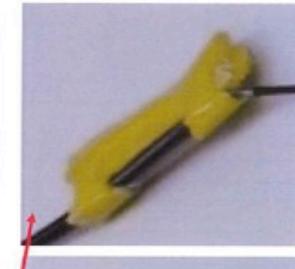
圧力ゲージ

30秒間に圧力ゲージの値の偏差を確認  
0.01Kpa以下の偏差であれば合格と判断

$$(測定例) Q(Pa,L/S) = \frac{V(P1-P2)}{\Delta t} = \frac{1.57(48.90-48.89)}{30} = 0.00052 \text{ リーク量}$$

| サンプルNo | ゲージ圧力(*,**Kpa) |        |         |
|--------|----------------|--------|---------|
|        | 0秒             | 30秒    | リーフ量    |
| 1      | -10.24         | -10.24 | 0       |
| 2      | -9.50          | -9.50  | 0       |
| 3      | -9.85          | -9.85  | 0       |
| 4      | -9.36          | -9.35  | 0.00052 |
| 5      | -9.59          | -9.53  | 0.00052 |
| 6      | -9.73          | -9.72  | 0       |
| 7      | -9.89          | -9.89  | 0       |
| 8      | -9.37          | -9.37  | 0.00052 |
| 9      | -9.13          | -9.11  | 0       |
| 10     | -8.97          | -8.97  | 0.00052 |
| 11     | -8.85          | -8.84  | 0.00052 |
| 12     | -8.67          | -8.66  | 0.00052 |
| 13     | -8.11          | -8.10  | 0.00052 |
|        |                |        |         |
|        |                |        |         |

上記試験にて12本とも圧力偏差は0.01Kpaまでであった為  
0.01mbar・ml/s=0.001kpa・ml/s以下としております。



# Summary

- Feeding materials to NCU has been managed so far not to stop their activities.
- 12 Staves are to be delivered by the end of April. These preproduction versions are to be evaluated in BNL before we move on to production.
- Stave is the schedule driver of the INTT ladder assembly.
- Shipping to BNL of HDI and Staves are on hold. I need a logic to approve this shipping as the essential business in RIKEN.
- What we can do?